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**Monitoring Groundwater and  
River Interaction Along the  
Hanford Reach of the  
Columbia River**

M. D. Campbell

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April 1994

Prepared for the U.S. Department of Energy  
under Contract DE-AC06-76RLO 1830

Pacific Northwest Laboratory  
Operated for the U.S. Department of Energy  
by Battelle Memorial Institute



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Richland, Washington 99352

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## Executive Summary

As an adjunct to efficient Hanford Site characterization and remediation of groundwater contamination, an automatic monitor network has been used to measure Columbia River and adjacent groundwater levels in several areas of the Hanford Site since 1991. Water levels, temperatures, and electrical conductivity measured by the automatic monitor network provided an initial database with which to calibrate models and from which to infer ground and river water interactions for site characterization and remediation activities. Measurements of the dynamic river/aquifer system have been simultaneous at 1-hr intervals, with a quality suitable for hydrologic modeling and for computer model calibration and testing. This report describes the equipment, procedures, and results from measurements done in 1993.

During 1993, Columbia River and groundwater elevations were measured hourly at 50 locations in seven areas of the Hanford Site in southcentral Washington State. Water temperature was measured at 10 of these locations; electrical conductivity was measured at five.

Water level accuracy is unknown, but is believed to be within  $\pm 0.1$  ft. Factors affecting accuracy are topographic surveys, instrument calibrations, and steel tape measurements. Measurement precision appears to be within  $\pm 0.02$  ft for wells and  $\pm 0.2$  ft for river stage. Repeated steel tape measurements vary within  $\pm 0.01$  ft. Survey errors vary with distance between sites, but most appear to be less than  $\pm 0.07$  ft.

Visual inspection and graphic review of data confirmed its continuity. Comparisons between simultaneous steel tape and datalogger readings were used as periodic data quality checks. River elevations varied up to 15 ft during the year and up to 9 ft during a single day. The 300 Area river elevation varied about 60% as much as the other stations because of the influence of the McNary Dam forebay. Ice Harbor Dam tailwater also influenced the fluctuation of the river in the 300 Area. Groundwater elevations varied up to about 3 ft per day in a few wells nearest the river and up to about 6 ft over the season in some wells.

Electrical conductivity of water in wells was influenced by river intrusion to a small degree. Riverbank seep conductivity varied between river and well values. Each of these factors is important in more efficient site characterization and remediation.

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## 1.0 Introduction

Aquifer hydraulic properties and head gradients control contaminant migration to the Columbia River. Contaminant migration also depends on concentration and thermal gradients operating in the aquifer/river system. Properly calibrated computer models can process such data to simulate interactions between the unconfined aquifer and the Columbia River to show likely consequences of remediation. Measurement variety, frequency, and accuracy must satisfy model requirements for acceptable predictive reliability.

The monitor network is a feasible and economical system of collecting the simultaneous and frequent data required for remedial investigation of river and groundwater interaction. Monitors collect the data automatically and transmit it by radio telemetry to a computer for storage and processing.

During 1993, river and groundwater levels were measured by an automatic monitor network at 50 locations in seven areas along the Columbia River on the Hanford Site. Water temperatures at 10 locations and electrical conductivity at five locations were also measured. Pacific Northwest Laboratory (PNL)<sup>(a)</sup> personnel, under contract to Westinghouse Hanford Company (WHC), initiated network installation early in FY 1991 at 35 sites in the 300 Area, with nine sites added later that year in 100-F, -H, and -B Areas.

Emphasis and equipment were shifted from the 300-FF-5 Operable Unit to the 100 Aggregate Area Operable Unit during the spring of 1993. Monitors removed from the 300 Area were installed in 100-D, -N, and -K Areas and added to the number in the -F, -H, and -B Areas. Eleven wells and one river station are still monitored in the 300-FF-5 boundary while the others are spread about evenly among the 100 Areas. The monitor network currently consists of 44 radio transceivers and 42 automatic dataloggers, with one station in each area, except 100-N, serving two wells. The seven areas currently monitored are shown in Figure 1.

This report summarizes conductivity, temperature, and water level data obtained by the network. Equipment and procedures are detailed. The monitor stations are discussed. Quality and calibration are discussed, followed by measurements and the programs used to make them. Electrical conductivity, temperatures, and water levels are presented and discussed. Finally, measurements and their frequency and precision are presented and discussed, and conclusions are presented. Network programming and other information are presented in the appendixes.

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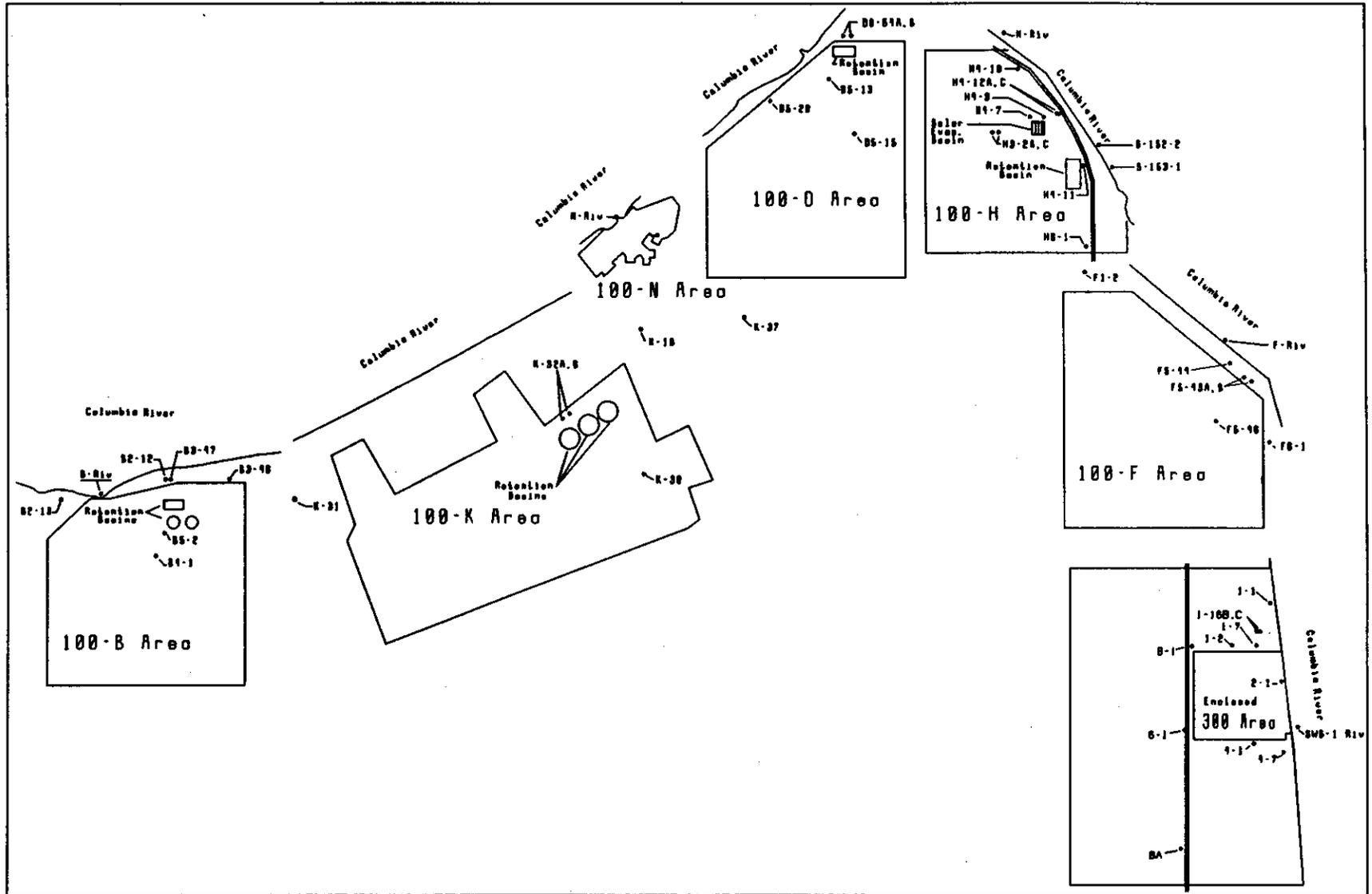


Figure 1. Network Monitor Station Locations During 1993

## 2.0 Equipment

Monitor network stations have a datalogger, a frequency modulated (FM) radio transceiver with a radio frequency (RF) modem connected to the datalogger, an FM antenna, and a 12-volt battery with a solar recharging panel. The datalogger, modem, and transceiver are installed in a weather enclosure. The entire assembly is mounted on a tripod or a well post pipe. Forty-eight of the 50 sites have pressure transducers to measure water depth. Ten sites have thermocouples to measure water temperatures. Five sites have probes to sense electrical conductivity and water temperature. The electrical conductivity measurements, corrected for temperature, reflect the concentration of dissolved ions.

### 2.1 River Stations

Two of the five river stations have the transducer retainer pipe extending down the river bank slope into the water at an angle. One station is staked to the bank and is likely to move with time. These two stations, located at 100-F and 100-H, require adjustments to the steel tape measurements taken along the pipe to compensate for their non-vertical angle. The 100-F correction is  $0.2425 \times$  tape reading. The 100-H correction was  $0.4395 \times$  tape reading up to January 25, 1994 and  $0.4417 \times$  tape reading thereafter. The other three stations, 100-B, 100-N, and SWS-1 in the 300 Area, have vertically mounted transducer retainer pipes. SWS-1 in the 300 Area has a river stage scale mounted on the concrete wall next to the retainer pipe. Although river stage can be read directly from the scale, survey indicated the need for a 0.4 ft adjustment. The 100-N and 100-B stations require steel tape measurements from the top of the top pipe coupling to the water surface.

All river station elevations were surveyed. The SWS-1 scale was reported to be 0.4 ft lower than its indicated value. Thus, the 345-ft stage scale mark is actually 344.6 ft above mean sea level (MSL). The 100-F river station surveyed as 373.33 ft above MSL at the top, south corner of the channel iron. The bottom south corner of the channel was 368.48 ft above MSL. The 100-H river station was originally surveyed as 386.47 ft above MSL at the top of the 2-in. pipe coupling; resurvey on January 25, 1994 set the elevation at 386.83 ft above MSL. The 100-N river station surveyed as 426.09 ft above MSL at the top of the pipe coupling. The 100-B river station surveyed as 448.32 ft above MSL at the top of the pipe coupling.

The 100-H river station has an electrical conductivity cell as well as a pressure transducer attached. This station measured depth, electrical conductivity, and temperature of the water. Water depth was recorded as a feet-per-volt ratio, ranging between 0. and 15.xxxx. Electrical conductivity was recorded as milliSiemens, ranging from 0.0000 to 0.5xxx. Electrical conductivity before October 5, 1993 required temperature compensation during data processing, but it was compensated in the datalogger after that date. Temperature ranged from 0 to 30°C.

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## 2.2 Single-Well Stations

Single-well stations have transducers connected to channels 1 and 2 of the current dataloggers, with orange, black, yellow, and blue wires connected to 1H, 1L, 2H, and 2L, respectively. The red wire is connected to the E1 excitation channel and the white wire connected to any AG. The silver wire is not connected because of its tendency to create a ground loop.

## 2.3 Multiple-Well Stations

Multiple-well stations have transducers connected sequentially. The transducer from the first well, numerically or alphabetically, is connected as described for the single well station. The second transducer is connected with orange, black, yellow, and blue going to 3H, 3L, 4H, and 4L, respectively. The red wire is connected to E1 with the first transducer, and the white wire is connected to any AG terminal.

The readout from multiple-well stations is in the sequence wired. Early in the monitor project, some well numbers were unknown when we began monitoring them. In some cases, the sequence was reversed, causing difficulty in quality control. This problem required help from the Database Manager in the Geosciences Department of WHC or reference to the Laboratory Record Book to avoid errors in data interpretation.

## 2.4 Multiple Sensor Stations

Pressure, temperature, and electrical conductivity of water were measured in some locations. Stations that measured all three were wired to measure pressure, electrical conductivity, and temperature, in that order. The electrical conductivity cell has six wires. Either the blue or the black wire can be used, but not both. The black wire is used when high resolution is required. The connections used were red-6L, white-6H, green-E3, black-E2, purple-AG, and clear-G. This configuration avoids interference and allows for use of two pressure transducers on a single datalogger.

Where electrical conductivity is measured, temperature is also measured by the same transducer and used to compensate for thermal changes in the river or groundwater solution.

## 2.5 Datalogger Programs

The transducers used in our monitor systems require precise, selectable excitation, and simultaneous measurements of transducer excitation and output. The datalogger programs to accomplish this task are shown in Appendix A.

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### 3.0 Procedures

Periodic maintenance and tests were required to assure quality data through proper equipment operation. Tape and datalogger readings recorded simultaneously were compared with previously recorded sets to detect changes. Errors and problems were addressed. Initial calibration and recalibration determined the factors for data reduction. Battery voltage was measured periodically, and desiccant packages were replaced to help ensure proper equipment operation.

#### 3.1 Paired Tape and Datalogger Tests

Water levels at a site were simultaneously measured by steel tape and by a datalogger. Readings were repeated when paired reading sets disagreed with previously paired reading sets.

An equivalent change in water level is required by the tape and the datalogger. The following equation was used to deal with errors:

$$T_1 - T_2 = f(DL_1 - DL_2) \tag{1}$$

where  $T_1$  and  $T_2$  are steel tape readings 1 and 2, "f" is the calibration factor for the transducer, and  $DL_1$  and  $DL_2$  are the paired datalogger readings 1 and 2.

Dataloggers measured volt ratios as transducer voltage output/input. The following equation converts the datalogger reading into elevation relative to MSL elevation:

$$E_{MSL} = E_{ToC} - T + (DL - DL_T) \times F \tag{2}$$

- where  $E_{MSL}$  = elevation above Mean Sea Level
- $E_{ToC}$  = surveyed elevation at top of the well casing
- T = steel tape measurement
- DL = ambient datalogger reading
- $DL_T$  = datalogger reading taken with the tape reading
- F = the calibration factor for the transducer.

All pressure transducer readings were preserved as volt ratios. Calibration factors were not stored with raw data. Raw data were preserved in computers in two separate locations, readily accessible for processing.

Datalogger resolution is  $0.33\mu V$  on its most sensitive range, which corresponds with 0.000123 ft of water elevation change. Both voltage and depth resolution are displayed in Table 1.

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**Table 1. Datalogger Range and System Resolution, Assuming Calibration Factor of 0.93 ft/volt-ratio**

Datalogger			
Range		Sensitivity (mv)	System Resolution (ft)
Code	(mv)		
21	2.5	0.00033	0.0001
22	7.5	0.00100	0.0003
23	25.	0.00333	0.0012
24	250.	0.0333	0.012
25	2500.	0.333	0.12

### 3.2 Calibration Checks

Cross-checking the datalogger readings with the steel tape measurements helped identify errors. Errors have been traced to well casing extension, misread tape, transducer movement, transducer failure, and datalogger wiring panel failure. Table 2 shows examples of correct and erroneous tape and datalogger reading sets. (See Appendix B for all reading sets.) Some well casings were extended upward approximately 1 ft when some of the older wells were renovated. When the work was done, a time lag occurred before resurvey records were available, so the water elevations appeared incorrect until resurvey.

Steel tape measurements are commonly accepted as the standard, but tape reading accuracy depends on technique, individual observation, and weather conditions. For example, tape may be lodged on an obstacle rather than suspended straight into the water. Detection of this problem depends on the observer's skill and judgment. Also, the wet line across the tape scale may result from either normal water submergence or from contact with a condensing surface and may also require the observer's judgment. Repeated tape measurements revealed observer errors ranging up to 10 ft. Errors were more difficult to detect and resolve in wells with other equipment. Large amounts of condensation near the top of the well casing made accurate measurement more difficult. However, we repeated measurements to verify the steel tape readings within 0.01 ft. Disagreement between steel tape and transducer readings required repeat readings to achieve consistency. Steel tape readings should be questioned and proven by replicated remeasurement.

### 3.3 Precautions and Sources of Error

Errors in Table 2 and Appendix B include those that are positive because a steel tape or datalogger reading was too small. Errors that are negative result from a steel tape or datalogger reading that is too large. Condensate wetting of a steel tape causes a positive error. Transducer cable slippage and steel tape hangup cause a negative error. Aquifer changes from wind cause both positive and negative

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errors. Survey or well casing modifications may cause either type of error. Survey errors usually affect accuracy, not precision. Gradual relaxation of the transducer cable causes errors, but they are usually small. Temporary hang-up of a transducer on a pump or other obstruction in the well causes error. Samplers and well maintenance crews frequently remove or adjust pumps; this cause of error is relatively common. Error detection is done by plotting normalized differences between simultaneous water elevations in similar wells. Differences are cause for system calibration recheck.

Errors increase with datalogger range because resolution decreases, as shown in Table 1. Since it is necessary to use a greater range in river stations than in wells, the errors in river measurements are greater in the river data. Errors from topographic survey should be less than  $\pm 0.06$  ft, for most wells.

Transducers produce errors as a result of plugged ports or vent tubes. Water, debris, or a compressed cable cause this type of error. The vent tubes are checked, and a dry desiccant is placed in the vented enclosure to keep air vents clean and dry. Small animals, most likely porcupines, have chewed through three transducer cables during 1993. Larger animals, such as coyotes, have not been able to bite through the cover, however.

If monitor system battery voltage drops too low, directly measured voltages increase. This type error is most likely where solar panels fail to recharge the lead-acid battery, especially during winter time. The pressure transducer and other readings will gradually go too high and will finally be recorded as -99999 when overrange conditions exist.

Errors in the data were detected by listing each file after data download and by field observation. Slipped fittings or observed well pumping or renovation called for error checks.

### 3.4 Desiccant and Battery Service

Battery voltages were measured monthly to detect potential power supply problems without data loss. During December of both 1992 and 1993, battery power proved inadequate on several stations. Low voltages were detected and batteries were replaced without significant data loss. However, the causal problems differed between years. During cold winter weather in 1992, the large, 80-Ah, liquid, lead-acid batteries discharged by parallel connection to the small gel-cell, lead-acid batteries and the sulfate hardened to prevent recharge. The liquid and gel cells should not be connected in parallel unless the solar charger and regulator are capable of voltage output great enough to recharge the liquid cell under low temperatures.

During December of 1993, the systems were operated without the large batteries, and the small gel cells lacked capacity to withstand the prolonged cloudy weather. Solar radiation was inadequate to recharge batteries during November, December, and January. Solar insolation during December 1993 was less than 10% of typical June radiation. Thus, it was necessary to replace and recharge batteries each week. Solar panel enlargement proved incapable of resolving the problem. Investigation of the power supply issue caused us to decide to do two things in the future: Install 40- to 60-Ah, sealed, lead-acid battery with a 2-yr shelf life, and set voltage regulators to output 14.1 V, with over-voltage supply with temperature drop. This will be done during early 1994.

The desiccant packs have been replaced when the 30% indicator button in each datalogger enclosure began to turn pink or when there was other evidence of humidity. When the packs were dried in the oven at the specified 250°F, they exploded. After securing new packs, we poked two small tack holes in the clear side of each pack to allow outgassing of the water vapor. We had no further problems. In each enclosure, all entrances except the breather vent were sealed. During cold, wet weather, replacement may be required each month. Desiccant replacement is not usually necessary during warm weather.

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## 4.0 Results and Conclusions

A year's data, from the earliest measured in 1993 up to day 340 (December 6), have been processed and plotted for representative sites in each of the seven areas (see Appendix B). We began by processing and plotting river data to show the potential driving forces for the Columbia River/aquifer interactions. Then data from selected wells in each area were processed and plotted to demonstrate the relative magnitude of interaction among the wells and between each well and the river. While all of the wells showed long-term change with the river, some wells showed no short-term interaction.

Electrical conductivity and temperature were measured in the river and in some wells. Examples and comparisons of seep conductivity and temperature changes were also prepared.

### 4.1 Data and Interpretations

River water elevation measurements for 1993 are shown in Figure 2. Note that time is displayed in Figure 2 and subsequent figures as day of year to match the database values. The range of fluctuation in Figure 2 is most notable, with the maximum just above 400 ft and the minimum just above 384 ft at the 100-B river station. The single-day fluctuation at 100-B was about 13 ft. Also notable in Figure 2 is the attenuation of the daily cycle as the water reaches the 300 Area. The cause of fluctuation in the 300 Area river between days 84 and 115 is evidently influenced by something other than the upstream river (e.g., the influences from McNary forebay and Ice Harbor tailwater).

Figure 3 depicts detail more than Figure 2 for four of the five river stations and more clearly displays the dependence of the downstream stations on the upstream water fluctuation. Again, the attenuation is apparent in the 300 Area. Figure 4 shows a still shorter and different interval for all five river stations. The attenuation in the 300 Area appears to be about 60% of the amplitude of the 100-B station, while all of the other stations demonstrate less than 20%. Figure 5 shows a nearly constant flow period for 10 days. However, the 300 Area river shows more than a foot of variation. The cause of this variation is the composite influence of the Ice Harbor Dam and McNary Dam releases. In short, the 300 Area is in the McNary forebay and responds to the releases from the Ice Harbor Dam.

Figure 6 shows the fluctuation of three wells and the river in the 300 Area, with the river data from station SWS-1. As expected, the river fluctuates most, and the well farthest from the river fluctuates least. Notably, the maximum river variation depicted is about 10 ft, whereas the 100-B river fluctuation for the same period was about 15 ft. Figure 7 shows a 3-day interval in which hourly elevations are visible. Clearly, the river appears to drive the variation. Well 2-1 is nearest the river, well 8-1 is farthest from the river, with well 1-2 midway between. It is somewhat surprising that fluctuations in well 2-1 are not larger because the well is within about a hundred feet of the river bank.

Figure 8 shows the 100-F river elevations, with variations from three wells. Measurements started in these wells in late May 1994. There is a clear pattern of related variation among the water levels. Figure 9 shows 10 days of water levels measured hourly. Wells F5-43A and F5-43B differ in that they access different horizons within the aquifer. It is surprising, however, that F5-43B responds to river

### RIVER WATER ELEVATION 300, 100-F, 100-H, 100-N, 100-B

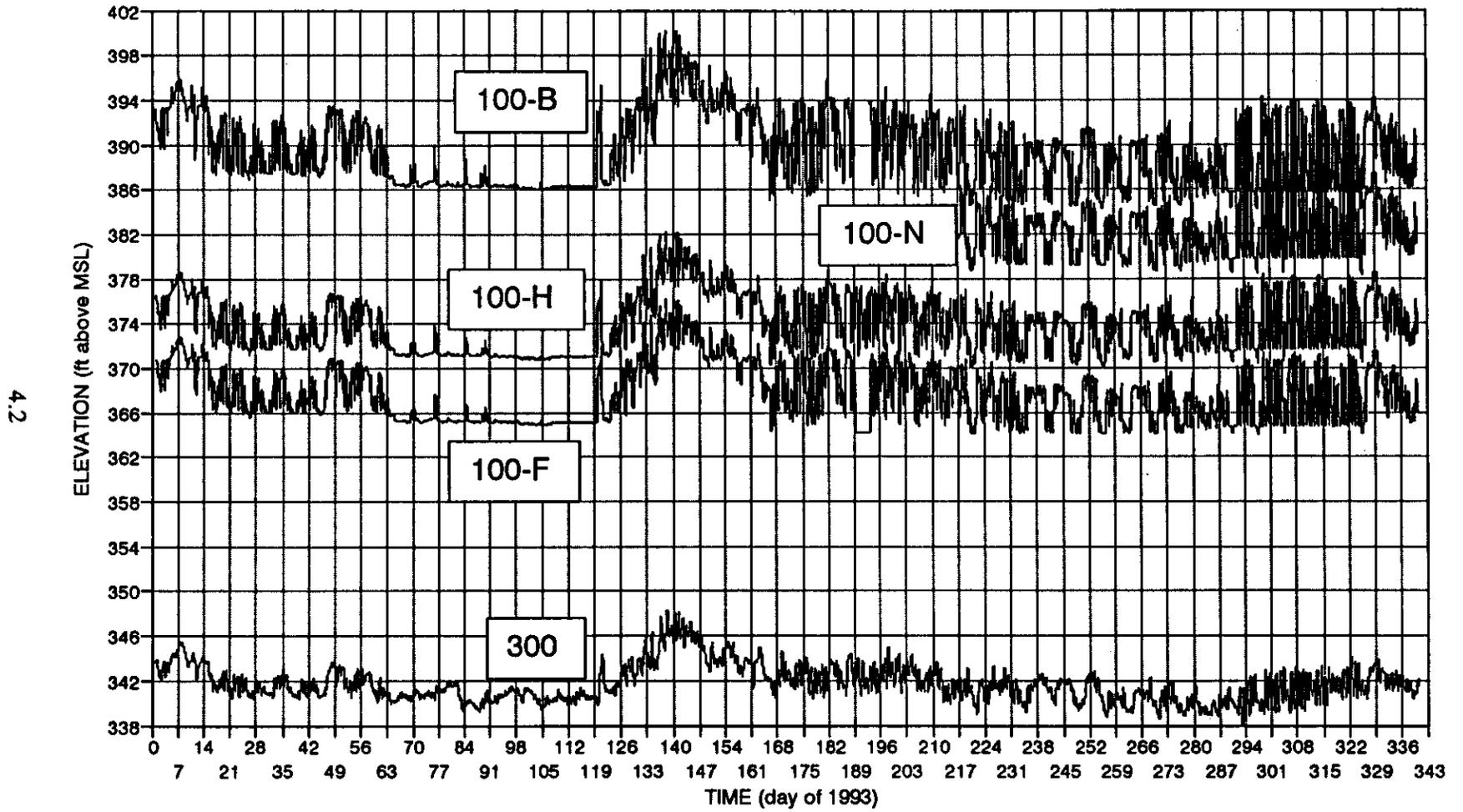


Figure 2. Columbia River Stage at Five Stations

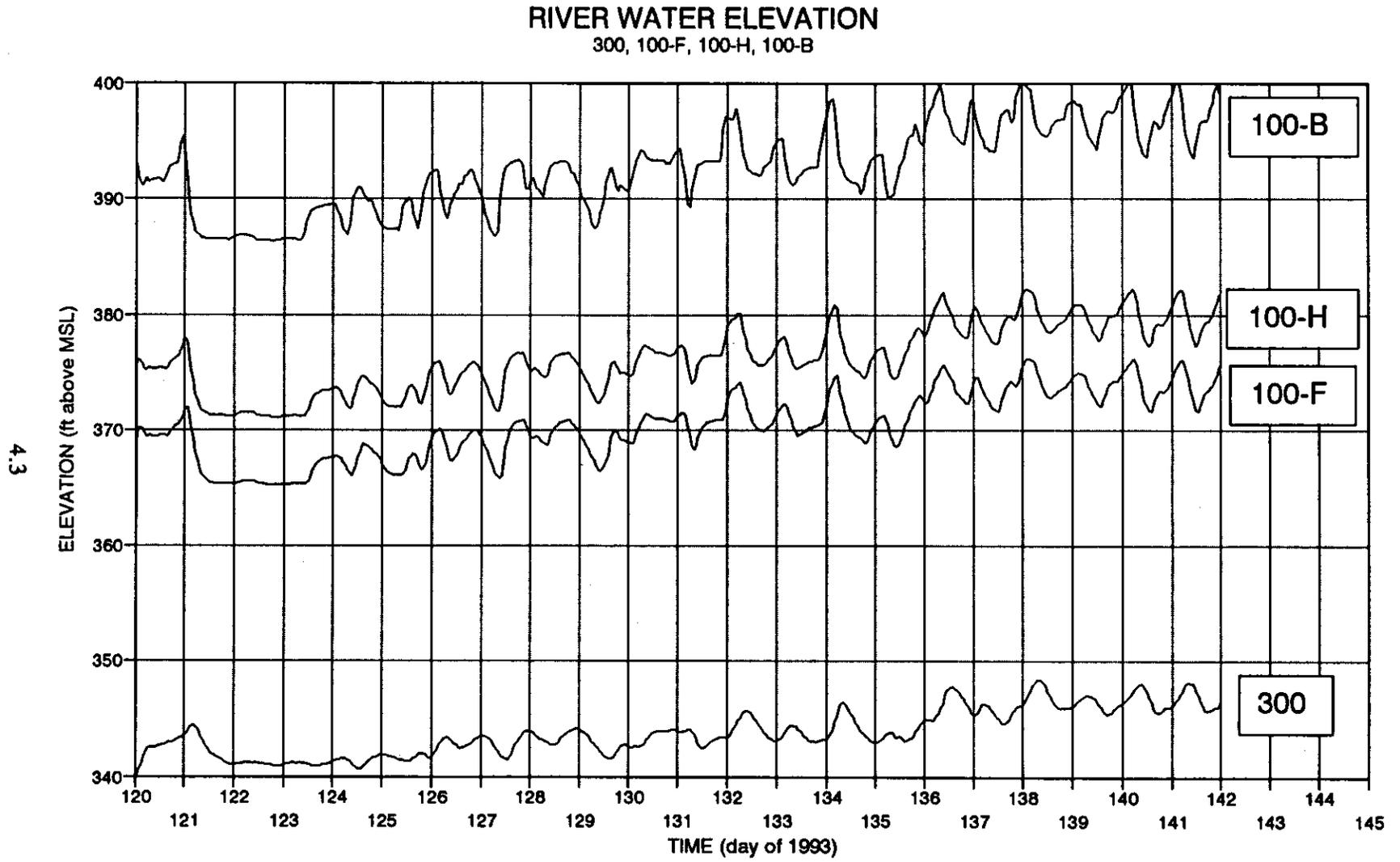


Figure 3. Columbia River Stage at Four Stations for 25 Days

### RIVER WATER ELEVATION 300, 100-F, 100-H, 100-N, 100-B

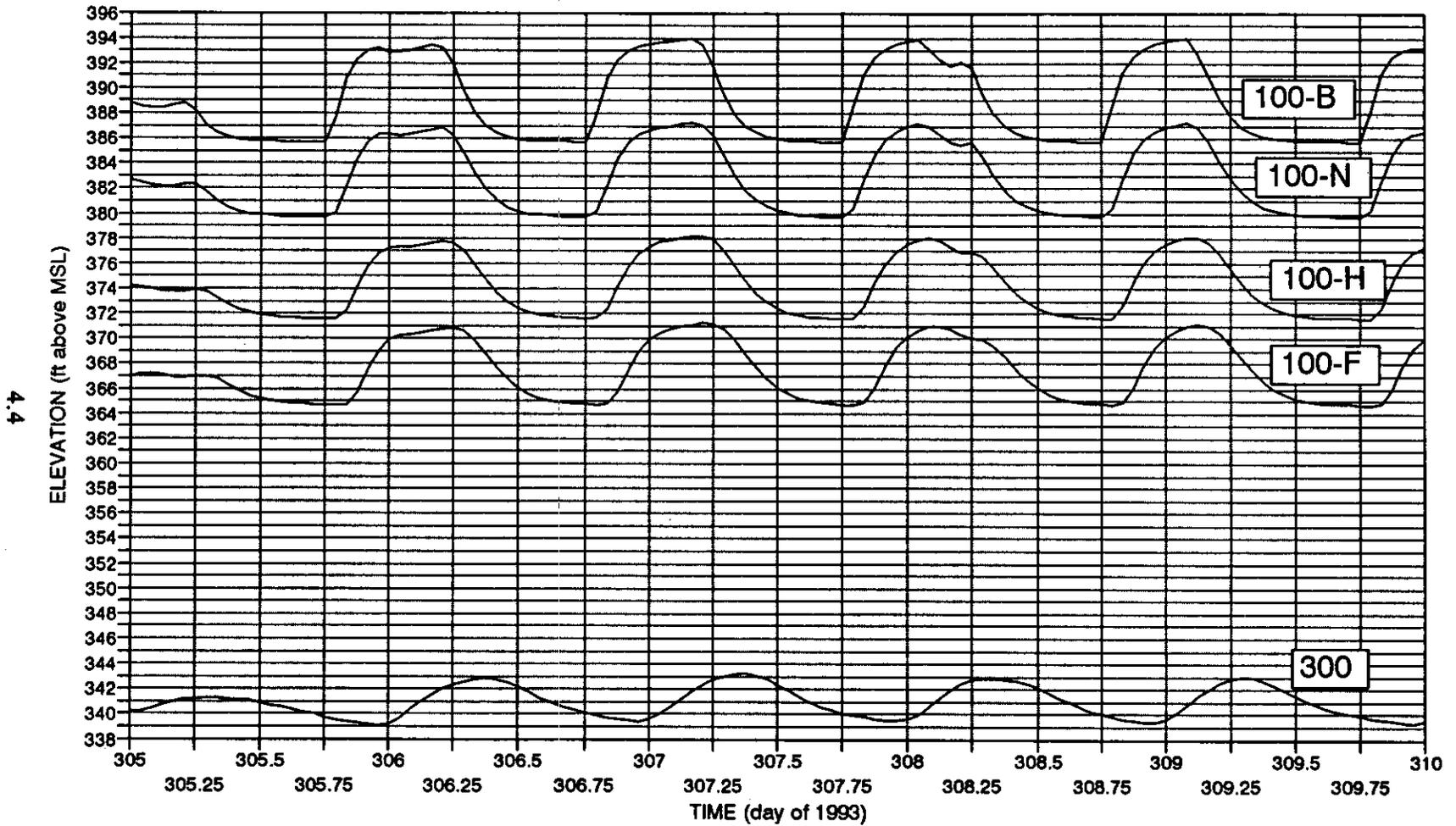


Figure 4. Columbia River Stage at Five Stations for Five Days, Showing Time Lag and Attenuation

### RIVER WATER ELEVATION 300, 100-F, 100-H, 100-B

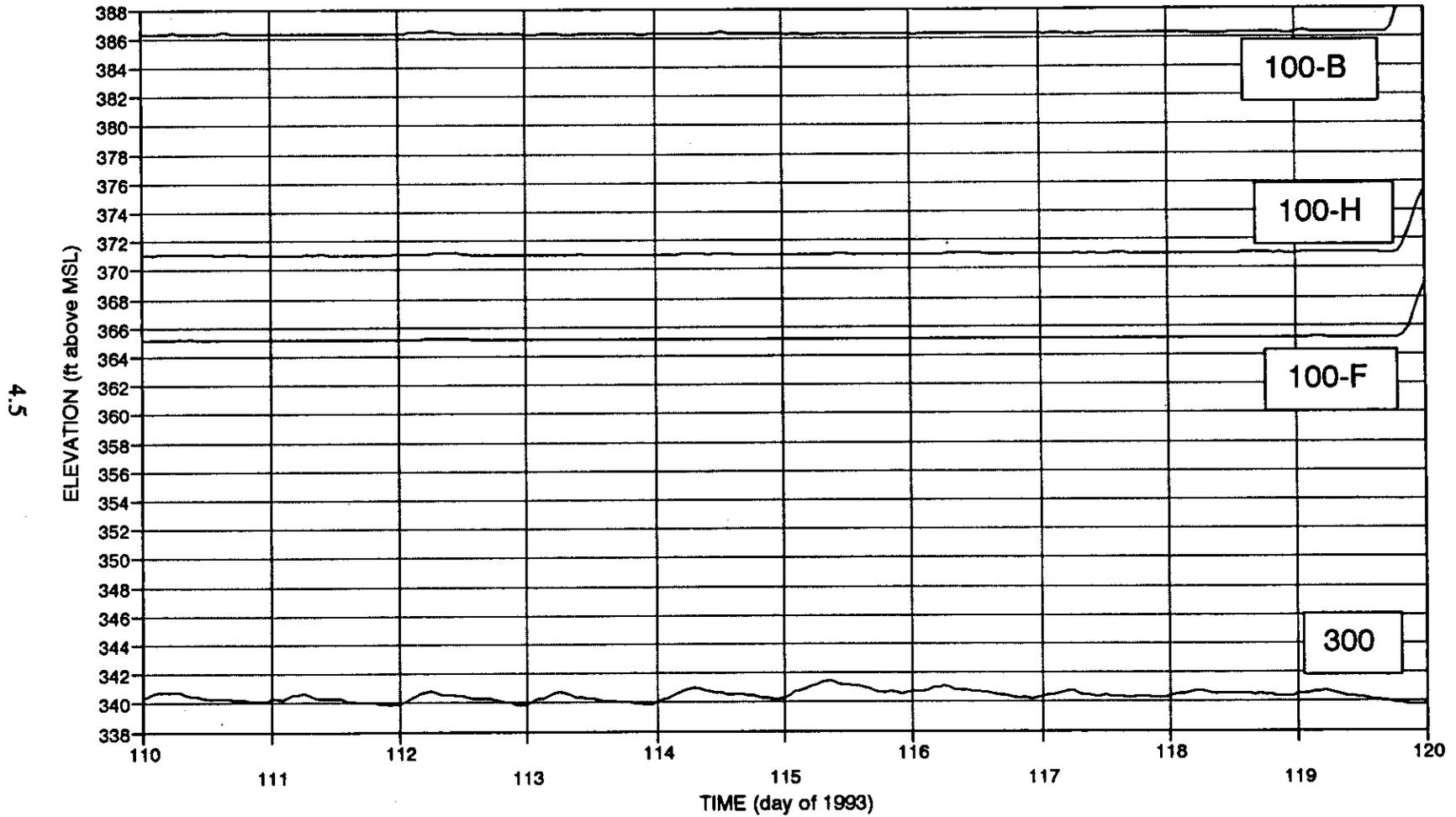


Figure 5. Columbia River Stage at Four Stations During 10 Days of Low Flow

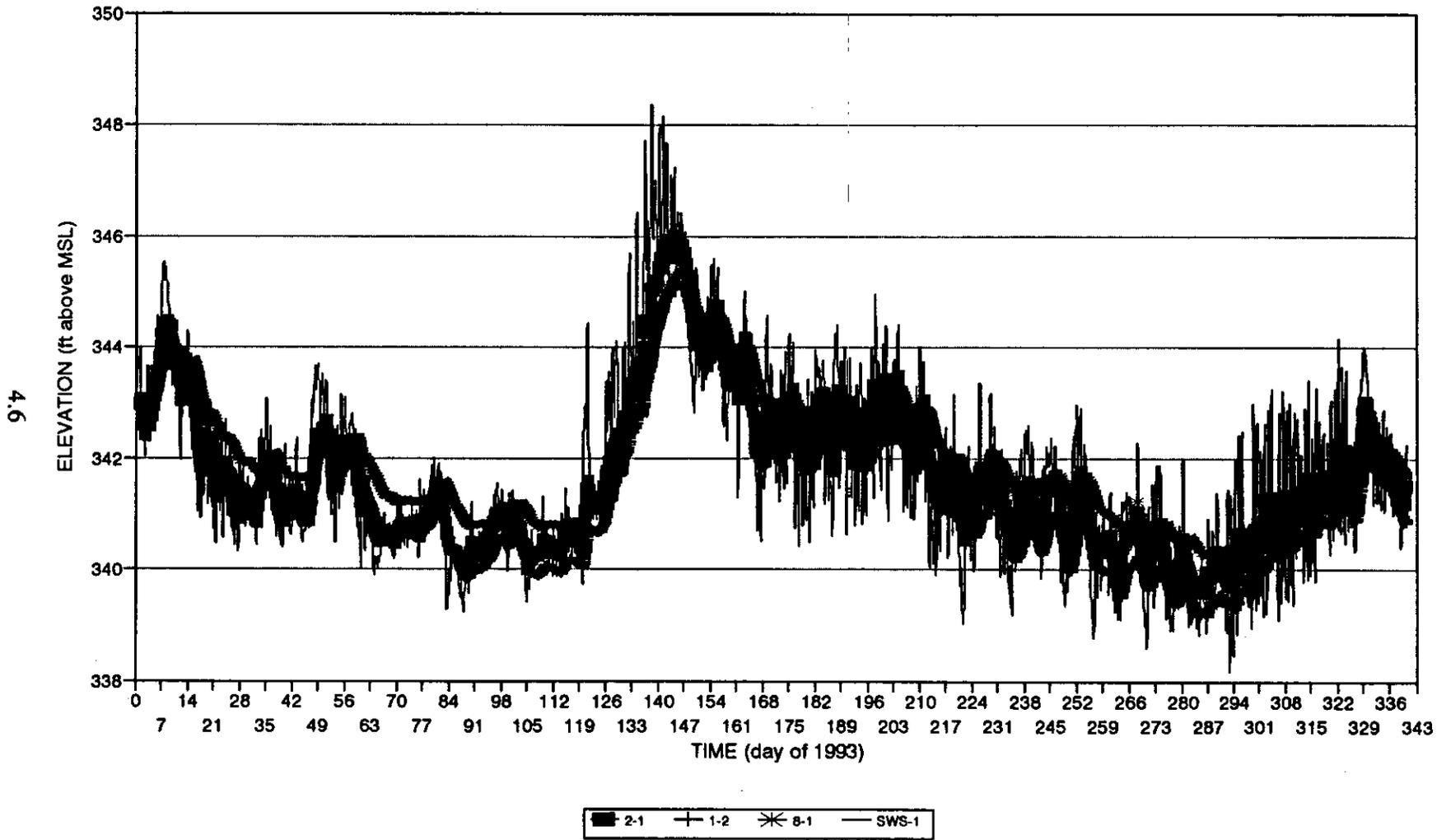


Figure 6. Water Elevations in Three Wells and The River in The 300 Area

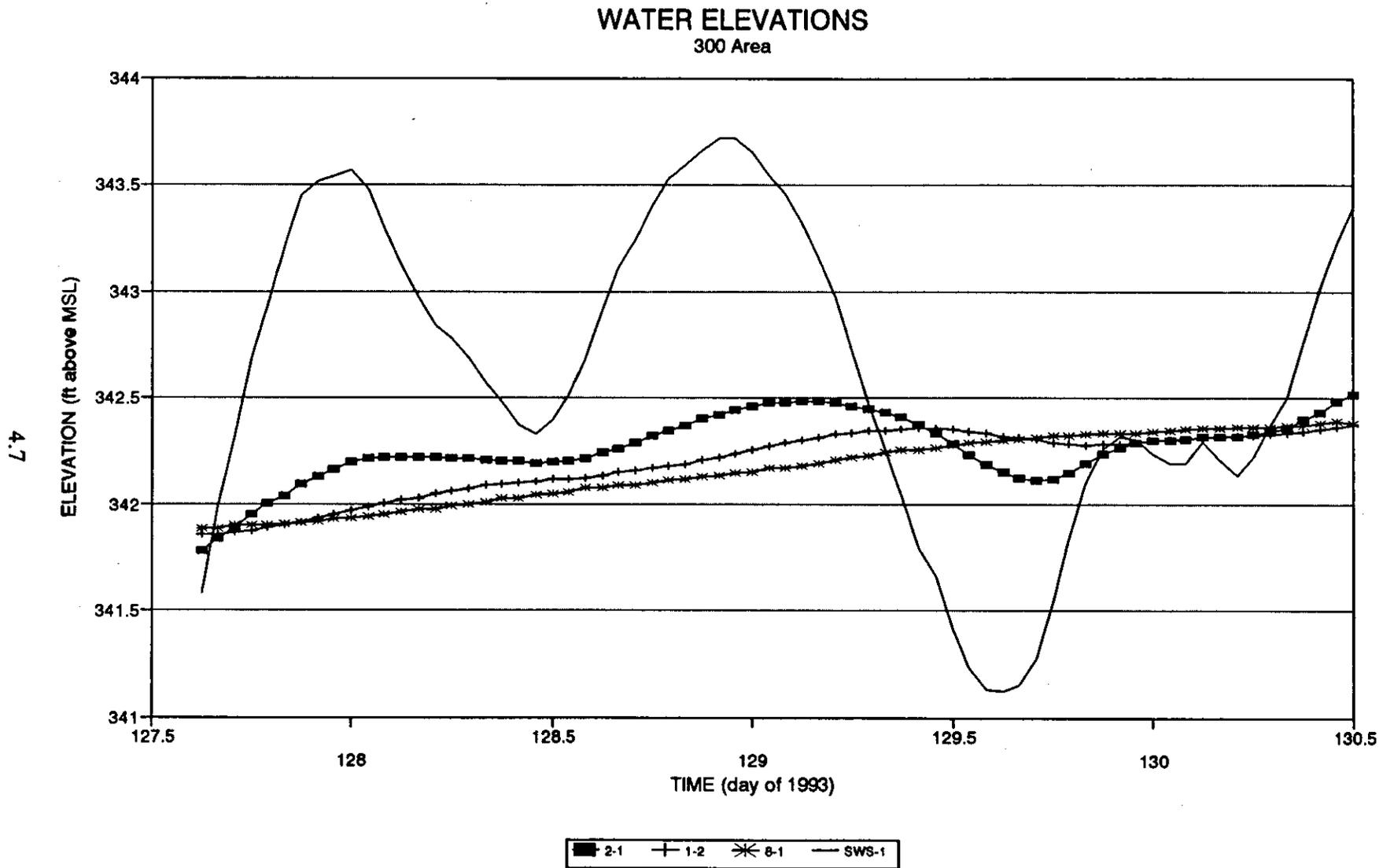


Figure 7. Detailed Variations in Water Elevations in The 300 Area

### WATER ELEVATIONS 100-F Area

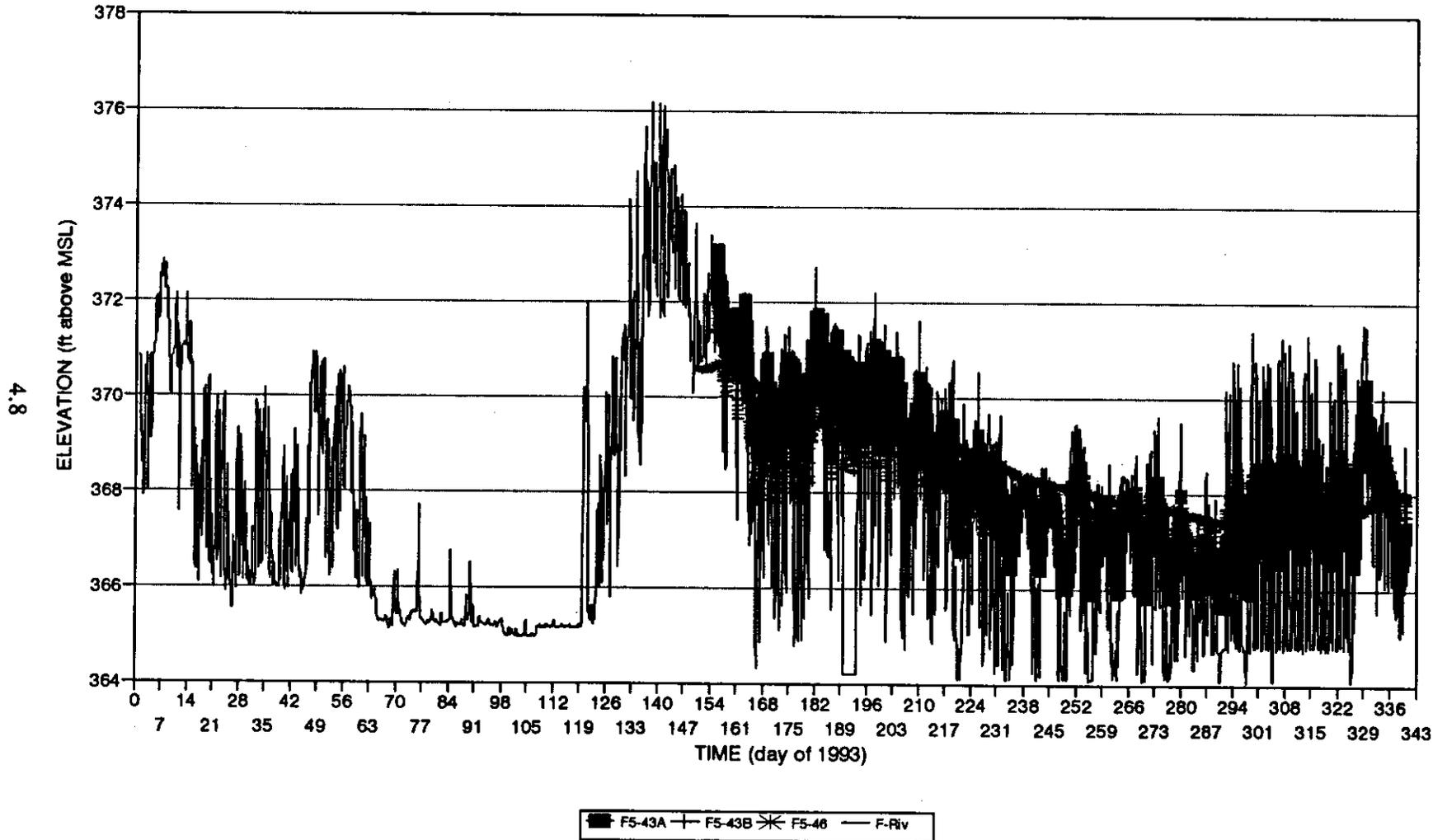


Figure 8. Water Elevations in Three Wells and The River at 100-F Area

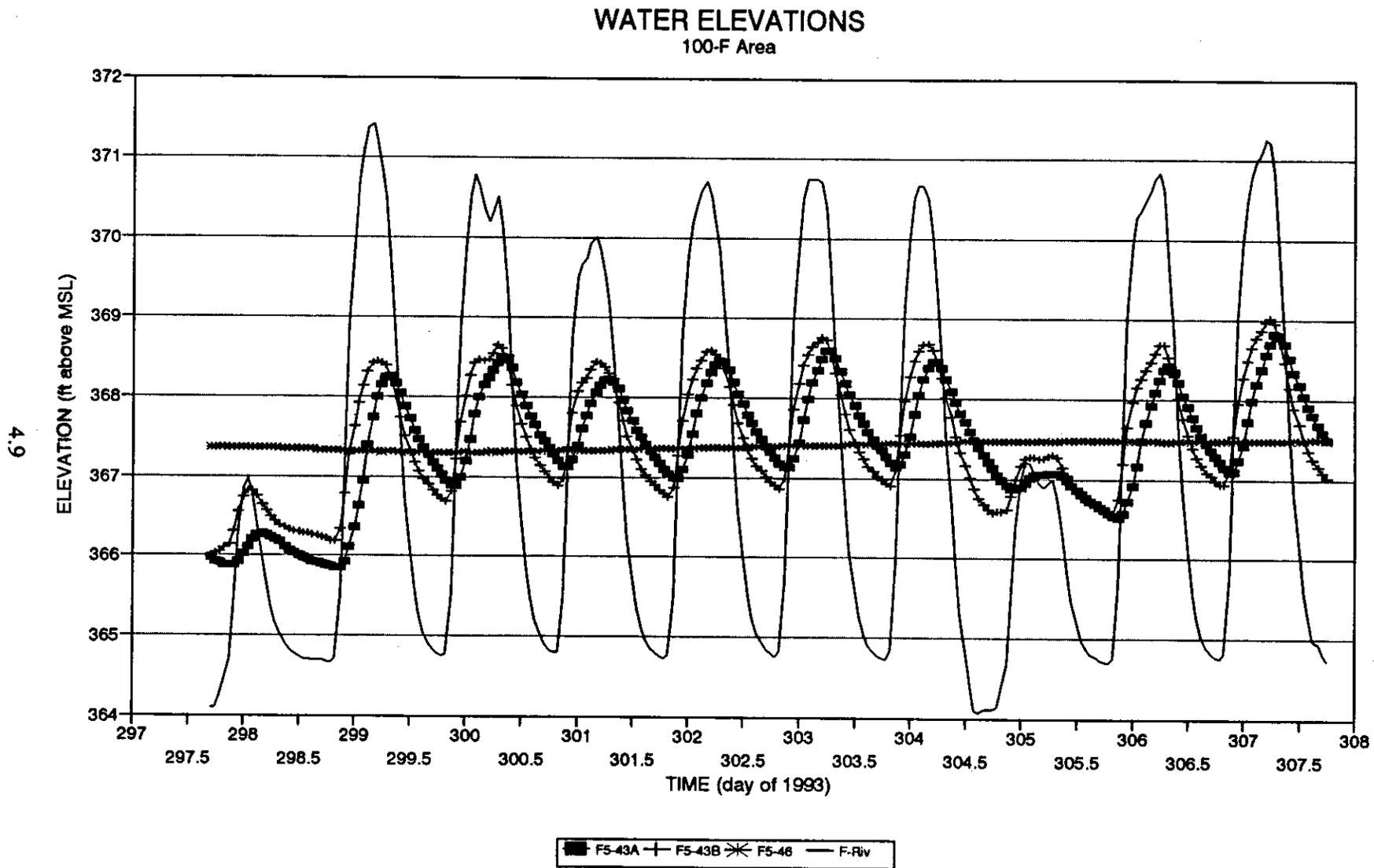


Figure 9. Detailed Variations in Water Elevations in 100-F Area

influence more rapidly and to a greater extent than F5-43A. Evidently, better hydraulic connection to or partial confinement of the lower phreatic aquifer accounts for the observed behavior in the 100-F Area. While there is long-term influence from the river on well F5-46, there appears to be essentially no influence within the 10-day time interval.

Figure 10 shows water elevations from the river and three wells in the 100-H Area. Here again, the river seems to influence all three wells. Well H4-11 is nearest the river and shows the greatest river influence. However, there appears to be an error in surveyed elevations. This appears to be why well H4-11 elevation is consistently higher than the river water elevation. There may, of course, be another cause for this phenomenon. There may be considerable water flow from up gradient toward the river past well H4-11. While this seems unlikely, it could justify the higher elevation observed in well H4-11. Another possibility is that the 100-H river station survey was incorrect. Resurvey revealed that there was an error of 0.45 ft. Also, transducer shift of about 1 ft was logged during tape and datalogger paired tests. The remaining possibility considered was that the top of casing survey for well H4-11 is in error. This has not been resurveyed. Even so, the relation of groundwater elevation to river elevation is unquestionable, in all three wells.

Figure 11 shows a data plot for a 5-day period, with data adjusted to display the relationships between river and groundwater changes. Well H4-11 clearly follows the river, even in fairly minor detail. While wells H3-2A and H3-2C are shown to follow the river in Figure 10, Figure 11 shows very limited response of H3-2C and no response from H3-2A. This also indicates either better hydraulic contact with the river or the existence of a partial confining layer between the upper and lower levels of the aquifer, as was the case in the 100-F area in well F5-43B.

Figure 12 shows a composite of wells in the 100-D and -K Areas with the 100-B river data superimposed. The 100-N river station was not installed until about day 217. Again, there appears to be a long-term trend for most wells to follow river fluctuation, with a greatly attenuated amplitude. Well D5-20 shows significant short-term fluctuation, with only token response from well K32A. Well D5-15 data remains unexplainable, though transducer error was a factor, and the transducer was replaced. Still, well behavior seemed independent of river fluctuation. Figure 13 demonstrates the short-term independence between the 100-D and -K Area wells and the river fluctuation. While Figure 4 showed the common pattern of fluctuation among all four 100-Area river stations, none of the 100-D or -K wells varied with this short-term pattern. Only well D5-20 shows cyclic response as short as 7 days.

Figure 14 shows water elevations in four wells in the 100-B Area, along with that in the river. Water levels in all four wells seem to vary with that in the river. Although all well water levels shown appear to be above the river level, it is helpful to recall from Figure 2 that 100-B river water elevations were more than 400 ft above MSL for a short period preceding the data interval shown. Figure 15 shows how well the well and river water elevations coincide. It would be more comfortable to explain the fluctuations in Figure 15 if well B2-12 were exactly 2 ft lower. However, well B2-12 is right next to well B3-47, and the tops of casings appear to be about the same, which survey has confirmed. Perhaps tape records were in error; but that is unlikely, based on seven separate sets of paired measurements without significant computed error. We would like to adjust the river level up, but the data from well B3-47 confirms a good match between it and the river. The only remaining explanation we have considered is the possibility that well B2-12 is upstream from the river in a close-coupled

6221-5726-116

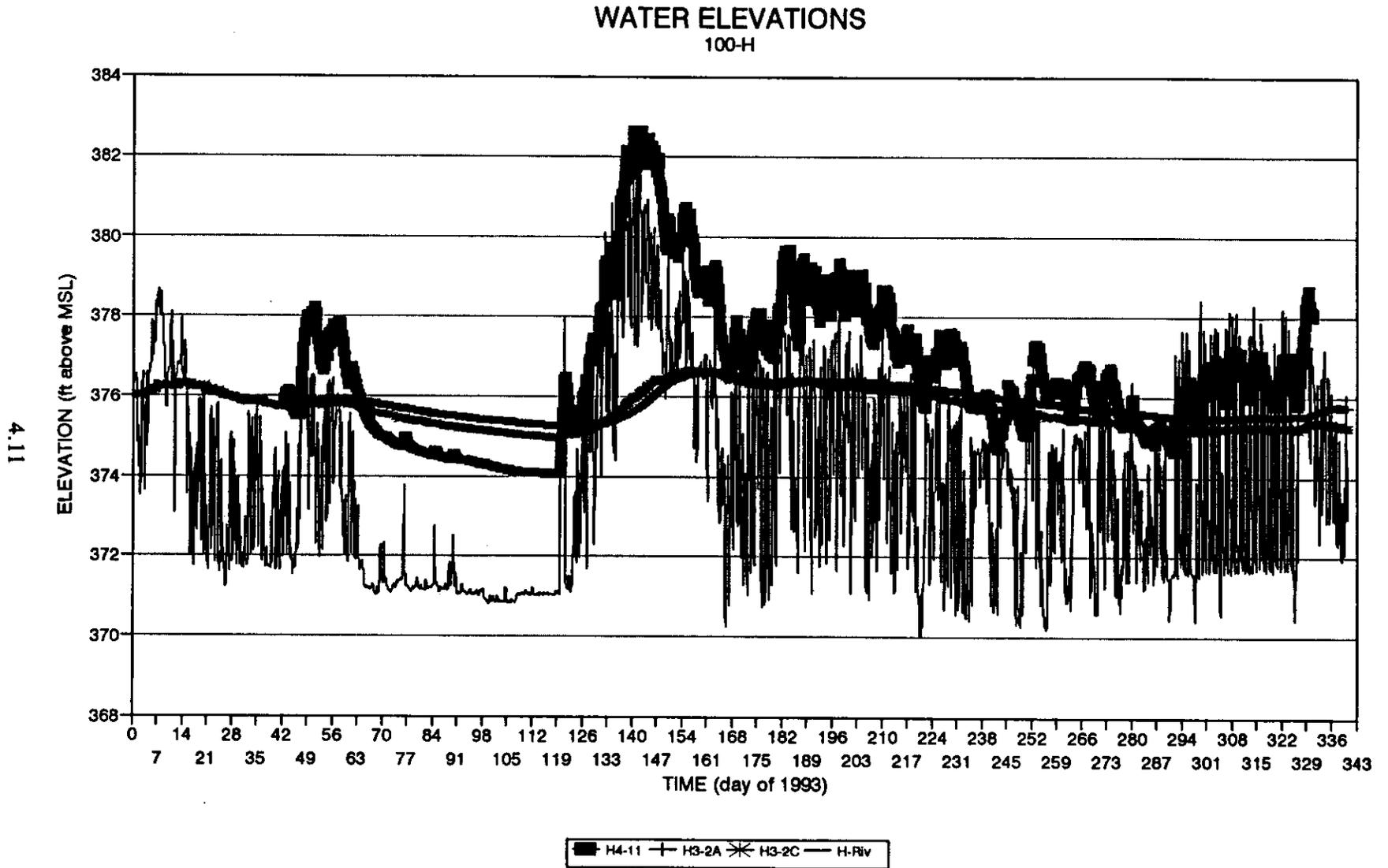


Figure 10. Water Elevations in Three Wells and The River in 100-H Area

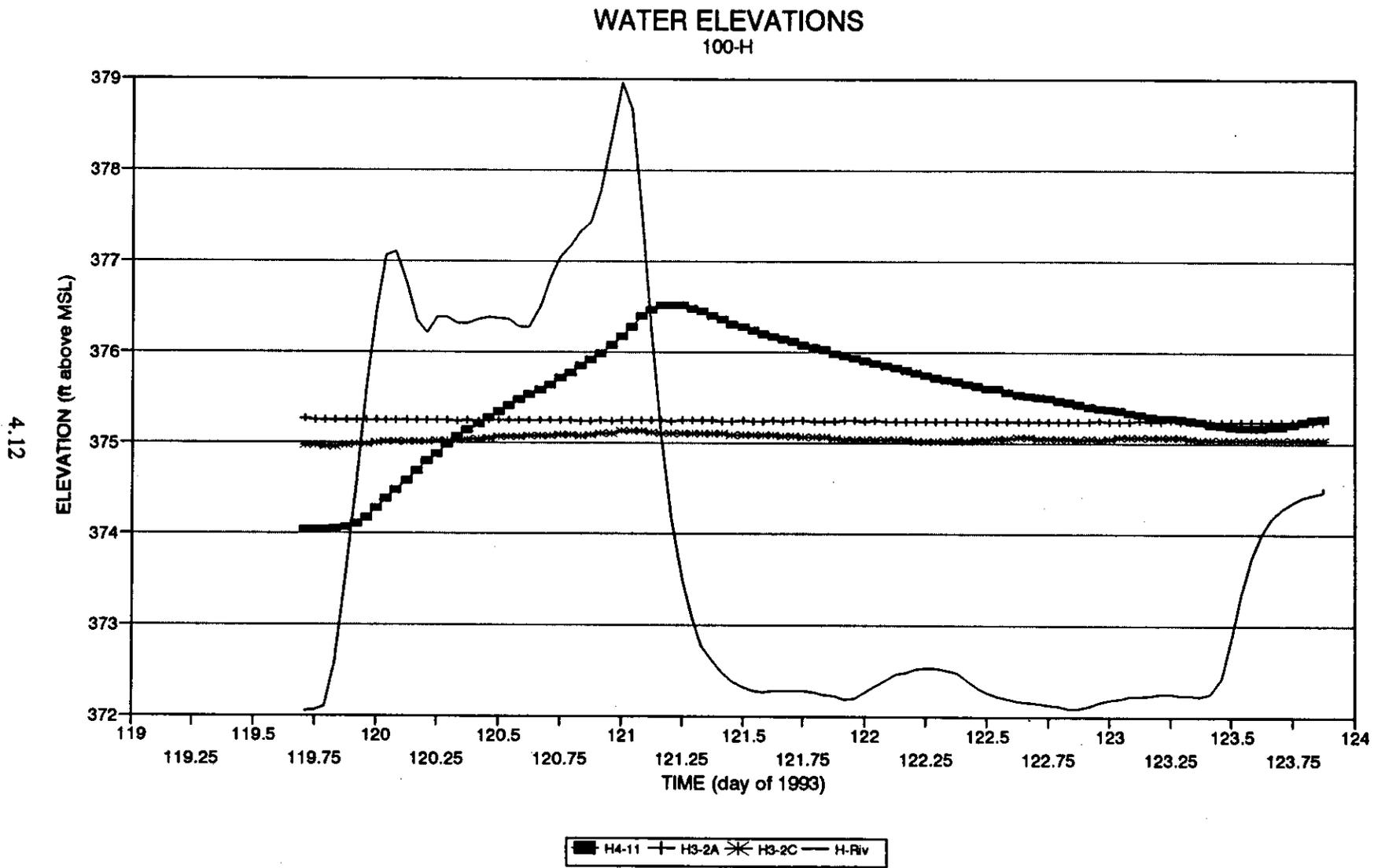


Figure 11. Detailed Variations in Water Elevations in 100-H Area

4.13

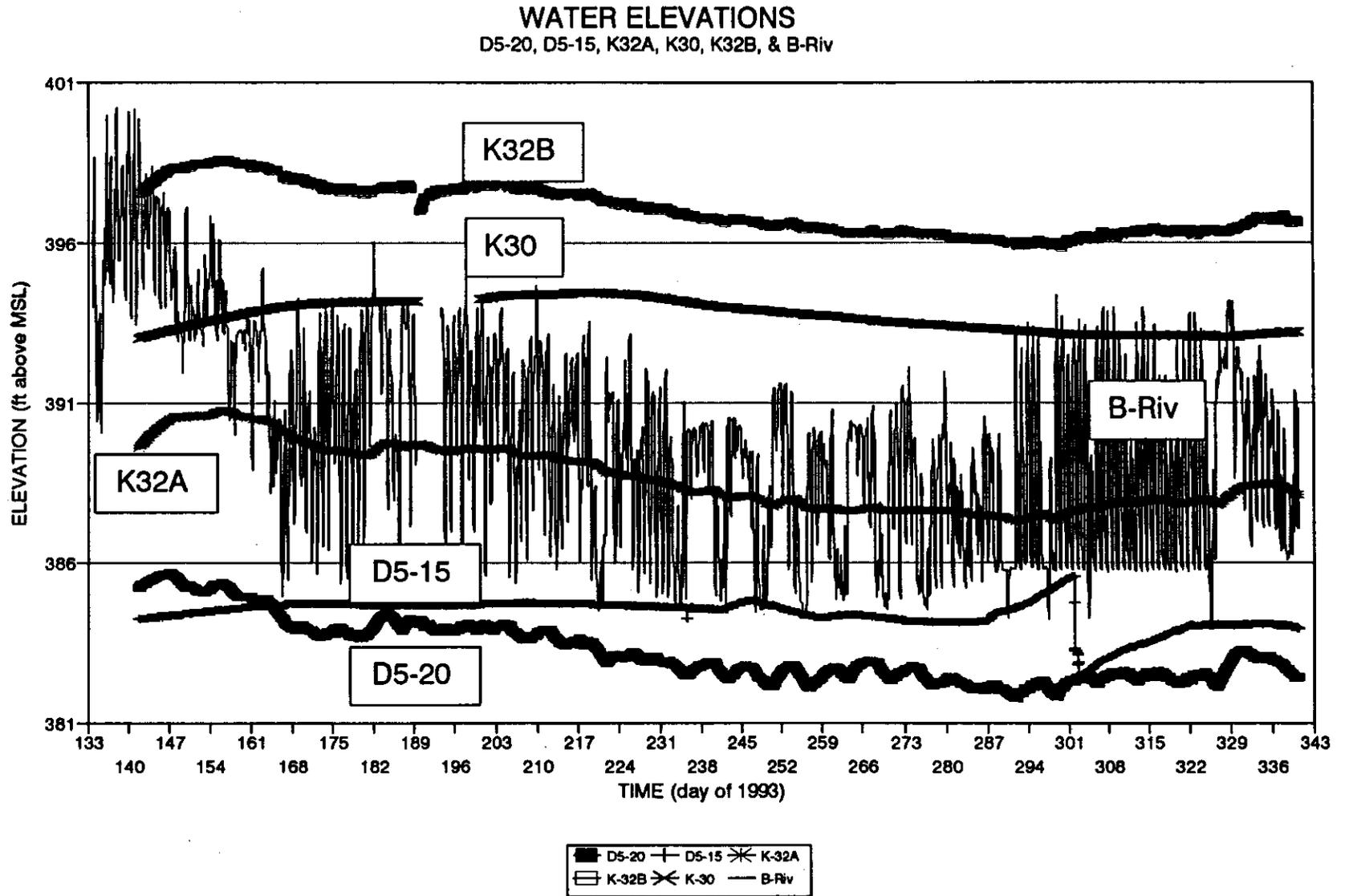


Figure 12. Water Elevations in 100-D and 100-K Wells and The 100-B River

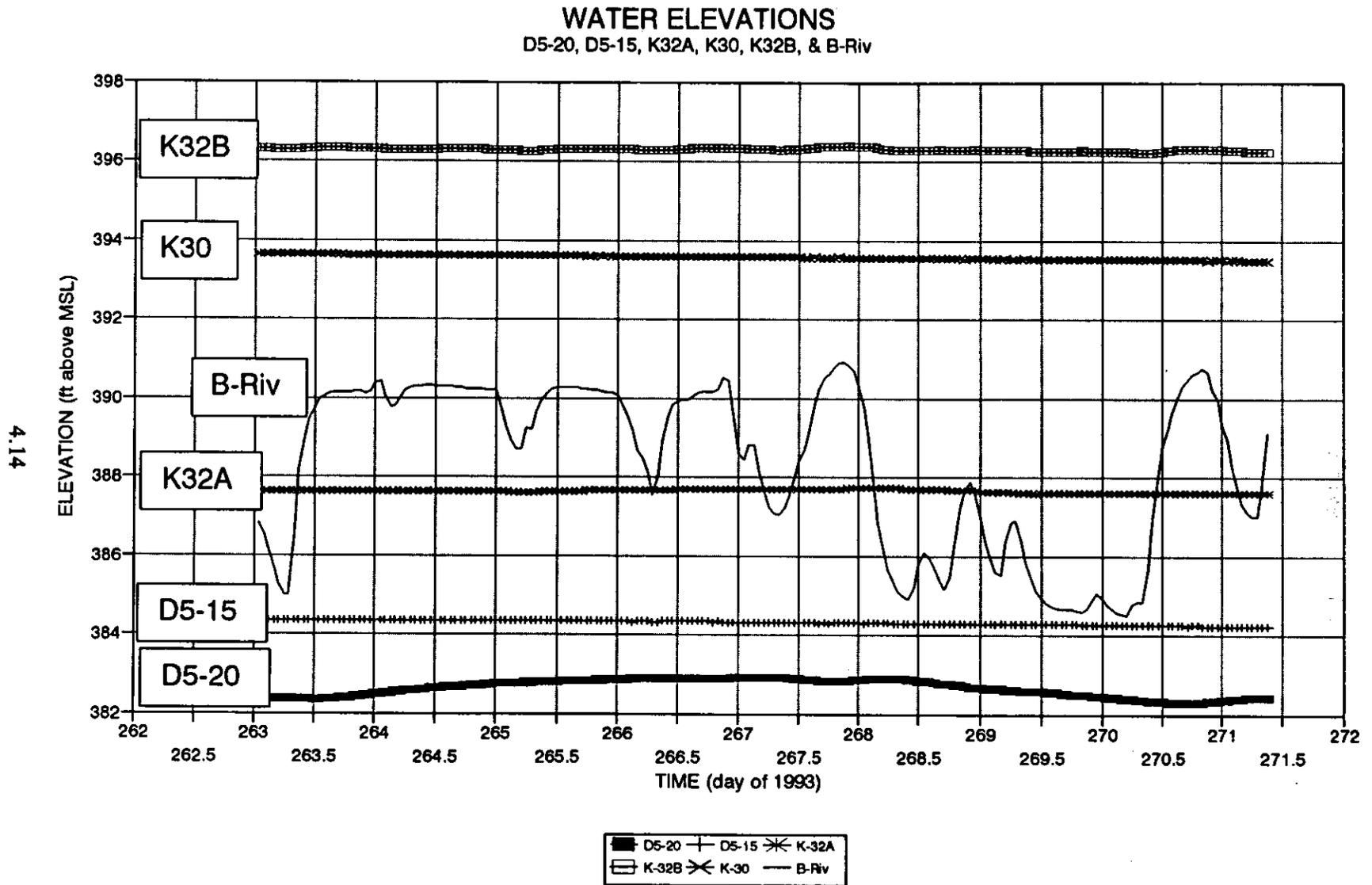


Figure 13. Detailed Variations of 100-D and 100-K Wells and The 100-B River

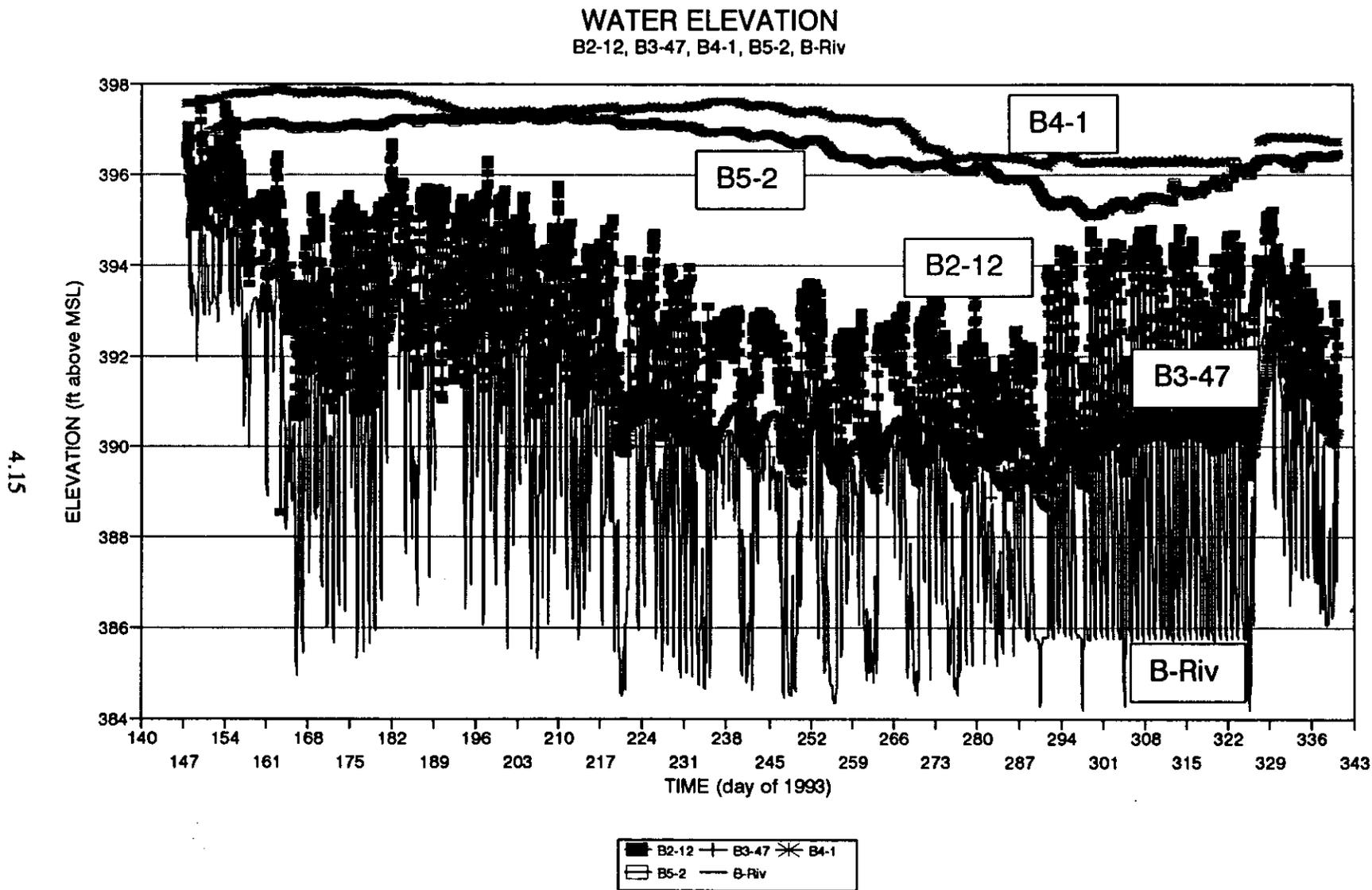


Figure 14. Water Elevations at 100-B Area

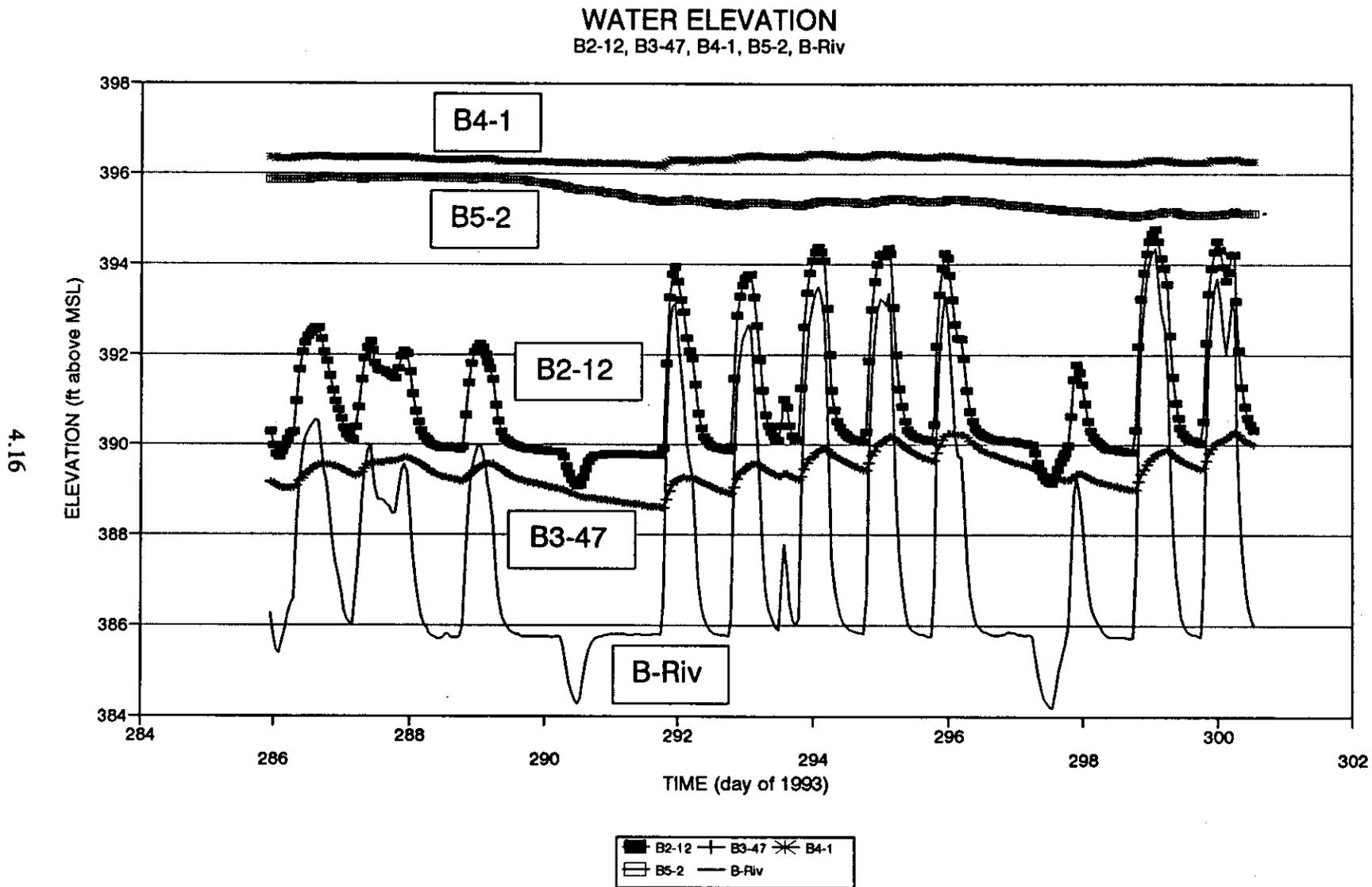


Figure 15. Detailed Variations in Water Elevations in 100-B Area

aquifer channel. This close-couple status is apparent from the detail with which the river level is duplicated in well B2-12. Wells B4-1 and B5-2 are distant from the river and are expected to have slow response, with B4-1 being the more distant.

Electrical conductivity (EC) was measured in the 100-H Area by sensors located in the river, well H4-11, and two nearby river-bank seeps, S-152-2 and S-153-1. Figure 16 shows well H4-11 EC as relatively constant at 0.35 mS. The river EC is even more constant at about 0.1 mS. While neither of these values is temperature compensated during the interval shown, their relative magnitude remains unaltered after compensation. Temperature compensation and individual calibration followed this interval when the transducer had to be replaced because a porcupine destroyed it. The EC at seep S-153-1 varied from the river value up toward the well value when the river flow dropped below the elevation of the seep, only to decline again as the river water covered the transducer. Just after day 180, the transducer reading dropped to zero for several hours. The same phenomenon occurred on day 184 and again about day 186. This drop to zero was caused by a reduction in bank storage and failure of the seep to yield drainage water. It is likely that the seep EC never would rise to the level of well H4-11 because bank storage represents a zone of river intrusion and influence. The evidence for this conclusion is shown at about day 172, where the river is not directly influencing the conductivity of the seep and yet the seep EC does not rise. On the other hand, well H4-11 clearly shows the influence of intruding river water, especially when the river level fluctuates strongly above the 375-ft elevation.

Figure 17 shows temperature compensated EC for the stations displayed in Figure 16 and for seep S-152-2 at the outfall. Here, the seep EC does exceed that of well H4-11 for a short interval when the river drops below the 375-ft elevation. Again, seep S-153-1 ran low on water when the river dropped below the 375-ft elevation. At no time did seep S-152-2 appear dry. Instead, it seeped up through the cracks in the concrete outfall apron and formed a significant stream that flowed off the apron and into the river.

Figure 18 shows some water temperatures measured by the EC probes. The large fluctuations near day 182 resulted from drying of the seep, leaving the transducer exposed to the atmosphere. The low temperatures shown near day 325 also represent periods of transducer exposure to air because of seep dry-down. The temperature in well H4-11 remained nearly constant near 20°C, while the river varied from about 4 to 22°C. With these relative temperatures, river water would be expected to intrude beneath the groundwater during cold periods and over the top during warm periods. It would be useful to find a long, screened section of well near the river where EC could be measured to distinguish river water intrusion level.

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### WATER ELECTRICAL CONDUCTIVITY 100-H WELLS AND RIVER

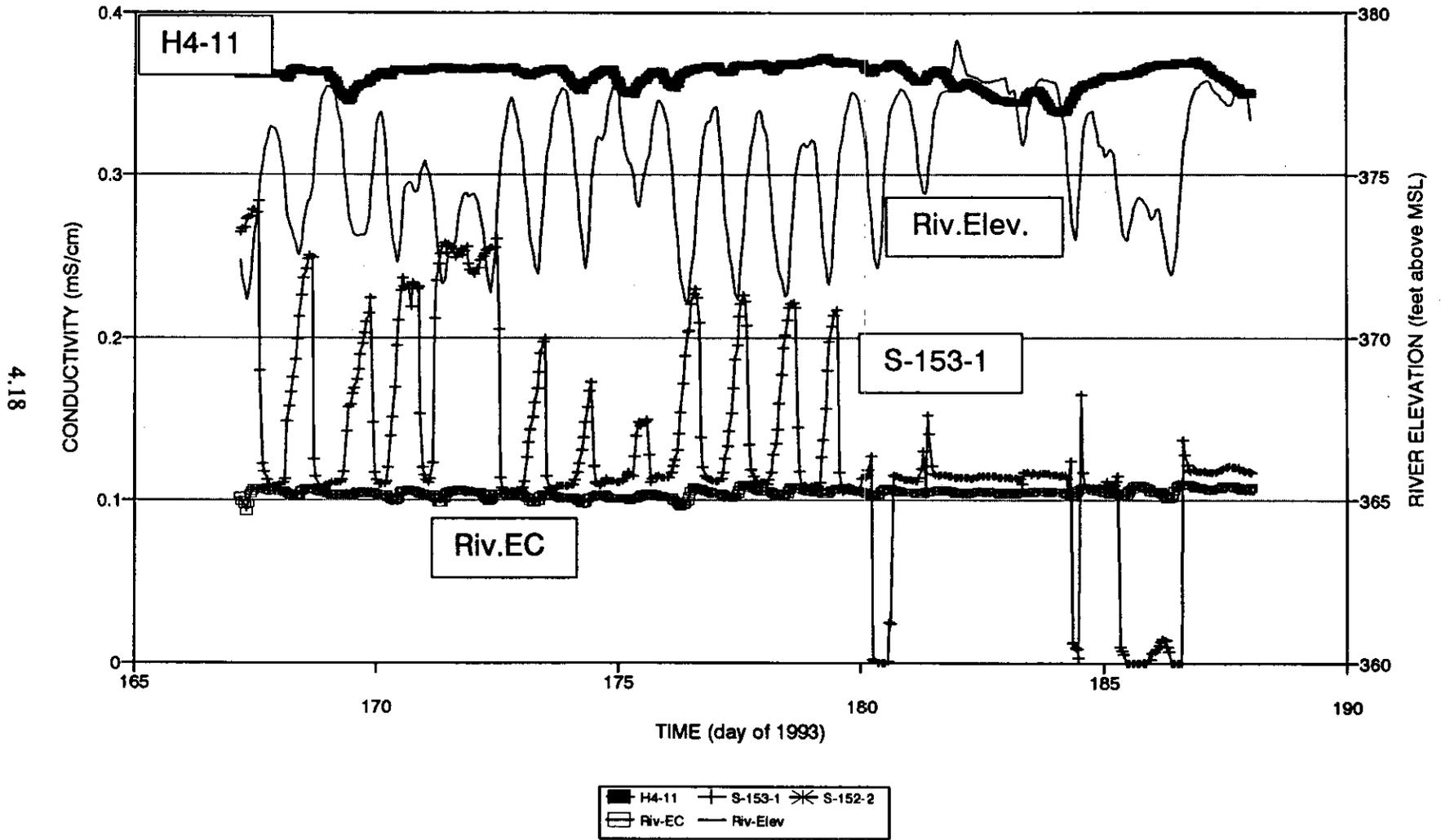


Figure 16. Electrical Conductivity of 100-H Seeps, Well, and River

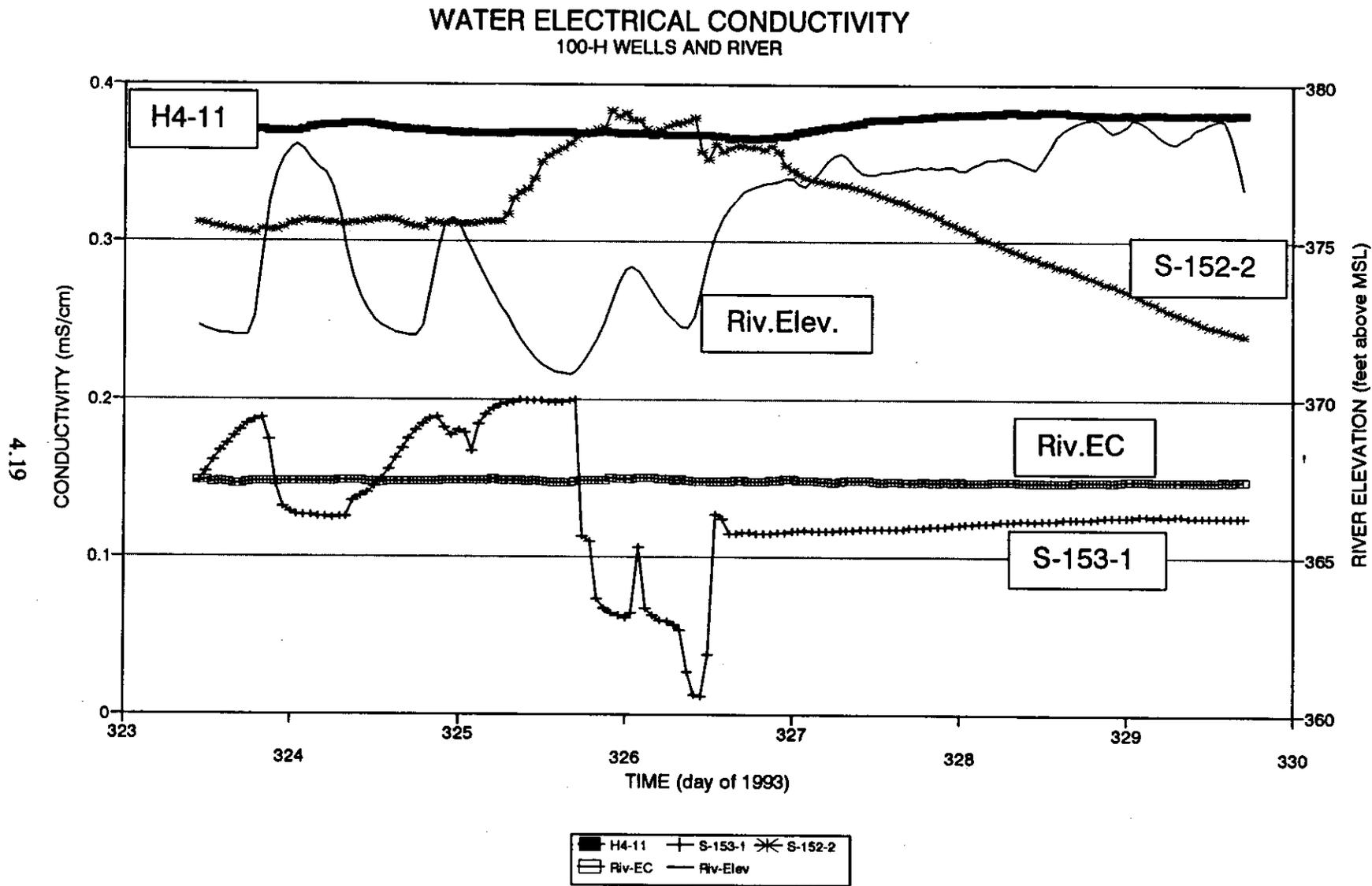


Figure 17. Detailed Variation of Electrical Conductivity at 100-H Area

### WATER TEMPERATURES 100-H

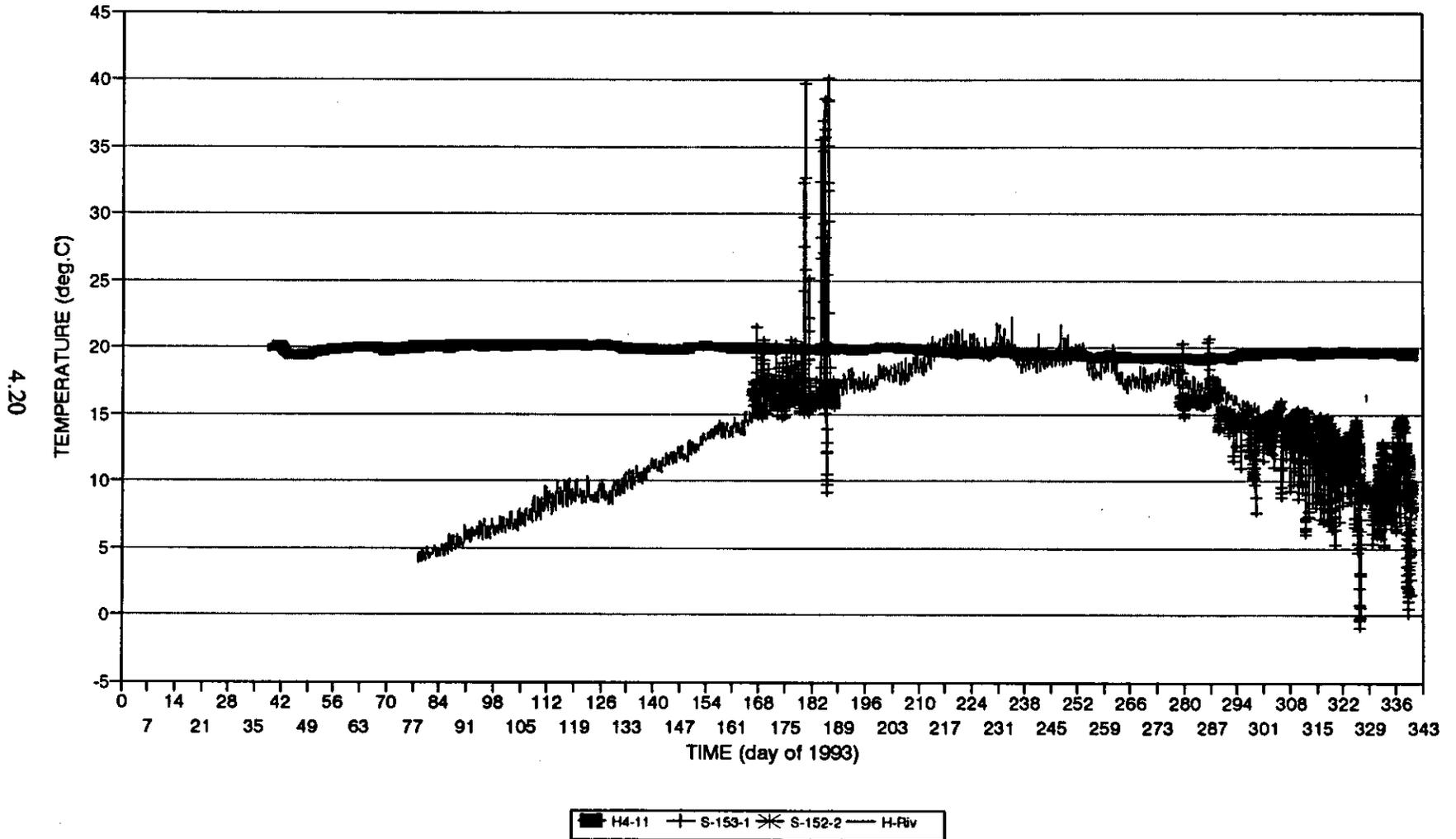


Figure 18. Thermal Variations of River and Groundwater at 100-H Area

## 4.2 Conclusions

Emphasis and equipment shifted from the 300-FF-5 Operable Unit to the 100 Aggregate Area Operable Unit during spring 1993. Monitors removed from the 300 Area were installed in 100-D, -N, and -K Areas and added to the number in the -F, -H, and -B Areas. Eleven wells and one river station are still monitored in the 300-FF-5 boundary while the others were spread about evenly among the 100 Areas. The monitor network currently consists of 44 radiotransceivers and 42 automatic dataloggers, with one station in each area, except 100-N, serving two wells.

Electrical conductivity and temperature, measured at well, seep, and river locations, showed the influence of intruding river water in both seep and well water. Measurement frequency remained at 1-hr intervals.

Elevation accuracy is believed to be within  $\pm 0.1$  ft. Topographic surveys, instrument calibrations, and steel tape measurements all contribute error. Short-term network precision appeared to be within  $\pm 0.02$  ft. Steel tape measurements were read within  $\pm 0.01$  ft. Survey error varied with distance from the reference, but was probably less than  $\pm 0.07$  ft. Periodic tape and datalogger tests helped ensure precision and accuracy by including the entire measurement system in the tests. Accuracy of survey errors or ground shift approached 0.5 ft at SWS-1 and 100-H river stations.

Examples of conductivity, temperature, and water levels were presented for each area monitored. River water levels at all five river stations were shown to fluctuate together, with a phase shift and amplitude change to adjust for river mile and channel cross section. Only in the 300 Area was the river amplitude attenuated significantly because of the McNary Dam forebay. Ice Harbor influence on the water level in the 300 Area is apparent when water elevations drop to 340 ft above MSL.

Some equipment problems were reported, such as transducer drift and battery discharge. Transducer drift was resolved by replacement or compensated by periodic manual measurements using steel tape coupled with datalogger readings. Questionable data were tested by comparison with similar stations. For example, 100-H and 100-F river stations were compared by subtracting the mean and dividing by the standard deviation. This normalized the data about a common zero. It did not correct for data divergence due to time lag. Where data drift was apparent, linear adjustment was used from the last known correct point to the measured divergent point. Long-term drift of transducers was accommodated in this manner. Key factors in data reliability were in situ calibration of pressure transducers, periodic steel tape and datalogger paired readings, difference tests of data, and visual data checking. Solar radiation at Hanford was inadequate to recharge batteries during November, December, and January. Experience demonstrated the necessity to use batteries with at least 40-Ah capacity to operate the network remote stations reliably during this period.

Water levels, temperatures, and electrical conductivity measured by the automatic monitor network provide an initial database with which to calibrate models and from which to infer ground and river water interactions for site characterization and remediation activities.

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## 5.0 Bibliography

Campbell, M. D., R. Schalla, and D. R. Newcomer. 1991. *Accuracy and Cost Effectiveness of Manual and Automated Water-Level Monitoring Technology*. PNL-7566, Pacific Northwest Laboratory, Richland, Washington.

Campbell, M. D., and D. R. Newcomer. 1992. *Automatic Measurement of Water Levels Within the 300-FF-5 Boundary*. PNL-7874, Pacific Northwest Laboratory, Richland, Washington.

EPA (U.S. Environmental Protection Agency). 1986. *Resource Conservation and Recovery Act (RCRA) Ground-Water Monitoring Technical Enforcement Guidance Document*. OSWER-9950.1, Washington, D.C.

Ferris, J. G. 1952. *Cyclic Fluctuations of Water Level as a Basis for Determining Aquifer Transmissibility*. United States Department of the Interior, Geologic Survey, Water Resources Division, Ground Water Branch, Ground-Water Hydraulics Section, Washington, D.C. Contribution No. 1, April 1952.

Lindberg, J. W., and F. W. Bond. 1979. *Geohydrology and Ground-Water Quality Beneath the 300 Area, Hanford Site, Washington*. PNL-2949, Pacific Northwest Laboratory, Richland, Washington.

McMahon, W. J., and R. E. Peterson. 1992. *Estimating Aquifer Hydraulic Properties Using the Ferris Method, Hanford Site, Washington*. DOE/RL-92-64, Rev. 0, Westinghouse Hanford Company, Richland, Washington.

Runchal, A. K., and B. Sagar. 1989. *PORFLO-3: A Mathematical Model for Fluid Flow, Heat, and Mass Transport in Variably Saturated Geologic Media*. WHC-EP-0041, Westinghouse Hanford Company, Richland, Washington.

Schalla, R., R. W. Wallace, R. L. Aaberg, S. P. Airhart, D. J. Bates, J. V. M. Carlile, C. S. Cline, D. I. Dennison, M. D. Freshley, P. R. Heller, E. J. Jensen, K. B. Olsen, R. G. Parkhurst, J. T. Rieger, and E. J. Westergard. 1988. *Interim Characterization Report for the 300 Area Process Trenches*. PNL-6716, Pacific Northwest Laboratory, Richland, Washington.

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## **Appendix A**

### **Datalogger Programs**

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# Appendix A

## Datalogger Programs

Several datalogger programs were used to gather the required data. Each program combination is shown separately for reference. All programs begin with instructions to measure battery voltage and store it for display. Also, an instruction is included to measure with high resolution.

The widest use was made of the program to measure pressure. This program appears first. The second program adds thermocouple temperature to pressure. The third program replaces thermocouple temperature with a combination of solution electrical conductivity (EC) and temperature. The fourth program is for EC and temperature.

9416273-1243

Pressure Measurement Only

Program:

\* 1 Table 1 Programs  
01: 3600 Sec. Execution Interval

01: P78 Resolution  
01: 1 High Resolution

02: P10 Battery Voltage  
01: 5 Loc :

03: P9 Full BR w/Compensation  
01: 1 Rep  
02: 25 2500 mV 60 Hz rejection EX Range  
03: 24 250 mV 60 Hz rejection BR Range  
04: 1 IN Chan  
05: 1 Excite all reps w/EXchan 1  
06: 2500 mV Excitation  
07: 1 Loc :  
08: 1 Mult  
09: 0 Offset

04: P86 Do  
01: 10 Set high Flag 0 (output)

05: P77 Real Time  
01: 110 Day,Hour-Minute

06: P70 Sample  
01: 1 Repts  
02: 1 Loc

07: P End Table 1

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412 427116

Pressure and Thermocouple Temperature Measurement

Program: mc112

\* 1 Table 1 Programs  
01: 3600 Sec. Execution Interval

01: P10 Battery Voltage  
01: 5 Loc :

02: P78 Resolution  
01: 1 High Resolution

03: P9 Full BR w/Compensation  
01: 1 Rep  
02: 25 2500 mV 60 Hz rejection EX Range  
03: 24 250 mV 60 Hz rejection BR Range  
04: 1 IN Chan  
05: 1 Excite all reps w/EXchan 1  
06: 2500 mV Excitation  
07: 1 Loc :  
08: 1 Mult  
09: 0 Offset

04: P86 Do  
01: 10 Set high Flag 0 (output)

05: P77 Real Time  
01: 110 Day,Hour-Minute

06: P70 Sample  
01: 1 Repts  
02: 1 Loc

07: P17 Module Temperature  
01: 2 Loc :

08: P14 Thermocouple Temp (DIFF)  
01: 1 Rep  
02: 21 2.5 mV 60 Hz rejection Range  
03: 3 IN Chan  
04: 1 Type T (Copper-Constantan)  
05: 2 Ref Temp Loc  
06: 3 Loc :  
07: 1.8 Mult  
08: 32 Offset

09: P86 Do  
01: 10 Set high Flag 0 (output)

10: P70 Sample  
01: 1 Repts  
02: 3 Loc

11: P End Table 1

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Pressure, Electrical Conductivity, and Temperature Measurement

Program: mc125

\* 1 Table 1 Programs  
01: 3600 Sec. Execution Interval

01: P10 Battery Voltage  
01: 5 Loc :

02: P78 Resolution  
01: 1 High Resolution

03: P9 Full BR w/Compensation  
01: 1 Rep  
02: 25 2500 mV 60 Hz rejection EX Range  
03: 24 250 mV 60 Hz rejection BR Range  
04: 1 IN Chan  
05: 1 Excite all reps w/EXchan 1  
06: 1000 mV Excitation  
07: 1 Loc :  
08: 1 Mult  
09: 0 Offset

04: P86 Do  
01: 10 Set high Flag 0 (output)

05: P77 Real Time  
01: 110 Day,Hour-Minute

06: P70 Sample  
01: 1 Repts  
02: 1 Loc

07: P5 AC Half Bridge  
01: 1 Rep  
02: 15 2500 mV fast Range  
03: 11 IN Chan  
04: 2 Excite all reps w/EXchan 2  
05: 2500 mV Excitation  
06: 6 Loc :  
07: 1 Mult  
08: 0 Offset

08: P59 BR Transform  $R_f[X/(1-X)]$   
01: 1 Rep  
02: 6 Loc :  
03: .7042 Multiplier (Rf)

09: P42  $Z=1/X$   
01: 6 X Loc  
02: 6 Z Loc :

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Pressure, Electrical Conductivity, and Temperature Measurement (contd)

Page 2 Table 1

10: P11 Temp 107 Probe  
01: 1 Rep  
02: 12 IN Chan  
03: 3 Excite all reps w/EXchan 3  
04: 7 Loc :  
05: 1 Mult  
06: 0 Offset

11: P34 Z=X+F  
01: 7 X Loc  
02: -25 F  
03: 8 Z Loc :

12: P37 Z=X\*F  
01: 8 X Loc  
02: .01 F  
03: 8 Z Loc :

13: P55 Polynomial  
01: 1 Rep  
02: 8 X Loc  
03: 9 F(X) Loc :  
04: 1 C0  
05: -2.021 C1  
06: 4.0445 C2  
07: -6.3483 C3  
08: 0 C4  
09: 0 C5

14: P36 Z=X\*Y  
01: 6 X Loc  
02: 9 Y Loc  
03: 10 Z Loc :

15: P86 Do  
01: 10 Set high Flag 0 (output)

16: P70 Sample  
01: 1 Repls  
02: 10 Loc

17: P70 Sample  
01: 1 Repls  
02: 7 Loc

18: P End Table 1

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Electrical Conductivity and Temperature Measurements Only

Program: mc139

\* 1 Table 1 Programs  
01: 3600 Sec. Execution Interval

01: P10 Battery Voltage  
01: 5 Loc :

02: P78 Resolution  
01: 1 High Resolution

03: P5 AC Half Bridge  
01: 1 Rep  
02: 15 2500 mV fast Range  
03: 11 IN Chan  
04: 2 Excite all reps w/EXchan 2  
05: 2500 mV Excitation  
06: 6 Loc :  
07: 1 Mult  
08: 0 Offset

04: P59 BR Transform  $Rf[X/(1-X)]$   
01: 1 Rep  
02: 6 Loc :  
03: .7148 Multiplier (Rf)

05: P42  $Z=1/X$   
01: 6 X Loc  
02: 6 Z Loc :

06: P11 Temp 107 Probe  
01: 1 Rep  
02: 12 IN Chan  
03: 3 Excite all reps w/EXchan 3  
04: 7 Loc :  
05: 1 Mult  
06: 0 Offset

07: P34  $Z=X+F$   
01: 7 X Loc  
02: -25 F  
03: 8 Z Loc :

08: P37  $Z=X*F$   
01: 8 X Loc  
02: .01 F  
03: 8 Z Loc :

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Electrical Conductivity and Temperature Measurements Only (contd)

Page 2 Table 1

09: P55 Polynomial  
01: 1 Rep  
02: 8 X Loc  
03: 9 F(X) Loc :  
04: 1 C0  
05: -2.021 C1  
06: 4.0445 C2  
07: -6.3483 C3  
08: 0 C4  
09: 0 C5

10: P36 Z=X\*Y  
01: 6 X Loc  
02: 9 Y Loc  
03: 10 Z Loc :

11: P86 Do  
01: 10 Set high Flag 0 (output)

12: P77 Real Time  
01: 110 Day,Hour-Minute

13: P70 Sample  
01: 1 Repls  
02: 10 Loc

14: P70 Sample  
01: 1 Repls  
02: 7 Loc

15: P End Table 1

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## **Appendix B**

### **Steel Tape and Datalogger Paired Sets**

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## Appendix B

### Steel Tape and Datalogger Paired Sets

Appendix B shows steel tape and datalogger paired sets that were used as data quality checks on the monitor system. Data from the initial sets in 1991 through December 1993 are included.

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Tape and Datalogger Reading Pairs (contd)

Weld/Dr	Time	Sr.Type	DLRdg	Am.Ch	Weld/Dr	Time	Sr.Tr	DLRdg	Am.Ch	Weld/Dr	Time	Sr.Type	DLRdg	Am.Ch
1-108					1-188					2-2				
1-24-92	1351	32.97	5.2823	0.11	7-23-91	1110	44.03	4.8157	0.00	8-18-92	1145	36.35	4.9639	0.00
2-5-92	1219	33.70	4.5786	0.04	8-15-91	908	43.87	4.9892	-0.00	8-6-92	746	36.41	5.0153	-0.11
3-5-92	1310	33.35	4.9036	0.03	8-22-91	1058	44.94	3.8226	0.01	11-16-93	817	36.24	5.2066	-0.11
4-4-92	811	32.95	5.4234	-0.00	9-5-91	727	45.70	3.0024	0.02	12-8-92	925	34.5	7.5153	-0.13
6-3-92*	756	31.94	6.5104	0.00	11-15-91**	46.00	46.00	3.6289	-0.01	1-7-93	904	33.46	8.2109	-0.13
7-2-92	728	31.67	6.815	-0.01	12-5-91	1500	46.54	3.0378	0.01	2-9-93	835	36.35	5.1672	-0.19
8-1-92*	716	32.17	6.2674	-0.00	1-9-92	1535	45.54	4.1063	0.01	3-9-93	826	36.97	4.28	0.02
9-8-92	733	43.73	4.4183	-0.04	2-5-92	1012	46.57	3.0259	-0.01					
10-8-92	1236	34.09	4.1024	0.09	3-5-92	1251	46.44	3.1473	0.00	3A				
11-16-9	805	34.11	4.4021	0.07	4-8-92	835	46.41	3.164	-0.01	1-8-92	1524	28.52	4.6721	-0.63
12-8-92	836	33.61	4.6649	0.05	5-5-92	1141	46.01	3.6125	0.00	2-5-92	1059	30.59	3.5262	-0.63
1-7-93	933	31.72	6.7429	0.00	6-2-92	1014	43.17	4.5192	-0.00	3-5-92	1248	30.41	3.7111	-0.62
2-9-93	903	33.99	7.6954	-0.00	6-30-92	1020	44.32	5.2291	-0.03	4-8-92	820	28.89	3.0946	0.07
3-9-93	837	34.79	4.2441	0.05	8-4-92	1027	46.69	2.9184	-0.03	5-5-92	1131	28.89	3.6001	0.00
				0.05	9-8-92*	627	47.26	2.283	-0.01	6-2-92	1025	28.00	4.5552	0.00
					10-8-92	841	47.27	2.3301	-0.07	6-30-92	1029	28.46	5.1709	-0.03
					11-16-9	927	47.23	2.6176	-0.29	8-6-92	1015	30.61	3.0287	-0.19
1-108					1-18-92	1031	45.7	4.1919	-0.23	9-8-92*	620	31.12	2.5745	-0.28
7-23-91	1037	36.80	6.7317	-0.06	12-8-92	1112	41.70	4.2031	0.02	8-15-91	1028	43.07	6.2603	0.00
8-15-91	1003	36.57	7.1367	-0.18	1-7-93	1003	45.12	4.7982	-0.17	8-22-91	1217	44.80	4.2962	0.00
8-22-91	1146	38.11	5.3128	-0.03	2-9-93	945	47.02	2.715	-0.17	8-18-92	832	31.19	2.5521	-0.31
9-5-91	743	38.63	4.7563	-0.03	3-9-93	912	47.5	2.1773	-0.15	11-16-9	918	31.02	2.7419	-0.33
12-5-91	1520	36.35	3.9832	2.97						12-8-92	1019	28.46	4.4322	-0.36
1-8-92	1506	37.87	5.5572	-0.02	1-18-92					2-9-93	935	28.82	3.1562	-0.38
2-5-92	1030	39.28	3.9364	-0.02	1-18-92					3-9-93	906	30.95	2.8425	-0.36
3-5-92	1442	39.07	4.2565	-0.01	7-23-91	1112	41.70	4.2031	0.02					
4-4-92	917	38.9	4.4339	0.00	8-22-91	1100	42.49	1.7859	0.03					
5-6-92	827	37.98	5.4168	0.01	8-15-91	909	42.49	2.9275	0.03					
6-5-92	750	37.58	5.8618	-0.01	11-18-91**	43.61	2.112	Adj.						
7-2-92	730	37.81	5.6138	0.01	12-5-91	1506	47.00	1.6866	-1.19	8-5-91	756	45.20	3.8632	0.01
8-1-92	705	39.45	3.6826	0.15	1-8-92	1535	43.08	2.6649	-0.18	12-8-91	1011	46.31	3.1102	-0.31
10-8-92	731	39.86	3.3976	0.00	2-5-92	1251	43.97	1.5547	0.02	3-5-92	1421	44.33	4.8762	0.03
11-16-9	810	39.73	3.5833	-0.04	4-8-92	835	43.98	1.4669	-0.04	3-6-92	1125	46.46	3.4672	0.02
12-8-92	918	37.73	5.7082	-0.02	5-5-92	1141	44.03	1.8579	0.00	4-8-92	950	46.25	3.7143	-0.29
1-7-93	856	36.92	6.5691	-0.01	6-2-92	1014	42.79	2.7937	-0.01	5-5-92	1238	45.69	4.6332	0.00
2-9-93	827	39.8	3.4723	-0.01	6-30-92	1020	42.26	3.3622	-0.03	6-2-92	1219	43.65	5.0023	0.00
3-9-93	821	40.46	2.7988	-0.00	8-6-92	1027	44.87	0.5457	0.00	6-30-92	1155	44.91	3.5863	-0.38
4-6-93	729	40.43	2.7952	-0.01	9-8-92	627	44.87	0.5457	0.00	8-6-92	850	47.38	2.6510	0.04
5-6-93	727	40.01	3.2263	0.00	10-8-92	841	44.88	0.6109	-0.07	8-6-92	756	46.95	2.9204	0.04
7-9-93	725	37.69	5.7689	-0.03	11-16-9	927	44.85	0.8827	-0.29	9-8-92	1208	47.28	2.4657	0.04
8-2-93	708	39.29	3.8564	0.05	1-7-93	1003	42.83	1.5752	-0.28	10-8-92	1320	47.28	2.295	0.20
10-15-93	712	41.19	2.0574	0.00	2-9-93	945	44.58	1.6392	-0.73	11-16-9	1122	46.96	2.6900	0.43
11-15-93	1511	39.44	3.9097	-0.05	3-9-93	912	44.97	1.1142	-0.63	1-7-93	1131	44.22	5.5835	0.31
12-22-93	1129	38.78	4.7638	-0.19	2-1					2-10-93	806	47.16	2.1974	0.50
					1-28-92	1000	33.41	5.0283	0.07	3-9-93	944	47.74	1.5149	0.56
1-16C					2-5-92	1145	33.78	4.6186	0.08	3-12				
9-28-93*	1230	8.82	6.2864	0.00	4-8-92	1413	33.52	4.9822	0.02	2-15-92	1200	46.82	4.8204	0.05
10-15-93	712	8.44	6.7337	-0.05	5-8-92	749	33.27	5.2568	0.00	2-6-92	1130	46.52	4.9893	0.03
11-15-93	1511	8.69	6.4924	-0.06	6-4-92	742	33.22	6.2786	0.00	4-8-92	940	46.2	5.1354	0.02
12-22-93	1129	8.25	6.929	-0.03	6-2-92*	704	31.94	6.7143	-0.03	5-5-92	1247	45.64	5.7568	0.00
					7-2-94	728	32.27	4.2827	1.91	6-2-92	1226	44.97	6.3741	0.00
1-18A					7-8-92	1255	34.48	1.9634	0.48	6-30-92	1203	44.51	3.7228	-0.00
7-23-91	1103	45.23	5.9405	-0.05	8-7-92	745	33.95	1.0511	0.00	8-6-92	749	46.82	4.6507	0.03
8-15-91	905	44.97	6.2738	-0.10	9-8-92	810	34.35	2.6855	-0.01	9-8-92	1214	47.24	3.7728	0.18
8-22-91	1055	46.03	5.0414	-0.01	10-8-92	813	34.19	2.8055	-0.06	10-8-92	1227	47.15	3.9409	0.19
9-5-91	726	46.90	4.1335	-0.04	11-16-9	908	33.91	1.3632	-0.25	11-16-9	1130	46.97	4.1463	0.17
12-5-91	1504	47.65	3.2359	-0.03	12-8-92	952	32	5.6197	-0.44	12-8-92	1023	44.48	4.9706	1.46
1-8-92	1535	46.68	4.3624	-0.03	1-7-93	933	31.14	6.7382	-0.62	1-7-93	1124	44.48	5.026	1.84
2-5-92	1012	47.68	3.2686	-0.01	2-9-93	911	34.07	3.633	-0.66	2-10-93	813	47.06	1.9745	2.10
3-5-92	1251	47.57	3.3714	0.00	3-9-93	844	34.81	2.9014	-0.72	3-9-93	948	47.59	1.6603	1.91
4-8-92	835	47.59	3.3406	0.01	4-6-93	742	34.69	3.1085	-0.79					
5-5-92	1141	47.15	3.8226	0.00	5-6-93	745	32.27	5.7951	-0.87					
6-2-92	1014	48.3	4.7426	-0.01	6-8-93	745	32.27	5.7951	-0.87					
6-30-92	1020	45.51	5.5982	-0.01	7-9-93	816	32.63	5.4005	-0.86					
8-6-92	1027	47.72	3.2265	-0.02	8-2-93	729	33.4	4.1147	-0.44					
9-8-92	627	48.43	2.4699	-0.02	9-14-93	906	35.03	2.7857	-0.63					
10-8-92	841	48.4	2.6904	-0.01	10-15-93	644	35.47	2.3498	-0.87					
11-16-9	927	48.41	2.4393	0.03	11-19-93	1429	33.75	4.2156	-0.88					
12-8-92	1031	46.86	3.9787	0.14	12-21-93	1527	35.48	4.5544	-0.93					
1-7-93	1003	46.28	4.5366	0.21	10-15-93	644	35.47	2.3498	-0.87					
2-9-93	945	48.17	2.3999	0.20	11-19-93	1429	33.75	4.2156	-0.88					
3-9-93	912	48.61	1.7931	0.43	12-21-93	1527	35.48	4.5544	-0.93					



Tape and Datalogger Reading Pairs (contd)

Wd/Da	Time	St:Type	D:L:Rd	A:M:Ct	Wd/Da	Time	St:Type	D:L:Rd	A:M:Ct	Wd/Da	Time	St:Type	D:L:Rd	A:M:Ct	Wd/Da	Time	St:Type	D:L:Rd	A:M:Ct
6-13-92	808	53.91	4.8994	0.00	12-5-91	1200	6.24	3.8467	0.16	11-19-92	926	26.74	2.4189	0.00	6-4-93	1340	25.38	8.8833	0.18
8-8-92	605	54.55	4.2034	-0.03	2-5-92	1332	5.76	4.5725	0.01	12-8-92	1148	6.10	7.3216	-0.15	7-8-93	1338	27.48	6.8209	0.00
10-8-92	634	54.41	4.4125	-0.05	3-5-92	1508	5.34	4.7808	-0.01	1-6-93	1357	11.94	7.3372	-1.58	12-5-92	1223	27.93	6.3299	0.00
11-10-92	1138	54.3	4.5452	-0.06	4-7-92	1027	5.90	4.3735	0.01	2-8-93	1150	29.58	2.3657	-0.04	8-2-93	1207	28.65	5.5342	0.02
12-8-92	940	52.53	6.4519	-0.06	5-5-92	1347	5.76	4.5385	0.00	3-8-93	1116	32.57	0.9163	0.21	9-16-93	833	30.82	4.2628	0.04
1-7-93	1146	52.13	6.8838	-0.07	6-2-92	959	6.53	3.709	0.00	4-6-93	844	33.04	0.9683	-0.00	11-18-93	1315	33.57	0.8604	-0.02
2-10-93	739	54.24	4.6183	-0.07	6-30-92	1001	6.46	3.7637	0.04	5-6-93	1046	24.64	3.0769	-0.18	12-21-93	1409	14.63	5.5065	-0.30
3-8-93	749	54.64	4.1751	-0.06	8-4-92	858	6.38	3.8248	0.04	7-14-93	1410	20.35	3.6641	-0.07	6-4-93	1340	25.38	8.8833	0.18
					9-8-92	717	7.16	2.9691	0.06	8-2-93	1310	26.76	2.5189	-0.11	7-4-93	1338	27.48	6.8209	0.00
6-1					10-14-93	824	27.18	2.5009	0.04	9-16-93	824	27.18	2.5009	-0.19	12-8-92	1148	6.10	7.3216	-0.15
1-28-92	1412	46.24	5.826	0.13	11-1-92	1017	6.55	3.6445	0.00	10-14-93	1325	23.94	3.2476	-0.19	8-2-93	1207	28.65	5.5342	0.02
2-5-92	46.61	5.5082	0.06	13-8-92	1120	5.97	4.2842	0.03	11-18-93	1515	33.57	0.8604	-0.02	9-16-93	833	30.82	4.2628	0.04	
3-5-92	1541	46.65	5.5016	0.02	1-7-93	1027	5.69	4.5782	0.00	12-21-93	1409	14.63	5.5065	-0.30	11-18-93	1315	33.57	0.8604	-0.02
4-7-92	1043	47	5.386	-0.03	2-10-93	840	5.49	4.7897	0.04										
5-5-92	1323	46.17	6.0429	0.00	3-8-93	1030	5.52	4.787	0.01	FI-2									
6-2-92	1151	45.24	7.0736	-0.03						FI-1									
6-30-92	1130	44.3	5.5028	0.00	84 (528-E12)	1600	45.31	3.4644	-0.05	9-12-91	1415	36.00	no DL	0.00	12-8-92	1156	35.85	2.512	0.01
8-4-92	917	46.67	4.5028	0.00	1-8-92	1504	45.42	3.3462	-0.05	6-24-92	832	32.99	5.1947	0.03	8-5-92	1154	37.64	0.6251	0.01
9-8-92	1140	47.34	4.7781	0.01	2-5-92	1504	45.42	3.3462	-0.05	6-30-92	832	32.99	5.1947	0.03	9-8-92	858	46.49	5.6179	-1.97
10-8-92	1253	47.38	4.7414	0.00	3-5-92	1545	45.75	2.9829	-0.04	8-2-93	1207	28.65	5.5342	0.02	10-14-93	1315	33.57	0.8604	-0.02
11-10-92	1145	47.24	4.8921	0.00	4-7-92	1047	45.83	2.8734	-0.02	12-5-91	1522	37.64	4.9302	0.00	1-6-93	1154	37.64	0.6251	0.01
12-8-92	1130	45.71	6.4593	0.07	5-5-92	1410	45.71	2.9777	0.00	12-5-91	1325	36.90	5.0882	-0.11	8-2-93	1207	28.65	5.5342	0.02
1-7-93	1044	45.36	6.7876	0.12	6-2-92	1239	44.98	3.7427	0.02	1-6-92	1250	36.62	7.4882	-1.56	9-14-93	1039	46.49	5.6179	-1.97
2-10-93	854	47.11	4.9047	0.12	6-30-92	1215	44.59	4.1226	0.06	4-7-92	745	36.71	6.9423	-1.14	10-15-93	743	48.32	3.638	0.19
3-8-93	958	47.46	4.5194	0.13	8-4-92	922	45.28	3.3759	0.06	5-5-92	758	36.30	6.9285	-1.14	11-19-93	1542	47.09	4.9371	0.11
4-6-93	658	47.87	4.0652	0.11	9-8-92	1225	45.60	3.1474	0.00	5-21-92	***	***	***	***	12-21-93	1533	46.64	5.4563	0.08
5-4-93	1323	47.45	4.5533	0.14	9-8-92	1339	45.71	3.0548	-0.07	6-24-92	832	32.99	5.1947	0.03	3-8-93	1030	5.52	4.787	0.01
6-8-93	819	44.89	7.3122	0.10	11-10-9	1032	45.73	2.9512	-0.04	8-2-93	904	44.87	3.871	0.04	4-7-92	1027	42.67	3.2126	-0.04
8-2-93	848	45.88	6.2654	0.08	12-8-92	1135	45.58	3.1427	-0.02	6-30-92	832	32.99	5.1947	0.03	5-4-92	1508	42.48	3.4746	-0.02
9-14-93	833	46.49	5.6179	0.08	1-7-93	1030	45.42	3.3272	-0.04	8-5-92	855	37.64	0.6251	0.01	4-7-92	1027	42.67	3.2126	-0.04
10-15-93	743	48.32	3.638	0.12	2-10-93	859	45.73	2.9892	-0.03	10-8-92	924	37.84	0.6425	0.00	5-4-92	1508	42.48	3.4746	-0.02
11-19-93	1542	47.09	4.9371	0.11	3-8-93	1357	45.9	2.7798	-0.01	11-10-92	924	37.84	0.6425	0.00	4-7-92	1027	42.67	3.2126	-0.04
12-21-93	1533	46.64	5.4563	0.08	Apr-Jun No Log	922	45.04	3.6498	0.00	5-21-92	***	***	***	***	12-8-92	1237	38	0.676	0.02
					7-8-93	922	45.04	3.6498	0.00	6-24-92	832	32.99	5.1947	0.03	8-5-92	1154	37.64	0.6251	0.01
					8-2-93	904	44.87	3.871	0.04	6-30-92	832	32.99	5.1947	0.03	9-8-92	858	46.49	5.6179	-1.97
					9-14-93	1029	45.09	3.6714	-0.07	8-5-92	1240	36.5	1.9008	0.01	1-7-93	1027	42.69	3.1354	0.01
					10-15-93	750	45.12	3.6459	-0.08	10-8-92	924	37.84	0.6425	0.00	2-10-93	840	42.68	3.1354	0.02
					11-19-93	1550	44.96	3.8049	-0.06	11-10-92	924	37.84	0.6425	0.00	3-8-93	1030	42.75	3.0241	0.06
					12-21-93	1603	44.90	3.8998	-0.09	12-8-92	1156	35.85	2.512	0.01	4-7-92	1027	42.67	3.2126	-0.04
					FI-1					12-8-92	1237	38	0.676	0.02	5-4-92	1508	42.48	3.4746	-0.02
					8-2-93	904	44.87	3.871	0.04	1-6-93	1154	37.64	0.6251	0.01	6-2-92	1001	42.5	3.2018	0.00
					9-14-93	1029	45.09	3.6714	-0.07	12-5-91	1347	41.27	1.0775	0.07	6-30-92	1001	42.5	3.2018	0.00
					10-15-93	750	45.12	3.6459	-0.08	1-6-93	1154	37.64	0.6251	0.01	8-4-92	858	46.49	5.6179	-1.97
					11-19-93	1550	44.96	3.8049	-0.06	3-8-93	1030	5.52	4.787	0.01	9-8-92	717	7.16	2.9691	0.06
					12-21-93	1603	44.90	3.8998	-0.09	4-6-93	848	38.75	4.1508	0.00	10-1-92	1015	42.76	3.0633	0.01
					FI-2					8-5-92	855	37.64	0.6251	0.01	11-10-9	1015	42.76	3.0633	0.01
					8-5-92	855	37.64	0.6251	0.01	9-8-92	858	46.49	5.6179	-1.97	11-10-9	1015	42.76	3.0633	0.01
					10-8-92	924	37.84	0.6425	0.00	1-7-93	1030	5.52	4.787	0.01	12-8-92	1238	42.68	3.1596	0.00
					11-10-92	924	37.84	0.6425	0.00	2-4-92	1203	41.55	1.4777	0.01	11-10-9	1015	42.76	3.0633	0.01
					12-8-92	1156	35.85	2.512	0.01	3-8-93	1030	5.52	4.787	0.01	11-10-9	1015	42.76	3.0633	0.01
					1-6-93	1154	37.64	0.6251	0.01	4-6-93	79	54.89	3.367	-0.21	12-8-92	1238	42.68	3.1596	0.00
					2-8-93	805	54.5	3.801	-0.23	5-5-92	750	41.85	1.1715	-0.00	1-7-93	1027	42.69	3.1406	0.01
					3-8-93	805	54.5	3.801	-0.23	6-2-92	1017	52.56	5.8861	-0.04	12-8-92	1238	42.68	3.1596	0.00
					4-6-93	79	54.89	3.367	-0.21	6-30-92	1001	42.5	3.2018	0.00	11-10-9	1015	42.76	3.0633	0.01
					5-5-92	750	41.85	1.1715	-0.00	8-4-92	858	46.49	5.6179	-1.97	11-10-9	1015	42.76	3.0633	0.01
					6-2-92	1001	42.5	3.2018	0.00	9-8-92	717	7.16	2.9691	0.06	12-8-92	1238	42.68	3.1596	0.00
					6-30-92	1001	42.5	3.2018	0.00	10-1-92	1015	42.76	3.0633	0.01	1-7-93	1027	42.69	3.1406	0.01
					8-4-92	858	46.49	5.6179	-1.97	1-11-91	1144	41.04	2.044	-0.01	2-10-93	840	42.68	3.1354	0.02

Tape and Datalogger Reading Pairs (contd)

Ward/Dr	Time	SrType	DURdg	AltCh	Ward/Dr	Time	SrType	DURdg	AltCh
PS-6									
9-12-91	1348	44.50	no DL	0.01	12-5-91	1150	no tape	5.7357	-0.02
11-11-91	1303	44.18	2.9385	0.03	1-9-92	1420	22.20	10.2590	0.09
12-5-91	1335	44.46	2.6153	0.03	2-4-92	1423	26.99	7.8775	0.02
1-9-92	1311	43.10	4.1478	-0.04	3-6-92	1311	25.07	8.8355	0.02
2-4-92	1244	44.43	2.6845	0.00	4-1-92	815	30.28	6.4188	-0.00
3-4-92	1245	44.01	3.1344	-0.00	5-5-92	837	28.40	7.2659	0.00
4-7-92	741	43.91	3.2248	0.01	6-2-92	748	25.67	8.6190	-0.02
5-5-92	754	43.49	3.6579	-0.01	6-30-92	820	32.18	5.4775	0.03
6-2-92	730	42.26	5.0073	-0.01	9-5-92	917	28.99	7.0651	-0.02
6-30-92	848	41.48	5.8726	-0.04	10-8-92	954	35.08	4.0866	0.06
8-5-92	1235	44.23	2.9048	-0.01	11-10-92	1330	36.25	3.5064	0.08
9-9-92	850	44.97	2.0827	0.03	12-8-92	1500	22.28	10.118	0.07
10-8-92	921	45.29	1.7315	0.07	1-4-93	1441	20.15	11.331	-0.12
11-10-92	1235	45.35	1.7862	0.07	3-8-93	932	36.2	4.0084	-0.35
12-8-92	1139	42.99	4.2866	0.04	5-8-93	1148	36.19	4.0046	-0.35
1-6-93	1346	42.67	4.5204	0.04	6-14-93	1006	31.2	6.4315	-0.46
3-8-93	1145	44.88	2.1303	0.09	7-8-93	1251	25.6	9.144	-0.48
3-9-93	1110	43.69	1.249	0.13	8-2-93	1315	28.64	8.1512	-0.89
4-6-93	834	46.34	0.5131	0.13	9-16-93	1215	32.51	6.1918	-0.77
PS-0A									
6-4-93	1029	21.38	7.8075	-0.30	10-14-93	1423	36.84	4.7291	-1.35
7-8-93	1400	25.58	5.1306	0.00	12-21-93	1339	24.95	10.6020	-1.55
7-12-93	1153	26.48	4.1109	0.05	H4-9				
8-2-93	1331	27.37	2.9684	0.23	9-26-91	1410	43.90	1.6211	-0.04
8-3-93	1235	26.9	3.4895	0.21	10-5-91	1219	44.40	1.4620	-0.01
9-16-93	753	27.9	2.1383	0.33	12-9-92	1354	44.30	2.0366	-0.02
10-14-93	1339	28.28	1.6671	0.54	1-9-92	1315	43.90	1.5453	0.00
11-18-93	1538	27.20	2.7052	0.64	2-4-92	1345	43.95	1.5453	0.00
12-21-93	1427	26.28	3.6707	0.66	3-6-92	1315	44.02	1.4372	0.01
PS-0B									
6-4-93	1029	21.13	11.381	0.29	5-5-92	820	43.75	1.7417	0.00
7-8-93	1402	24.94	9.7428	0.00	7-8-93	1154	45.49	1.4714	-0.01
7-12-93	1152	25.91	8.6553	0.04	8-2-93	804	44.15	1.2885	0.02
8-2-93	1332	27.32	8.0018	-0.04	6-2-92	740	42.43	3.1667	-0.01
9-16-93	754	27.52	7.0307	0.13	6-30-92	810	41.20	4.5037	-0.03
10-14-93	1339	27.45	6.9993	0.09	8-5-92	1300	43.85	1.6489	0.01
11-18-93	1538	27.54	6.8205	0.11	9-9-92	913	44.66	0.7769	-0.01
12-21-93	1427	25.80	8.7096	0.10	10-8-92	943	44.86	0.5745	0.03
PS-44									
7-8-93	1353	32.91	2.9657	0.00	11-10-92	1317	43.21	5.3715	0.00
7-12-93	1142	34.3	1.3917	0.10	12-8-92	1343	42.78	5.8512	-0.02
8-2-93	1237	35.23	0.11106	0.26	1-6-93	1437	42.59	6.08	-0.04
8-3-93	1232	34.48	0.9178	0.36	2-9-93	1131	42.90	5.6132	0.00
9-16-93	815	35.28	0.5071	-0.06	3-8-93	1141	43.17	5.4149	-0.00
9-28-93*	1420	35.06	4.7646	0.15	4-6-93	923	43.6	4.9779	-0.02
10-14-93	1334	35.25	4.7207	-0.15	Disconnected XD				
11-18-93	1524	35.13	4.7283	-0.04	8-2-93	1443	42.59	6.0148	0.02
12-21-93	1426	33.18	6.139	0.60	9-15-93	1443	42.52	5.9914	0.11
PS-46									
5-20-93	823	47.72	5.1912	0.07	10-14-93	1154	43.43	5.0640	0.07
7-8-93	1330	46.87	6.1678	0.01	11-16-93	1557	43.38	5.0472	0.13
7-12-93	1423	47.02	6.0171	0.00	12-21-93	1310	43.32	5.0851	0.16
7-14-93	1423	47.09	5.9709	-0.03	H4-10				
8-2-93	1257	47.29	5.7447	-0.02	5-26-93*	1059	26.26	8.6749	0.00
8-3-93	1224	47.33	5.7019	-0.02	6-14-93	1113	20.03	4.6504	-0.03
9-16-93	745	48.56	4.3629	-0.00	7-8-93	1247	28.83	4.8555	-0.02
10-14-93	1305	49.03	3.8976	-0.04	8-2-93	1212	30.78	3.858	-0.04
11-18-93	1455	48.84	4.0729	-0.02	9-15-93	1457	31.99	2.6361	-0.12
12-22-93	1420	48.51	4.4629	-0.05	10-14-93	1223	32.28	2.3870	-0.18
PS-1									
6-4-93	906	33.27	10.09	0.00	11-16-93	1439	31.17	3.5918	-0.19
7-8-93	1410	35.75	7.5071	-0.09	12-21-93	1329	30.79	4.0059	-0.19
8-2-93	1339	36.44	6.7852	-0.11					
9-16-93	804	37.93	5.212	-0.14					
10-14-93	1347	38.45	4.6934	-0.18					
11-18-93	1553	38.05	5.0008	-0.14					
12-21-93	1437	37.74	5.5159	-0.23					



Tape and Datalogger Reading Pairs (comid)

Well/Da	Time	St.Tape	DLRdg	Abs.Ch	Well/Da	Time	St.Tape	DLRdg	Abs.Ch
B3-1					B4-1				
9-27-91	1257	46.79	2.7586	-0.04	9-23-91	1355	61.91	1.7979	-0.11
12-5-91	1030	47.06	2.4401	-0.01	12-5-91	1050	62.98	0.5319	-0.00
1-9-92	1516	45.30	4.3026	0.00	1-9-92	1458	63.06	0.4435	0.00
2-4-92	1520	46.83	2.6705	0.00	1-21-92*	Replace			
3-6-92	1357	46.25	3.2911	0.00	2-4-92	1510	63.20	5.8207	-0.12
4-7-92*	910	46.54	-0.2865	3.06	3-6-92	1353	63.39	5.9804	-0.06
5-5-92*	935	46.01	4.9500	-1.32	4-7-92	853	63.53	5.4742	-0.13
5-21-92	...	...	...	...	5-5-92	915	63.59	5.2738	0.00
7-2-92	...	...	...	...	6-2-92	821	63.19	5.6286	0.07
7-28-92*	1142	46.63	2.6544	0.00	7-2-92*	.....			
8-5-92	1406	46.90	2.4125	0.01	7-28-92*	842	63.14	5.8577	0.00
9-9-92	1004	48.08	1.2926	0.01	8-5-92	1348	63.27	5.7775	-0.06
10-4-92	1044	48.42	0.955	0.03	9-9-92*	955	63.72	5.3417	-0.10
11-10-92	1436	48.63	0.7541	0.03	10-4-92	1000	64.13	4.7133	0.07
12-8-92	1444	45.46	3.6704	0.12	11-10-92	1417	64.57	3.9033	0.39
1-6-93	1540	45.22	4.0144	-0.01	12-8-92	1418	64.3	4.1218	0.45
2-9-93	1244	47.9	0.9188	0.58	1-6-93	1535	64.01	4.5143	0.38
3-9-93	1318	48.87	0.1601	0.41	2-9-93	1231	64.06	4.4078	0.43
3-23-93	1532	49.63	4.6987	0.00	3-9-93	1304	64.34	4.206	0.33
4-6-93	1035	48.78	4.4504	1.11	4-6-93	1017	64.85	3.4061	0.38
					5-27-93	1021	64.25	4.6367	0.02
B3-46					7-14-93	1203	63.91	4.4111	0.37
5-28-93	1230	46.05	8.489	0.11	8-2-93	737	63.95	4.468	0.48
7-4-93	857	48.63	5.8379	0.00	9-15-93	700	64.58	4.3185	-0.01
7-14-93	1222	48.94	5.4307	0.07	10-14-93	713	64.97	3.3586	0.49
8-2-93	825	49.74	4.5124	0.13	11-17-93	1346	65.20	3.2786	0.33
9-15-93	801	51.31	2.8968	0.06	12-21-93	912	64.95	3.5066	0.37
10-14-93	750	51.43	2.6889	0.14					
11-17-93	1445	51.12	3.1281	0.04	B3-2				
12-21-93	947	49.72	4.6379	0.03	5-31-93	1100	61.98	8.2133	0.00
					7-14-93	1214	61.78	8.4549	-0.05
B3-47					8-2-93	804	61.84	8.4491	-0.11
5-28-93	1050	43.04	8.3201	0.00	9-15-93	713	62.55	7.8876	-0.23
7-4-93	838	46.1	5.1022	-0.08	10-14-93	737	63.04	7.5173	-0.33
8-2-93	815	47.61	3.5853	-0.10	11-17-93	1409	63.16	5.8401	1.31
9-15-93	747	49.27	1.7057	-0.09	12-21-93	931	61.55	7.7241	0.94
10-14-93	746	49.48	1.5425	-0.15					
11-17-93	1422	48.77	2.2444	-0.09					
12-21-93	941	45.94	3.8654	1.23					
B4-4									
9-27-91	8346	73.92	3.4563	-0.04					
12-5-91	1115	74.93	2.3084	0.02					
1-9-92	1448	75.12	2.0982	0.02					
2-4-92	1449	75.15	2.0675	0.02					
3-6-92	1346	75.80	1.7948	-0.38					
4-7-92	847	75.86	1.7174	-0.36					
5-5-92	910	75.63	1.5748	0.00					
6-2-92	813	75.24	1.9500	0.04					
7-2-92*	.....	.....	.....	.....					
7-28-92*	759	75.43	2.1547	0.00					
8-5-92*	1342	75.36	2.0631	0.15					
9-9-92	949	75.96	1.5866	-0.00					
10-8-92	1020	76.00	1.1793	0.34					
11-10-92	1401	76.35	0.7727	0.37					
12-8-92	1406	76.35	0.7728	0.37					
1-6-93	1525	76.06	1.0903	0.36					
2-9-93	1218	75.96	1.1928	0.37					
3-9-93	1259	76.13	1.0011	0.38					
4-6-93	1011	76.57	0.5219	0.38					

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## Appendix C

### Location and Calibration Data

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# Appendix C

## Location and Calibration Data

Appendix C contains information about the locations of the wells and river stations, their assigned station number, and the transducers used there. Next is the initial calibration data pertaining to each transducer.

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# Installation Data

SN\_LBTS. 110 Gable Bute Relay  
 Rev.2/94 130 High Bay, 300 Area Relay

ELEV.MS ToC	STA.	WELL	XD SN & Date In		ELEV.MS ToC	STA.	WELL	XD SN & Date In		ELEV.MS ToC	STA.	WELL	XD SN & Date In	
381.40	(300AREA)	129	4-9	409783	removed									
				7/16/91										
345.00		128	300-RIV	400814		412.12	054	F5-4	400921	removed	471.49	171	D5-13	426122
	Scale slipped down 0.4ft			11/6/91					9/24/91		470.88	77		5-21-93
574.19		127	4A	409780	409779 removed	412.95	056	F5-6	400925	removed	471.53	170	D5-15	400806
				10/4/91					9/24/91					5-19-93
				6/25/92		406.56	051	F5-1	400927	501375 removed	468.11	172	D5-20	425865
373.89			4B	425860	removed				9/24/91	6/24/92				5-19-93
				10/4/91		373.33	140	F-RIV	501357		442.78	173	D8-34A	409773
372.24	(371.10*)	4C		409774	400927 removed	397.95	132	F1-2	409783	6-4-93	442.75	77		5-19-93
	base angl			1/24/92					6-4-93		442.51	173	D8-54B	409776
373.86		126	3A	400615	removed				390088	482452				5-19-93
				12/13/91		395.35	151	F5-43A	6-4-93	1/19/94				
379.74		121	1A	410070	409776 removed	394.87	151	F5-43B	400615		426.09	133	N-Riv	395112
				11/23/91					6-4-93					8/6/93
379.88			1B	400613	removed	402.65	144	F5-44	395108	409780				
				11/23/91					5-28-93	9-28-93				
379.48			1C	409773	removed	416.95	154	F5-46	400921					
				11/23/91					5-20-93					
394.88		120	8-1	425876		405.15	150	F6-1	426120		409.85	183	K-18	426118
				5/1/92					6-4-93					5-21-93
387.31		119	3-9	400808	removed						466.09	180	K-30	425860
				7/17/91										5-21-93
390.83		118	18A	395108	removed									
				7/2/91		386.47	125	H-RIV	404333					
389.94			18B	410075	410067 removed	Top 2" Pipe - 0.4395 ± Tape			9/26/91					
				7/2/91		EC probe			SN1033	± = 1.42	412.30	181	K-31	390084
388.05			18C	400806	removed				11/15/93					5-21-93
				7/2/91		420.59	124	H4-7	426125		444.02	182	K32-A	409779
375.87		117	1-30B	425877	removed				9/26/91					5-21-93
				1/24/92		418.08	123	H4-9	395112	501395	445.27	182	K32-B	394990
381.14		116	16B	409782					9/26/91					5-21-93
				7/15/91		413.50	122	H4-12A	394990	501362	441.80	184	K-37	425871
382.29			16C	507401					9/26/91	6/24/92				5-27-93
				9-28-93		413.52	122	H4-12C	390089					
400.61		115	5A	426118	removed				2-11-93					
				1/23/92		417.83	138	H3-2A	425875					
400.14			5B	426120	removed				11-7-92					
				1/23/92		418.22	138	H3-2C	390092					
400.20			5C	390084	removed	404.44	160	H4-10	410071					
				1/23/92					5-26-93					
386.34		113	3-12	3990887	removed	416.84	137	H4-11	386999	481177	503403			
				2/13/92					2-8-93	10/5/93	12-29-93			
376.99		112	4-7	390466	400928 removed				EC probe	SN ???	± = 1.42			
				11/22/91		418.10	161	H6-1	410067					
395.00		111	4-1	409775					5-26-93					
				11/22/91					SN1086	± = 1.371				
385.63		109	1-7	409779	425875	1/20/94			EC probe	SN1087	± = 1.399			
				12/18/91					139	Seep153-1				
384.91			1-8	404587	removed				EC probe					
				7/15/91										
384.80			1-9	410071	425874 removed									
				7/15/91										
389.76		108	8A	400930										
				12/18/91										
390.26		107	7A	426122	removed	472.14	044	B4-4	404586	GEOLOG	404586	removed		
				11/20/91					9/27/91	4/21/92	7/28/92	spg.93		
390.43			7B	425871	removed	461.80	041	B4-1	400928	426127	GEOLOG	426127	400925	507400
				11/20/91					9/23/91	1/21/92	4/21/92	7/28/92	5-27-93	11/23/93
390.34			7C	425865	removed	439.79	031	B3-1	400929	GEOLOG	501354	removed		
				11/20/91					9/27/91	4/21/92	7/28/92	spg.93		
386.93		106	6-1	409778		439.06	191	B2-12	425874					
				1/28/92					5-27-93					
395.60		105	5-1	394990	removed	448.31	114	B-Riv	425863					
				8/13/92					3/11/92					
384.52		104	1-2	394096		418.53	143	B2-13	501375					
				1/29/92					5-29-93					
375.53		103	2-2	410071	removed	441.62	192	B3-46	404586					
				9/16/92					5-29-93					
375.26		102	2-1	425872		438.78	191	B3-47	404587					
				1/29/92					5-28-93					
375.80		101	1-1	425864		458.91	141	B5-2	501370	409774				
				1/29/92					5-31-93	1/19/94				

92-0278-116

Initial Calibration Data

CALIBRATION FROM LRB54110

*****							
XD SN	Factor	Original Order	Page Listed IN 54110	XD SN	Factor	Original Order	Page Listed IN 54110
386999	0.930129	49	57	425871	0.930162	34	55
390008	0.929759	45	57	425872	0.925998	46	57
390084	0.925817	44	56	425873	0.924778	53	58
390088	0.921753			425874	0.927466	52	58
390089	0.930984	50	57	425875	0.923511	55	58
390092	0.933043	48	57	425876	0.933277	38	55
390466	0.931572	32	43	425877	0.924719 recal	54	58
394096	0.940487	10	38	426118	0.919618	40	56
394990	0.934299	2	38	426120	0.927198	41	56
395108	0.928344	23	42	426122	0.927131	33	55
395112	0.934208	5	38	426123	0.928045	43	56
400613	0.928318 r	25	42	426125	0.924634	39	56
400615	0.926237	30	43	426127	0.92888 recal	42	56
400806	0.925422	22	41	REPAIRED XD's added 9-4-92			
400808	0.924320	26	42	394990	0.924224	3	108
400814	0.934277	24	42	400927	0.919469	1	108
400921	0.928259	6	38	400928	0.924320	4	108
400925	0.938906	4	38	409779	0.930646	5	108
400927	0.925948	3	38	410071	0.929051	2	108
400928	0.930894	9	38	NEW XD's added 9-4-92			
400929	0.937396	7	38	501356	1.056266	3	108
400930	0.928236	11	40	501357	1.050504	4	108
404333	0.934862	1	38	501359	1.063546	2	108
404586	0.932610	8	38	501362	1.056783	5	108
404587	0.927600	12	40	501370	1.049866	1	108
409773	0.933826	17	41	501375	1.059638	6	108
409774	0.9307 rec	15	40	NEW XD's added ----			
409775	0.930978	28	42	481177	1.053189		147
409776	0.933341	27	42	482452	1.05196 recal		146
409778	0.931615	16	40	495533	1.051341		146
409779	0.935513	13	40	500042	1.051024 recal		146
409780	0.927762	29	43	501379	1.05512 recal		146
409782	0.930449	31	43	503403	1.052781		147
409783	0.928530	14	40	503546	1.058283		146
410067	0.931645	20	41	507381	1.067479 recal		146
410070	0.931287	18	41	507384	1.047854 recal		147
410071	0.931156	19	41	507389	1.038989 recal		147
410075	0.923157	21	41	507392	1.068226 recal		147
425860	0.925743	36	55	507394	1.055505 recal		146
425863	0.926984	51	58	507396	1.062276 recal		147
425864	0.929513	47	57	507397	1.055673 recal		146
425865	0.932000	35	55	507400	1.051118		147
425871	0.930162	34	55	507401	1.053642		146

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