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Author	Addressee	Correspondence No.
R. J. Schepens/ORP	M. A. Wilson/DOEC	05-ED-085

Subject: FINAL DANGEROUS AND/OR MIXED WASTE RESEARCH, DEVELOPMENT, AND DEMONSTRATION PERMIT FOR THE DEMONSTRATION BULK VITRIFICATION FACILITY: DESIGN - AGREED TO REVISIONS FOR SECONDARY WASTE AND WASTE DRYER SYSTEM DESIGNS

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05-ED-085

OCT 27 2005

Mr. Michael A. Wilson, Program Manager
Nuclear Waste Program
State of Washington
Department of Ecology
3100 Port of Benton Blvd.
Richland, Washington 99352

Dear Mr. Wilson:

FINAL DANGEROUS AND/OR MIXED WASTE RESEARCH, DEVELOPMENT, AND DEMONSTRATION PERMIT FOR THE DEMONSTRATION BULK VITRIFICATION FACILITY: DESIGN – AGREED TO REVISIONS FOR SECONDARY WASTE AND WASTE DRYER SYSTEM DESIGNS

References:

1. Ecology letter from M. A. Wilson to R. J. Schepens, ORP, K. A. Klein, RL, and E. S. Aromi, CH2M HILL, "Final Dangerous and/or Mixed Waste Research, Development, and Demonstration Permit for the Demonstration Bulk Vitrification Facility," dated December 13, 2004.

2. ORP letter from R. J. Schepens to M. A. Wilson, Ecology, "Final Dangerous and/or Mixed Waste Research, Development, and Demonstration Permit for the Demonstration Bulk Vitrification Facility: Required Design Submittal for Secondary Waste and In-Container Vitrification (ICV™) Storage Area Foundation Systems," 05-TPD-050, dated May 13, 2005.

3. ORP letter from R. J. Schepens to M. A. Wilson, Ecology, "Final Dangerous and/or Mixed Waste Research, Development, and Demonstration Permit for the Demonstration Bulk Vitrification Facility Required Submittal for the Waste Dryer System," 05-TPD-053, dated May 26, 2005.

4. ORP letter from R. J. Schepens to M. A. Wilson, Ecology, "Final Dangerous and/or Mixed Waste Research, Development, and Demonstration Permit (RD&D Permit) for the Demonstration Bulk Vitrification Facility Required Submittal for the Secondary Waste System," 05-ED-057, dated July 20, 2005.

This letter transmits the revised drawings to the Secondary Waste System (Attachment 1) and the revised certified Independent Qualified Registered Professional Engineer report for the Waste Dryer System (Attachment 2) for the State of Washington, Department of Ecology (Ecology) review and approval. A CH2M HILL Hanford Group, Inc. (CH2M HILL) and U.S. Department of Energy (DOE), Office of River Protection (ORP) certification is provided in Attachment 3.

The Final Dangerous and/or Mixed Waste RD&D Permit for the Demonstration Bulk Vitrification System requires submittal of engineering design and supporting information for Ecology review and approval (Reference 1). On May 13, 2005, DOE ORP and CH2M HILL submitted engineering design and support information for the Secondary Waste System and two ICV™ Storage Area foundation systems (Reference 2). On May 26, 2005, ORP and CH2M HILL submitted engineering design and support information for the Waste Dryer System (Reference 3).

Ecology and the U.S. Environmental Protection Agency staff reviewed the submitted information and provided comments in the Review Comment Record (RCR) (Attachment 4). All comments were successfully resolved. Revisions to the initial submittal for the Secondary Waste System were previously provided (Reference 4). Ecology staff subsequently requested that two of the drawings provided as Attachment 5 to the submittal be amended to include information as provided in the original RD&D Permit application. The changes have been made and the revised drawings are provided with this letter (Attachment 1).

For the Waste Dryer System, the certified report provided by the Independent Qualified Registered Professional Engineer was revised and is also included (Attachment 2). There were other changes that will be made to the Waste Dryer System design based on RCR comments. However, as agreed to in the comment resolution, these changes will be documented in later revisions to the overall facility design, or will be incorporated into the as-built drawings.

If you have any questions, please contact me, or your staff may contact Woody Russell, Environmental Division, (509) 373-5227.

Sincerely,

Roy J. Schepens
Manager

ED:RWR

Attachments: (3)

cc: See page 3

cc w/attachs:
F. R. Miera, CH2M HILL
J. Cox, CTUIR
S. Harris, CTUIR
K. A. Conaway, Ecology
D. Hendrickson, Ecology
S. A. Thompson, FHI
G. Bohnee, NPT
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cc w/o attachs:
L. Cusack, Ecology
S. L. Dahl, Ecology
G. P. Davis, Ecology
K. Niles, Oregon Energy
B. L. Charboneau, RL

Attachment 1
05-ED-085

State of Washington, Department of Ecology,
Review Comment Record

Any procedure, method, data, or information contained in this document that relates to the radioactive source, byproduct material, and/or special nuclear components of mixed waste (as defined by the Atomic Energy Act of 1954, as amended) is not provided for the purpose of regulating such components under the authority of this Permit and Chapter 70.105 Revised Code of Washington.

REVIEW COMMENT RECORD (RCR)

1. Date 7/17/05	2. Review No.
3. Project No.	4. Page 1 of 3

5. Document Number(s)/Title(s)	6. Program/Project/Building Number	7. Reviewers	8. Organization/Group	9. Location/Phone
Waste Dryer		CM	EPA	

17. Comment Submittal Approval:	10. Agreement with indicated comment disposition(s)	11. CLOSED
Organization Manager (Optional)	Reviewer/Point of Contract	Reviewer/Point of Contact
	Date	Date
	Author/Originator	Author/Originator

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
1	Permit Attachment LL, Section 4, Subsection 4.2.8, last paragraph, Page 4-7 amend this section to include a description of the following new components of the waste dryer system: sintered metal filter prior to condenser, vacuum off-gas condenser, and rupture disk. Also amend this section to address how the requirements under Permit Condition II.A.5. will be implemented under the scenario where the waste dryer is producing non-condensable gases and the OGTS is not operational.		In compliance with Permit Condition II.A.5., in the event the OGTS is not operational, waste will not be introduced into the waste dryer system. In the event that the waste dryer off-gas system vacuum pump is not operational—e.g., not pulling a vacuum on the dryer—waste will not be added to the dryer. Proper controls/hold points will be written-in to the DBVS operating procedures. Section 4.2.8 "Waste Feed Preparation" describes the process of mixing and drying the liquid waste and additives and a description of the off gas system would be better placed in section 4.2.14 "Mixer/Dryer Offgas Emission Control". The additional sintered metal filter and rupture disk can be described here with the off-gas condenser.	Closed
2	Permit Attachment LL, Section 4, Table 4-2, provide documentation from the vendors whether the equipment that is proposed will meet the efficiencies provided in this table including the equipment not previously included as part of the waste dryer system (i.e., Waste Dryer Vacuum Off-gas Condenser and Waste Dryer Sintered Metal Filter). Amend the table to reflect any revised efficiencies		Final vendor information for these two components is not available. It will be submitted with the installation assessment report in accordance with the permit condition I.E.9.a.i. However, our specifications to the vendor do require that the vendor provide the equipment to efficiencies as identified in Table 4-2.	Closed
3	Permit Table IV-1, amend to include Waste Dryer Vacuum off-gas Condenser Tank (33-D74-033) and update PFDs to include. Also based on the condensate from the pulse back filter draining through a steam trap to the Waste Dryer Steam Condensate Tank (33-D74-022) this tank must also be added to Permit Table IV-1. Permit		Will include 33-D74-033 in Table IV.1. 33-D74-022 is a steam condensate tank, which collects steam condensate from steam jackets on the waste dryer and dryer SMF. Note that these steam jackets isolate the steam from the liquid/solid/gaseous waste stream. The steam is therefore not	Closed

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
	Attachment KK, Section 4 needs to be revised to address these tanks.		contaminated and its associated equipment is not RCRA regulated. We believe that the tank should not be added to Permit Table IV-1.	
4	Permit Table V-1, amend to include Waste Dryer Vacuum Off-gas Condenser (33-D10-032) and update PFDs to include.		33-D10-032 acts as a cooler for the liquid seal for the vacuum pump and is not expected to be contaminated. Therefore, the Waste Dryer Vacuum Off-gas Condenser would not be added to Permit Table V-1. However, there is a potential that the liquid seal would become contaminated during a malfunction of the pump. Again, this is not anticipated, however, we will evaluate for any potential occurrence during the conduct of the RD&D.	Closed
5	Permit Table V-1, amend to include under Waste Dryer System, "Control System for glass former additives feed to dryer**". Zirconium oxide and boron oxide.		Permit Tables V-1 and V-4 will be amended to include under the Waste Drying System: "Control System for glass former additives feed to dryer[a*]"	Closed
6	Permit Table V-1, amend to include Waste Dryer Sintered Metal Filter (33-NO2-014) and Waste Dryer HEPA Filter (33-NO2-017) and update PFDs to include.		Tables V.1 and V.4 will be amended to include 33-N02-014 and 33-N02-017 and the PFDs will be updated at their next revision.	Closed
7	IQRPE Report No. DR-009, Rev. 0, Section 2.2.1.2, reference to Section 2.2.1.4 is incorrect. The correct reference is Section 2.2.1.5.		Will correct reference in the revision of IQRPE report. See Comment #9 below.	Closed
8	IQRPE Report No. DR-009, Rev. 0, Section 2.2.2.and 2.2.6, further IQRPE evaluation needs to be performed after spiking materials are selected for the campaign test plans.		Spiking materials are not expected to appreciably change the corrosive characteristics of the waste evaluated in the IQRPE Report. In the instances where spiking materials are to be used, the Campaign Plan will describe spiking materials and concentrations to be added to the waste feed. If it is anticipated that the spiking materials added to the waste feed could potentially change the waste feed chemistry in a manner that would appreciably increase the risk of corroding, causing a leak or rupturing DBVS waste contacting components, an independent, qualified corrosion engineer must evaluate the	Closed

REVIEW COMMENT RECORD (RCR)

1. Date 7-15-03	2. Review No.
3. Project No. N/A	4. Page 3 of 3

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
			extent of this risk.	
9	IQRPE Report No. DR-009, Rev. 0, Section 2.2.3.4, 2.2.4.1, 2.2.4.4, 2.2.5.4, in each of these sections the IQRPE has indicated that the information provided for review did not allow a determination that the design basis was sound. In packages provided for other components of DBVS that Ecology has provided approval to date for construction, there have been exceptions cited by IQRPE as needed to be addressed to allow the IQRPE's certification, but not to the extent that the design basis could not even be determined to meeting the requirements for certification. Ecology must be provided confirmation that these issues with potential flaws with design basis that the IQRPE has raised will be addressed prior to the acquisition of this equipment.		The IQRPE report is being revised and will be resubmitted.	Closed

Washington State Department of Ecology REVIEW COMMENT RECORD (RCR)	1. Date 6/10/2005	2. Review No. 2
	3. Project No.	4. Page 1 of 4

5. Document Number(s)/Title(s)	6. Program/Project/Building Number	7. Reviewer	8. Organization/Group	9. Location/Phone
RPP-24544, Rev 1a, Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package for the Waste Dryer System, Section 2.2 of RPP-24544 and Appendices		D. W. Hendrickson, P.E.	Washington Department of Ecology, NWP	3100 Port of Benton Blvd.; Richland, WA 509.372.7983

17. Comment Submittal Approval:	10. Agreement with indicated comment disposition(s)	11. CLOSED
Date Organization Manager (Optional)	Date Reviewer/Point of Contact Author/Originator	Date Reviewer/Point of Contact Author/Originator

Item	Location in Document	Comment	Hold Point	Disposition (Provide justification if NOT accepted.)	Status
1	RPP-24544, §2.2.2, page 2-15 & App. C2 drawings F-145579-00D-0029 & -0030	Text describes weep holes in the shield wall base to allow free drainage of rainwater. Drawings show no retention before such water would go to grade soil. Please confirm that the flooring within the shield walls, from which the rainwater is released, is not relied upon as dangerous waste secondary containment.		Correct. The flooring within the shield walls is not relied upon for dangerous waste secondary containment. Dryer pad/Dryer shield wall details were therefore not included in this design package. Drawing 00-B-0020, Rev. E, "Bulk Vitrification Dryer Area – Walls Plan and Details", shows the Dryer area shield wall and weep holes described in the text. This drawing is appropriately included in the Balance of Design package.	Closed
2	RPP-24544, §2.2.7.9, Table 2-3, Page 2-23	Foot note 'b' is not used within the table. It is apparent that interlocks DAA and DAB should be referred to F-145579-33-A-0101 (zone C4) and that footnote b should be in reference to this drawing.		Correct. Table 2-3 will be updated accordingly.	Closed

3	RPP-24544, §2.2.11, page 2-27	Repeat of 3/31/05 comment #3: *"§2.2.11: This text cites that the IQRPE installation report will be accessible at the DBVS site. The report should be submitted for Ecology operational approval."*		Proposed permit modification for certification of construction includes the following: "I.E.9.a.i. Permittees have submitted copies of all independent qualified registered professional engineer (IQRPE) installation reports to Ecology". Section 2.2.11 text will be modified as follows: "This report will be accessible at the DBVS site, will be submitted to Ecology and contain the following information:"	Closed
4	RPP-24544, App. A2, 145579-A-CA-004, Rev. D	Reiterate comment from 3/31: please consider tabulating material separation factors for unit operations. These assumptions (however justified) may then be clearly defended or corrected with RD&D results for final facility permit considerations.		Separation factors for melter contained in A-DC-002 section 3.5.2 and 3.5.3. Separation factors for quencher/scrubber contained in A-DC-002 section 3.6.1. Separation factor for Tri-Mer contained in A-DC-002 section 3.6.2. NOx conversion factor in SCR contained in A-DC-002 section 3.6.3	Closed
5	RPP-24544, App. A2, 145579-A-CA-004, Rev. D, Attach. 1, Page 28 of 35, and verification comments (A2-88)	This page is the PFD source for F-145579-00-A-021. This page and the verification reviews were dated circa April 6-13. Errors were highlighted upon stream 7 which are not been reflected in the Rev. 0H PFD (F-145579-00-A-0021), dated May 10, 2005. Please clarify the operating conditions and PFD data for Stream 7.		Stream conditions will be updated at the next logical revision, but vendor information must be available before the update can be done.	Closed

Washington State Department of Ecology REVIEW COMMENT RECORD (RCR)	1. Date 6/10/2005	2. Review No. 2
	3. Project No.	4. Page 3 of 4

6	RPP-24544, App. A2, 145579-A-CA-004, Rev. D, Attach. 1, Page 28 of 35	Mass balances around the dryer: given the limited number of balances available based upon this data, please describe how the water and sodium can nearly balance (probably only different due to precision of display), the continuous mass flow rate shows a 1.3% imbalance, and the design mass flow rate and batch match flow rate each show a 68% imbalance (hint – stream 5)		The design mass flow rate and batch flow rates balance within 1.7% when flow rates (pounds/hour) are multiplied by batch transfer times (hours) to get pounds.	Closed
7	RPP-24544, App. A2, 145579-A-CA-004, Rev. D, Attach. 1, Page2 2-6 of 35	I agree with reviewer that differences from the IDEAS print out are not generally significant – however, I simply do not understand how there ARE differences since these pages are "directly imported from the IDEAS software modules" and "no calculations or formulae" are present on this sheet. [Quotes from page 7 of 30 of calculation document.] Please clarify the source of uncorrected transcription errors.		The IDEAS program performs recycle loop calculations by using convergence routines. The mass flow rates are then fed into the pressure drop calculation and an iteration between the IDEAS program and the pressure drop calculation is performed. Between the convergence routines and the iteration, every run will produce slightly different results. The print out from IDEAS and the input to the may have been different runs. While this is not perfect, the important point is that the calculations are accurate within 2%. The calculations are done to the level of our knowledge at this point in time. During cold testing and during startup at DBVS, these material balances will be verified.	Closed
8	RPP-24544, App. G2, 143643-D-SP-001, §1.2	Nomenclature – the sintered metal filter is addressed within scope as a 'close coupled sintered metal filter,' in §3.1.1.9.g as a 'vacuum filter', and in 3.3.1.1.12 as a 'Pulse back filter'. Please ensure that your vendors can clearly deliver the requested material.		Vendor's design has progressed and he has demonstrated an understanding of equipment to be delivered.	Closed

	RPP-24544, App. G2, D-SP-001, §3.3.1.1.15 & §2.2	Please clarify the range, precision, and calibration standards to be employed in the load cell specification.		The range, precision and calibration standards employed will be to load cell manufacture's specification. Note that the load cell specification states that "Accuracy will be the larger of the following: 0.1% of the applied load or 1 scale graduation may be expected, scale graduations are a combination of the installation, the equipment used in the installation supplied by seller and the scale instrument." A load cell set point calculation, complete with instrument calibration data, will be prepared upon receipt of dryer vendor information.	

Washington State Department of Ecology REVIEW COMMENT RECORD (RCR)	1. Date 8/22/2005	2. Review No. 1
	3. Project No.	4. Page 1 of 17

5. Document Number(s)/Title(s)	6. Program/Project/ Building Number	7. Reviewer	8. Organization/Group	9. Location/Phone
RPP-24544, Draft, Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package for the Dryer Section 2.2 of RPP-24544 and Appendices, Rev. 1A dated April 29, 2005		R. K. Biyani, P.E	Washington Department of Ecology, NWP	3100 Port of Benton Blvd.; Richland, WA (509) 372-7884

17. Comment Submittal Approval:	10. Agreement with indicated comment disposition(s)	11. CLOSED
Date Organization Manager (Optional)	Date Reviewer/Point of Contact Author/Originator	Date Reviewer/Point of Contact Author/Originator

Item	Location in Document	Comment	Hold Point	Disposition (Provide justification if NOT accepted.)	Status
1	The dryer heat load calculation, 145579-D-CA-003 Note: This Comment was Transferred from Dryer RCR Part 1; Comment # 17 (Aug 17, 2005)	The dryer heat load calculation, 145579-D-CA-003; • The resistance to heat transfer, defined by heat transfer coefficients, has not been accounted for. • Steady state is never reached in the dryer because continual small additions of waste are planned to be made. Therefore the rate of water evaporation will continuously vary. Both these factors will limit the maximum amount of heat that can be transferred to the wet particle and I expect the overall time averaged production rate will be considerably lower than expected. This has not been taken into consideration in the calculation in the Scenarios described in Section 5. The assumption in your calculations (that whatever heat is applied to the wall of the dryer will be transferred to the dryer contents) is simplistic. Please refer to Appendix C2, Page C2-7, to see how Littleford Day, Inc. has determined the U-factor. Results (U-factors) from the pilot tests are applied to determine the time required for drying in the DBVS. Please	X	See Assumption #2. The energy required to evaporate the water dominates and is about 10x the heat transferred to a fluidized bed of soil in the dryer via convection. The dryer will be operated such that the bleed fed into the dryer is added at a constant rate and boiled-off at a constant rate. Pilot-scale testing proved that this can be done and full-scale commissioning testing will be performed to prove this out prior to facility start-up. The total operating efficiency for DBVS is 70%. Downtime while soil/waste & additives are in the dryer would be considered an abnormal event. Dryer maintenance/troubleshooting would be performed during DBVS facility downtime.	Closed 8/31/05

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		reconcile and revise your processing time determinations in DBVS.TRPT.002, Rev. 0 . In Appendix C3, Littleford Day in their test report Summary state the dry batch method has "… a production rate at approximately one third (1/3) of the wet batch method". Also, what Total Operating Efficiency has been assumed for the dryer? **1.a. Does your recommended baseline of 5000 L final product Batch Size in 8 hours include the stated 70% TOE?** - Is there downtime when either soil or waste or additives are added to the dryer? Please explain your assumption #1; what is the basis for choosing the three cases. Please provide copy of Ref 31 on page 4 of this calculation. **1.b. When will the AMEC document A-DC-002, "Bulk Vitrification Process Improvement Design Criteria – Full DBVS, Rev 0D dated February 14, 2005" (current Rev requested) be formally accepted by CH2M HILL and provided to Ecology?** **1.c. Littleford has calculated the Heat Transfer coefficient based on data gathered in the 130 L dryer test. Littleford has then used this measured value of heat transfer coefficient to determine the rate of heat transfer possible in the 10,000 L dryer. Littleford's primary objective of the test is to determine how long it will take to process one batch. Only then can a valid estimate of the dryer throughput be made the boiler properly sized.** **The sizing of the boiler can not be correctly done without evaluating the heat transfer coefficient. AMEC has chosen not to use this**		The three cases treated are meant to explore the possibilities of running the dryer differently than the baseline case. The chiller and boiler units selected are adequate for making the baseline operating case work. AMEC document A-DC-002 is an AMEC document that has been checked by CH2M HILL, but not accepted via the formal calculation acceptance process. The latest revision will be provided informally, when it becomes available. Heat transfer coefficient used in Litterford calcs is used for sizing steam supplies for their customer's dryer. It is intended to be a conservative estimate of needed steam supply. The DBVS dryer, as configured in the design package, will provide sufficient data to support design of a production facility. Confirmation of the estimated cycle time for producing an ICV box will be done during DBVS start-up testing and DBVS test campaigns. Information on DBVS throughput will be provided in DBVS Campaign Reports. **1.a. Yes. 5,000 L dryer product batch size is**	

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		approach. The basis of AMEC's assumption of a particular drying time (and then proceeding to size the boiler) is not evident. Please confirm if my understanding is correct. Littleford projects a drying time of 15 hours (see p. C2-12 of DBVS.TRPT.002) versus AMEC's assumption of 8 hour (see Section 5.4 on p. A2-94 of Calc 145579-D-CA-003). Please explain this discrepancy. 1.d. The throughput achievable in the DBVS will be a major factor in the decision of selecting this Supplemental Technology for treating approximately two-thirds of the Low Activity Waste from Hanford's waste tanks. It is important for Ecology to understand clearly and correctly the design basis that will drive the DBVS tests.		consistent with 70% TOE of DBVS plant. 1.b. At completion of Design, A-DC-002 will be finalized (number revision) and accepted by CH2M HILL (Note Rev. 0F, the most current version of this document, was provided to Ecology on 8/16/05). 1.c. The basis for AMEC's assumptions are evident in DBVS.TRPT.002, Section 4.5.2. The discrepancy between the Littleford calculation and the AMEC (DMJM) can be accounted for as follows: 1. AMEC calculation credits plow heating as a contributor to drying waste. 2. AMEC calculation dries 8037 kg of S-109 simulant, which equates to about 12,000 lbs of water driven off (consistent with the	

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				PDC); whereas the Littleford calc. removes 14,230 lbs of water. Validation of the calculations and dryer performance will occur during DBVS Operational Acceptance Testing (OAT), prior to start-up, wherein 16 batches of dried waste simulant (i.e., non-radioactive) are planned to be dried for the purpose of producing 2 full-scale ICV containers. 1.d. It should be kept in mind that the purpose for having an RD&D Permit is to optimize system performance and efficiency. Full-scale Bulk vitrification facilities can be run with multiple dryer/melt lines if necessary. Once DBVS operating data/experience is evaluated, DOE & CH2M HILL will provide Ecology information required to make a decision on treating the balance of the waste tanks' LAW. DBVS operating data will be used to	

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				recommend optimum dryer size/usage for a multiple melt train facility.	
2	IQRPE Report No. DR-009, Rev. 0; p. 7; Fig. 2 Note: This Comment was Transferred from Dryer RCR Part 2, Comment #2 (Aug 17, 2005)	• On P&ID, F-145579-33-0100, the rupture disk is "set at 5 psig". On p. G2-433 the design pressure of the rupture disk is given as 15 psig at 250°F. Please clarify what the design pressure means in this context. Can this one rupture disk be set at different pressures; if so, what is the lowest design pressure specification? The normal operating temp in the dryer is 140 °F so it appears that for adequate protection the specification of the rupture disk should state a temperature less than 140 °F instead of 250°F. Also review IQRPE evaluation in Section 2.2.3.1 in light of this comment. • Please explain your claim (by default) that the pressurization of the dryer by pluggage of the C-bed or other off gas equipment is an *incredible* scenario. Also, leaked steam at 250 °F when combined with the dryer contents at 140 °F will result in a temperature less than 250 °F. It appears that a rupture disk rated at 250 °F (instead of a lower temperature) would provide no protection in this case. This comment is also directed towards the IQRPE and his response is requested with reference to Section 2.2.3.1 of his report) • The rupture disk is shown leading to the Off gas Treatment System (OGTS) immediately downstream of the Waste Dryer Vacuum Off gas Condensate Tank, 33-D74-033. However, rupture disks are an important last resort safety item that should preferably be vented directly to the atmosphere. One scenario for pressurization of the dryer would be the plugging up of the off gas system causing the vacuum pump to be ineffective. In that situation it is not clear how the rupture disk would serve its purpose. If the off gas train were to plug up, it is conceivable that the dryer could get pressurized even with the vacuum pump running (with the discharge of the vacuum pump blocked it would not provide any function. Even if the rupture disk were to blow, the contents of the dryer would have no outlet. This could	X	The design pressure for the rupture disk is for the rupture disk housing. Per ASME the temperature of the rupture disk is defined as the temperature at which the disk is expected to burst. The only credible way of pressurizing the inside of the dryer would be by a leak of steam from the jacket directly into the dryer shell. The steam is 15 psig and 250 F. The steam would initially be superheated as it entered the dryer. Little cooling would be expected for a steam leak of such a size as to cause a rapid pressure increase. The burst temperature would be the temperature of the steam in the jacket. If steam leaks into dryer, head space of dryer will become 250 F rapidly, prior to dryer contents coming to equilibrium. If not, dryer will not need to vent. IQRPE report indicates rupture disk and off-gas pipe the rupture disk vents to is adequately sized. Rupture disk is vented into 6" diameter pipe routed to the off-gas system which will allow the rupture disk to perform its function while still providing containment	Closed 8/31/05

Item	Location in Document	Comment	Hold Point	Disposition (Provide justification if NOT accepted.)	Status
		result in a catastrophic breach in the dryer/off gas system. Has this scenario been evaluated? If it seems illogical to vent the rupture disk outlet inside the dryer enclosure, conceivably discharge from the rupture disk could be routed to a dedicated tank for subsequent pressure relief through a HEPA filter to the atmosphere. **2.a. Please refer to G2-590 (Rupture Disk Spec sheet) Line 18; Max. vacuum is given as 250 °F. This entry needs to be corrected.** **2.b. Moreover, the dryer is rated for 5 psig. Per routine Engineering practice it should be safeguarded against pressure surges at a pressure below 5 psig. It is unclear how the rupture disk as specified (5psig at 250°F) will provide a safety margin. Please have a safety engineer do a risk assessment of a pressurization event inside the dryer. In particular, evaluate the adequacy of the specification of the rupture disk and also its physical connection shown in P&ID F-145579-33-A-0100. Also please have the IQRPE reevaluate, and appropriately revise, the 1st para of Section 2.2.3.1 of his report, DR-009.**		for the hazardous material. If the rupture disk was vented to the dryer enclosure on an overpressure event, dried waste product would be released into the enclosure, resulting in significant personnel exposure to hazardous chemicals and radioactive material. If off-gas system is plugged, system will be shut-down. Several pressure indicators throughout the dryer off-gas treatment system and the main OGTS will provide operator indication that system is plugged and requires shut down. Need about 300 ft of off-gas piping to vent entire volume of dryer. About 500 ft available in DBVS OGTS. Vendor data sheet for rupture disk will be provided upon receipt of Dryer skid design. **2.a. Agreed. Line 18 will be changed to "Maximum Temp" at next revision of D-SP-006.** **2.b. The dryer design package was reviewed and evaluated by CH2M HILL industrial safety, nuclear safety and the design**	

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				authority along with Closure Projects Engineering. Further, the IQRPE has reviewed the adequacy of this portion of the design in his report. No change.	
3	IQRPE Report No. DR-009, Rev. 0; p. 9; 5th line Note: This Comment was Transferred from Dryer RCR Part 2, Comment # 3 (Aug 17, 2005)	The IQRPE report states there is one condenser in the off-gas line from the dryer. P&ID (F-145579-33- A-0101) shows there are two condensers in the off-gas line from the dryer. Please explain discrepancy. Please consider revising the nomenclature of 33-D10-032 ("Waste Dryer Vacuum off-gas **Condenser**") in the Dryer Vacuum P&ID, F-145579-33-A-0101. **3.a. You state that 33-D10-032 acts to cool the water. Please explain why the unit is called a "condenser".**		Strictly speaking, 33-D10-005 acts to condense the dryer *off-gas*. 33-D10-032 acts to cool the water for the liquid seal on the vacuum pump. The 3rd sentence on p. 9 is accurate as written. Accurate as written. No change necessary **3.a. The description as stated is accurate; however, to accommodate the review comment, the equipment title will be changed to "Liquid Seal Heat Exchanger" and will also change the symbol used on the P&ID to match.**	Closed 8/31/05
4	IQRPE Report No. DR-009, Rev. 0; p. 17; Fig. 4	How accurate is the dryer load cell readings given the vibration in the dryer body due to the mixer. This dryer weight is crucial to determine the % moisture and thereby the end point of drying. Is the dryer on load cells? How much experience does the dryer manufacturer	**X**	Materials loaded into the dryer (soil, waste, additives) are primarily controlled and metered in via the material input systems. Load cells on the soil and glass former impingement tanks provide	Closed 8/31/05

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	Note: This Comment was Transferred from Dryer RCR Part 2; Comment # 8 (Aug 17, 2005)	have in drying slurries that behave like Hanford waste? Please provide specific examples of similar industrial slurries that are being successfully processed in the full scale dryer. For processing of materials critically sensitive to final % moisture, is the method described to determine the end point of drying commonly used in industry (i.e. correlation with temperature of dryer contents)? How critical is it that the final moisture be controlled below 1%? **4.a. Please explain what is the role of Phelps-Dodge Corp? How is their experience being applied to enhance dryer control?** **4.b. Please substantiate via relevant documentation.** **4.c. How many "dry-batch test runs at the pilot scale" were done? DBVS.TRPT.002 describes only one.** **4.d. What fraction of this test remained unfinished?** **4.e. Is resumption of pilot tests planned? If so, when?**		a direct reading of how much material is discharged to the dryer. Flow meters measure the flow rate to and from the dryer and the difference is used to compute the amount of waste added to the dryer. % moisture is determined via dryer product temperature measurements. The time/temperature profile is used to determine the drying end-point. Following the completion of waste addition, drying continues until the dryer bed temperature begins to increase. The Dryer is on load cells. Load cells correlate material additions to the dryer. Waste stimulant testing for DBVS, CH-TRUM projects comprise vendor experience in drying Hanford-like wastes. The Phelps-Dodge Corp. has experience drying wastes sensitive to final % moisture. Pilot scale testing showed that it is critical that product moisture content is below 1 wt% moisture before adding glass former materials (ZrO_2) so as to prevent scaling/caking on the dryer walls. It is also critical to keep the dryer product below 3 wt% moisture throughout the	

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				drying cycle to prevent caking of the dryer product. No amount of caking on walls is desirable since it is difficult to account for all materials put in to dryer in such a situation. Further, excessive caking could lead to a Dryer upset condition. No caking / product build-up was observed during dry-batch test runs at pilot scale. During start-up of DBVS, the full-scale dryer will be tested (non-rad waste simulants) to correlate dryer product temperature with product moisture to characterize operation of full-scale dryer. **4.a. Phelps Dodge Corp. has no role in the DBVS Project, nor will they. Their name was simply provided as information to respond to previous Ecology request on other users of this dryer.** **4.b. DBVS TRPT.002, Run 2-2 concludes that the dry batch method works at pilot scale and can be controlled to achieve**	

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				product moisture between 0.5 and 2.5 wt.%. 4.c. 3 tests were conducted w/ a 5L unit to determine simulant properties during the drying process and to develop process parameters for the 130L scale testing. One pilot scale test run was conducted w/ the 130 L unit. 4.d. The test w/ the 130L unit was completed. Data gathered was deemed sufficient. There was some S-109 simulant that was not consumed during the test. 4.e. No further pilot scale testing will be conducted. As previously stated, validation of the calculations and dryer performance will occur during DBVS Operational Acceptance Testing (OAT), prior to start-up, wherein 16 batches of dried waste simulant (i.e., non-radioactive) are planned to be dried for the purpose of	

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				producing 2 full-scale ICV containers.	
5	Section 2.2.7.4, 3rd para, last sentence. Also, **Section 2.2.6 p. 2-17, 2nd para** Note: This Comment was Transferred from Dryer RCR Part 2; Comment # 13 (Aug 17, 2005)	The following comments relate to the "starting and stopping addition of material to the dryer" and are based on the documents: Engineering Scale In-container Vitrification Test Results (Final Report) August 2003; and "DBVS: Dryer Test Report August 2004". These are reports on development tests performed on bench and pilot scale dryers using Hanford soil and S-109 simulant. I request that the IQRPE be provided these two reports for his review. These reports form a basis for the Dryer Design package. **The former document's (August 2003) comments are**: Table 4.1 summarizes the results of 9 tests done on a dryer with 5-L capacity; four tests used the wet batch method while in the remaining five the simulant was added in increments. Some problems encountered (pluggage at dryer ends and heavy deposition on the baghouse filter, caking on shaft, heavy paste product) during these tests would prevent proper operation in full scale. From this document it appears that further tests were not done during that campaign to indicate that these problems can be solved. *My recommendation is that developmental tests on the pilot scale dryer should continue.* I reiterate my considerable concern that instead of establishing parametric benchmarks and gaining confidence in repeatability at the pilot scale, CHG and ORP have chosen to do this at considerable greater expense and risk at the DBVS. Below, a comment response, "Vendor *information and experience indicates that 130L test results are scaleable to 10,000L operation*", supports my assertion of the need and usefulness of bench scale dryer data. **The latter document (Aug 2004) comments are**: *My copy of this report does not have appendices that give details of the tests performed. An electronic copy of these is requested.* Thank you for providing the electronic copy of this report and Appendices. In Appendix C3, the Littleford Day, Inc. Summary Report, strongly recommends	X	Test reports do not address IQRPE review scope under the WAC. No need to send IQRPE test reports. Development tests were conducted after the August 2003 tests to overcome the problems experienced in the 5L test dryer. Agree that there is risk and potential for greater expense. DBVS project avoids the risk by maximizing use of the pilot-scale test data we have and testing the dryer during DBVS start-up to correlate desired product moisture to product temperature with an off-line moisture analyzer. A copy of the report was provided informally. Yes dry v. wet batch has been discussed with the vendor.	Closed 8/31/05

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		the wet batch method. The gist of this report is that besides giving a higher throughput, the operation would be considerably easier to control in "wet" batch. Has AMEC/CHG's choice of the "dry" method been discussed with Littleford; are they in consensus? Please clarify the reasons for the choice of the dry method; the bases for the reasons given in the Test Report are not clear. In Fig 4-3 please explain what plow heating is? In contrast to your calculation method, please note that Littleford Day in their evaluation of the pilot tests (Appendix C) take no credit for plow power . Please explain this disparity. Given the uncertain and varying nature of Hanford tank wastes it appears dryer data developed at the engineering scale would be of much value for DBVS. What was the highest ratio of dry waste to (soil + additives) achieved in the August 2004 tests. What waste loading, i.e. % Na_2O in glass would this dried feed equate to? Have any dryer tests been performed since August 2004? No. If not, why was the testing terminated? "Cost and schedule" at the engineering scale appear to be the attractions not the "constraints". ??? It is disconcerting that no complete run was performed at the 130 L scale and a crucial piece of equipment, the DBVS dryer, is being scaled up based on extrapolation of only one incomplete 130 L run. Found enough data to be confident that we can run tests at 10,000 L during start-up. Per the Executive Summary of the report of the August 2004 tests, maintenance needs will likely increase due to increased inlet valve cycling resulting from greatly increased number of increment additions of waste. *Prevention of erosion of internal components needs development work.* Section 1.1, 2nd para; *Please provide a copy of the "DBVS: Interim Dryer Test Report April 2004, A006.TRPT.001, Rev. 0"* Fouling of the dryer walls, blockage and buildup of dryer contents at the ends has occurred during bench and pilot testing and is possible in full scale operation. *How often is it expected that hands on maintenance will be required inside the full scale dryer. What difficulties are foreseen in adequately decontaminating the dryer to allow entry?*		Littleford-Day recommendation for wet-batch is driven by most efficient processing time; however, wet batch is inherently more risky in terms of creating and recovering from an upset condition. Recovery from upset condition in dry-batch is inherently less risky. Plow heating is the amount of power or heat energy put into the dryed waste mixture by way of mechanical agitation of material being mixed. Littleford Day calc aimed at conservative steam supply sizing, so this calc ignores plow power. The waste loading for "Run 2-2-Terminal" is equivalent to 20 wt% Na_2O in glass for an 8.3 hr run. Total waste loading for Run 2-2 is equivalent to ~ 14 wt% Na_2O for the 6.58 hrs duration of the test. Currently planned work. See response to #9 above. Latest Dryer Test report is DBVS.TRPT.002, Rev. 0. A copy of the report will be provided informally.	

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		Section 2.6, Table 2.5; There was only one Run (#2-2) that was done using the dry batch method of dryer operation. *What was the increment size and frequency of simulant addition in this Run?* Section 4.1.1, Item 4; *For the 10,000 L dryer, please confirm that the clearance between the dryer walls and the plough is ¼ "as stated.* Section 4.1.2 Item 5; *The maximum sustainable feed rate should be determined by pilot testing as this information would greatly facilitate scale up; it is stated that this was not done due to time constraints.* Section 4.2 item 5 states that a "change in the motor specifications would be required to accommodate the dry-batch method." *Does the dryer planned to be used have a motor with the revised specifications?* Section 4.2, Item 6 states, "Process control for the dry batch will require control over a narrow range throughout the process." To aid proper scale up, "temperature ranges and power curves" should be evaluated in the pilot scale and confirmed in the full scale. This appears to be more efficacious as *it is certainly easier to recover from an unsuccessful run in small size equipment. The stated "integrated testing" is not required to evaluate the drying process only.* The narrow (1%-3%) moisture range required for trouble free dryer operation concerns me. It appears that, during operations, measuring moisture content by testing dryer samples is not feasible and the control parameters that will be used are power and temperature profiles. *These profiles do not appear to be reproducible from one run to another to the accuracy required.* Is the dryer temperature an adequate indication of the end point? I'm unable to see the correlation between % Moisture and Temperature in Fig 3-24. *Further pilot scale testing to develop more data on control parameters needs to be done.* *Is the diameter to length ratio the same for both the 130 L and the 10,000 L dryers?* The surface area available per unit mass of the dryer contents is an important factor in scale up. Assuming the heat transfer coefficients and temperature difference (between the dryer wall and the contents) are the same for both dryers the ratios of surface areas will determine the throughput possible		Hands-on maintenance may be required once during the DBVS operational campaign for plow replacement. One concept for decon'ing the dryer is to run a batch of clean soil through the dryer and scour the inside dyer surfaces with clean soil. See DBVS-TRPT-002, p. 3-19, Table 3-1 for feed rate of Run 2-2. See D-SP-001, Section 3.3.1.1.8 for specified plow-wall clearance. The ¼" buildup on the dryer wall was a result of running the dryer "wet". DBVS intends to operate the dryer in dry-batch mode. This buildup was not observed in the dry-batch mode. Pilot scale showed that max sustainable feed rate was crept up on and achieved during the 4.33 – 6.58 hr interval, but not the entire dryer cycle time. Note that max sustainable feed rate achieved meets DBVS processing rate. Motor for DBVS dryer is capable at running at 45 rpm or at 90 rpm (standard speed), which is recommended for dry batch operation—see D-SP-001, Section 3.2.1.2. See above response on product temperature moisture correlation on full-scale dryer testing for DBVS. Dryer run-	

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		in the full scale dryer. *Another important unknown that does not appear to have been evaluated during the pilot tests is the periodicity and amount of each addition of the simulant; please address this.* Section 4.2 item 10; *It states that "higher shaft speed" is required in the dry batch method as compared to the wet-batch method; why is this so?* As stated in Section 2.3.2.1, the dry batch uses a full standard speed (160 rpm). *Has lower speeds been explored for the dry batch, and if so, what were the difficulties faced?* Section 4.2 item 12; The S-109 simulant used in the tests contained 2.5% solids. The actual waste to be delivered from S-109 to the DBVS is expected to contain negligible solids. *Please reconcile the difference.* Section 4.4, 2nd para; *Please provide the latest revision of the "Process Design Criteria" document. Also please provide a copy of "DBVS : Interim Dryer Test Report, April 2004; this is listed in Reference section 7.0 of RPP-24544 Rev 1a, (p. H2-39).* Has this document been provided to Ecology? Section 4.6, last sentence; In the dry-batch method the % moisture in the dryer is critical and, per Section 4.7 Item 4, is to be maintained between 1% and 3%. *Can temperature and power curves be used to accurately determine the boundaries of the narrow range of operating parameters?* In my comment under Section 4.2, Item 6 above, power demand and temperature need to be controlled within a narrow range. *Why then is it stated here that "Defining the relationship between power demand and dryness is not necessary with the current dry-batch process recommendation".* I have several questions on DBVS.TRPT.002 that could best be answered in a meeting. Please arrange this. Section 4.9 2nd para; When will the results of the PNNL testing with low-activity waste simulant be available. *Can we get a copy of this report?* **5.a. What is required to increase the IQRPE's review scope to include an independent evaluation of pilot test results?** **5.b. What will AMEC/CHG do for "maximizing use of the pilot scale**		time will also be a parameter that will determine cycle end-point. More pilot scale testing would confirm test results. **Cost and schedule constraints do not allow for this however.** **Vendor information and experience indicates that 130L test results are scaleable to 10,000L operation.** It is envisioned that the waste addition rate in the DBVS dryer will be controlled via dryer product temperature as done in the pilot scale tests (see Section 2.4.2.1). Will provide A006.TRPT.001. Higher shaft speeds in dry batch mode will keep the dry material "fluid" throughout the drying process, which is not necessary for wet batch drying. 2.5% solids in the stimulant will not affect the dryer test results. Requested references for Section 4.4 were provided to Ecology staff. Temperature can be more readily correlated to product moisture. The plow power demand will indicate if a pasty or stiff substance is forming in the dryer. Meeting on 8/16/05 addressed all questions on TRPT.002. See response to #9 above.	

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		test data we have?" The pilot scale test data does not seem to have been used to support your design basis. 5.c. Besides prompting you to select the dry batch method over the wet batch, what aspect of the test data has been used? 5.d. Please clarify and substantiate, "Found enough data to be confident that we can run tests at 10,000 L during start-up." 5.e How far beyond start-up can this data be used? 5.f. Please explain and clarify, "Note that max sustainable feed rate achieved meets DBVS processing rate." It is not clear from the data tabulated on p. C1-5 (Appendix) and Figure 3-24 in DBVS.TRPT.002		5.a. The RD&D Permit does not include conditions, nor should it under WAC 173-303-640, to require a review or independent evaluation of pilot test results. 5.b. DOE/CH2M HILL, as co-permittees for the DBVS RD&D Permit strongly disagree with this comment. Pilot scale test data was used to support our design basis in selecting the dry-batch method for drying. The wet batch method drawbacks include caking on dryer surfaces, which lead to greater exposure risks to facility worker, additional operational steps and wastes to deal with at the end of a batch drying cycle/risk of leaving ZrO_2 in dryer for next batch, material balance uncertainties and inherent potential for creating dryer upset condition (e.g., dryer	

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				seizing). The greatest advantage to the dry-batch method is that it allows for incremental addition of liquid tank waste to a dry medium that will be quickly sorbed and not pose the constraints and problems of the wet-batch method. 5.c. The reviewer is referred to Section 4.2 of DBVS.TRPT.002 for a complete list of recommendations that came out of the test. A short list includes: Dry time; Timing of glass former addition; Effectiveness of an antifoaming agent. 5.d. DBVS.TRPT.002, Section 3.2, Dry Batch (Test Results) provides data. 5.e. This data will not be needed beyond start-up. The 10,000L DBVS dryer	

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				will be available during facility acceptance testing for testing with waste simulants (non-radioactive waste). A total of 16 batches of dried waste stimulant are planned prior to start-up of the DBVS facility. 5.f. Referral to data reported in 3rd interval (4.33 – 6.58 hrs), a sustainable condensate rate of 28.8 lbs/hr results in a dry time of 8.3 hrs for Run 2-2 (see Figure 4-6, DBVS.TRPT.002, for scale-up calculation for this time interval).	

REVIEW COMMENT RECORD (RCR)

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	3. Project No.	4. Page	1 of 8

5. Document Number(s)/Title(s)	6. Program/Project/Building Number	7. Reviewers	8. Organization/Group	9. Location/Phone
DBVS Waste Dryer Package		Robbie Biyani	Ecology	372-7884

17. Comment Submittal Approval:	10. Agreement with indicated comment disposition(s)	11. CLOSED
Organization Manager (Optional)	Reviewer/Point of Contract	Reviewer/Point of Contact
	Date	Date
	Author/Originator	Author/Originator

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
1.	p. 2-13, Section 2.2.1.1 1st para, 5th sentence; Provide sketch of mixing profiles (movement of material) within the dryer. If the mixing paddles move material to the center, what prevents agglomeration at this location and uneven distribution of material along the length of the dryer? Please consider rewording, "The arrangement of the plows in the dryer is such that the waste is mixed by directing it from the ends of the dryer to the center."		The key to success in Littleford Day, Inc. mixers, is the unique action created by the movement of the mixing elements that produce intense, but gentle intermingling of materials of the mix in a mechanically fluidized bed. The mixing elements are arranged at intervals on the mixer shaft and their size, number, arrangement, geometric shape, and peripheral speed are designed to force the product into appropriate components of axial and radial motion. Will reword text in Section 2.2.1.1 as requested upon incorporation of all RCRA Design Packages in RPP-24544.	Closed
2.	p. 2-16, 1st para; See C4 of P&ID F-145579-33-A-0101, the off gas flow past the condensate tank 33-D74-015, is confusing. The flow path of the liquid used to seal the vacuum pump is unclear. The discharge of liquid from the vacuum pump seal to the tank 33-D74-033 is not shown.	X	The dryer condensate "drops-out" of condenser 33-D10-005 and is collected in condensate tank 33-D74-015. Gas flow continues through the head space of 33-D74-015 to the inlet of the vacuum pump. Discharge of the vacuum pump is routed to a gas-liquid separation tank, 33-D74-033, where the liquid that supplies the seal for the vacuum pump is cooled and routed back to the pump for the liquid seal. Discharge is via main vacuum pump outlet--VOG-33-0142	Closed
3.	p. 2-16, 1st para; it is not clear how containment and leak detection requirements per WAC-173-303-640(4) are met within the DCRS enclosure. Please clarify.		Secondary containment and leak detection is satisfied by the stainless steel floor pan in the bottom of the Dryer ISO container and leak detectors (LSH-018) in the low-point of the floor pan—see Zone A7, 33-A-0101 and discussion in Section 2.2.8.	Closed

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
4.	p. 2-17, 2nd para, 1st sentence; provide summary of test results; have the problems encountered been resolved and overcome?	X	Yes, problems encountered during initial small-scale dryer testing have been resolved and overcome. The test results are summarized by the 4th sentence in this paragraph—the dry batch method is the operational baseline with the lowest risk of seizing the dryer.	Closed
5.	p. 2-18, Section 2.2.7.1, 1st para, The end of drying is achieved by reaching a "target temperature". Is this a commonly used method of operating such dryers? Why is measurement of moisture content (by sampling of dryer contents) "not practical for this application." What is the expected drying cycle time? Also see comment # 18. A companion RCR lists questions generated by DBVS.TRPT.002.		Dried radioactive waste handling for data on the moisture content of dried waste product is not ALARA. Dryer test data that correlates moisture content of simulated waste materials to product temperature, vessel pressure and cycle time can be used and was used in dryer pilot scale testing (see DBVS-TRPT-002—copy previously provided). Expected drying cycle time is 8 hrs/dryer batch (~ 7,000 kg of dried waste material/glass formers). See companion RCR.	Closed
6.	p. 2-18, section 2.2.7.1, 2nd para; Rather than being added after waste drying, has addition of zirconium and boron oxides during waste introduction been considered?		Comment withdrawn	Closed
7.	p. 2-18, Section 2.2.7.2, 2nd para; Appendix E has not been provided.		Comment withdrawn	Closed
8.	p. 2-19, Section 2.2.7.3, 1st para, 2nd sentence; what is the smallest particulate size that can be collected in the sintered metal filter?		SMF will capture 99.97% of particles at 0.6 microns and above. See 143643-D-DS-001.1, attached to D-SP-001.	Closed
9.	p. 2-19, Section 2.2.7.4, 5th sentence; what is "spherical disk valves?"		Comment withdrawn	Closed
10.	p. 2-24, Section 2.2.8, 1st para; Describe where the leaked waste is transported to by the drain line? Provide the calculation to show how the liquid height of 8" is reached, as well as 86 gal (next para). Appendix A2 is missing. Calc. No. 145579-D-CA-030 does not provide information on the assumptions of where and how the leak might originate or the time to detect the leak. If only double contained HIHTLs are used where is the leak point?		The destination of leaked waste is condition dependent. Nominally, the drain line is connected to CP-03 on the Waste Transfer Pump Skid. The pump skid will be valved to either send the waste directly back to tank farms or to the DBVS Liquid Waste Staging Tanks. A liquid height of 8" is not reached; given the standard dimensions of an ISO container door, this is the maximum height of a containment pan in an ISO container (Note: capacity is ~ 2,680 gal for Dryer ISO container). 86 gal. is the worst case calculated value of waste required to trip the leak detector LSH-018. The time to detect this leak would be dependent on a leak rate, e.g., A leak rate of 0.06 gallons per minute would be detected within 24 hours. The leak calculation is independent of leak location inside the Dryer ISO enclosure—the calculation conservatively assumes	Closed

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
			that 0.25" of liquid covers the entire floor pan before draining to the sump. The reference to HIHTLs pertain to piping runs outside the Dryer ISO enclosure.	
11.	p. 2-25, 1st para; Identify the locations where carbon steel may be used for piping.		This detail will be provided by the DCRS Skid vendor. D-SP-001 and -006 require all piping used to be fabricated, inspected, examined and tested in accordance with ASME B31.3. Stainless or carbon steel must be a listed component as stated in ASME B31.3.	Closed
12.	p. 2-25, 2nd para; Have corrosion measurements been made during bench-scale testing? Will an erosion estimate be obtained for the inlet lines to the dryer?		Corrosion measurements have not yet been made. Planned for next FY prior to system start-up (test 33B – E feed prep is planned to be conducted in bench scale dryer). The erosion estimate & allowance will be determined by the fabricator of the inlet lines to the dryer based on data provided to him regarding the properties of the soil/additives to be used.	Closed
13.	Calc. No. 145579-A-CA-004, p. 5, Section 1, 1st para; How is the target figure of 0.76 gpm calculated? Please provide the connection between this number and the 10 gpm treatment rate envisioned during the MAI(C3T) effort. Granted that the DBVS processing rate is not designed to correlate to a full-scale facility; what is the numerical basis for the 0.76 gpm processing rate?	X	The target processing rate is calculated based on the demonstration facility being able to process approximately 200 kgal of S-109 saltcake waste in less than 24 months, of which approximately 4 months time is allowed for facility start-up and D&D. Although there is no direct connection between the DBVS average processing rate (which is based on a limited 2-year operational life) and the full scale facility, 0.76 gpm will allow for operating and processing data sufficient to demonstrate the Bulk Vitrification process. See above explanation for processing rate numerical justification. Note that 0.76 gpm is referenced to the feed into the DBVS facility, which is 5M Na concentration; in-situ S-109 saltcake + interstitial liquids is approximately 16.8 M Na.	Closed
14.	p.7 of Calculation 145579-A-CA-004; Section 5.1 last para, 1st sentence indicates that there are "no calculations or formulae" in Spreadsheets # 2, 3, and 4. To better understand process flows, verify the assumptions, and spot check the formulae and calculations, it is imperative that the Excel spreadsheet presented in the Full DBVS Process Flow Diagram be provided to Ecology. Please provide this otherwise it will take longer to complete the review. It is important that Ecology verify the accuracy of mass balance calculations for the Bulk Vit process. I understand that the main	X	Please see evidence of formal calculation review and checking performed and documented by WB Craft included in the design package; see also evidence that this calculation was reviewed and accepted by CH2M HILL process engineering. The level of detail of the reviews performed is appropriate. A copy of the PDC Rev. 0F, April 8, 2005, was provided 8/16/05.	Closed

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
	calculations were done on the IDEAS software to which we do not have access. Therefore in lieu of the spreadsheets that contain formulas, an updated version of the "Process Design Criteria" document may be submitted, including the source and Basis Bibliography. Questions relating to the mass balance would probably be more relevant to the ICV Box and Off Gas design packages. However, until the bases information stated above is not received it will not be feasible to review and evaluate the material flows.			
15.	p. G2-425; Figure 3-1 shows dryer condensate is a secondary waste that is sent for Treatment. Has reuse of this waste condensate stream been evaluated for retrieval of S-109 waste?		The DBVS testing will provide process information that will support the evaluation of bulk vitrification production facility dryer condensates for feasibility of reuse in the waste retrieval process.	Closed
16.	p. G2-382, Table 3-3; Waste is received directly into the dryer and processed. The waste does not appear to be staged at the Dryer as implied by the heading of Table 3-3.		Assume comment applies to Table 3-3 of D-SP-006 on p. G2-445. Waste is staged in the DBVS waste receipt tanks. Due to storage time in these tanks, waste temperature, as sent to the dryer, can differ from the waste as received from S-109.	Closed
17.	The dryer heat load calculation, 145579-D-CA-003; • The resistance to heat transfer, defined by heat transfer coefficients, has not been accounted for. • Steady state is never reached in the dryer because continual small additions of waste are planned to be made. Therefore the rate of water evaporation will continuously vary. Both these factors will limit the maximum amount of heat that can be transferred to the wet particle and I expect the overall time averaged production rate will be considerably lower than expected. This has not been taken into consideration in the calculation in the Scenarios described in Section 5. The assumption in your calculations (that whatever heat is applied to the wall of the dryer will be transferred to the dryer contents) is simplistic. Please refer to Appendix C2, Page C2-7, to see how Littleford Day, Inc. has determined the U-factor. Results (U-factors) from the pilot tests are applied to determine the time required for	X	See Assumption #2. The energy required to evaporate the water dominates and is about 10x the heat transferred to a fluidized bed of soil in the dryer via convection. The dryer will be operated such that the bleed fed into the dryer is added at a constant rate and boiled-off at a constant rate. Pilot-scale testing proved that this can be done and full-scale commissioning testing will be performed to prove this out prior to facility start-up. The total operating efficiency for DBVS is 70%. Downtime while soil/waste & additives are in the dryer would be considered an abnormal event. Dryer maintenance/troubleshooting would be performed during DBVS facility downtime. The three cases treated are meant to explore the possibilities of running the dryer differently than the baseline case. The chiller and boiler units selected are adequate for making the baseline operating case work. AMEC document A-DC-002 is an AMEC document that has been checked by CH2M HILL, but not accepted via the formal calculation acceptance process. The latest revision will be provided informally, when it becomes available.	Closed

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
	drying in the DBVS. Please reconcile and revise your processing time determinations in DBVS.TRPT.002, Rev. 0 . In Appendix C3, Littleford Day in their test report Summary state the dry batch method has "... a production rate at approximately one third (1/3) of the wet batch method". Also, what Total Operating Efficiency has been assumed for the dryer? Is there downtime when either soil or waste or additives are added to the dryer? Please explain your assumption #1; what is the basis for choosing the three cases. Please provide copy of Ref 1 on page 4 of this calculation.		Heat transfer coefficient used in Litterford calcs is used for sizing steam supplies for their customer's dryer. It is intended to be a conservative estimate of needed steam supply. The DBVS dryer, as configured in the design package, will provide sufficient data to support design of a production facility. Confirmation of the estimated cycle time for producing an ICV box will be done during DBVS start-up testing and DBVS test campaigns. Information on DBVS throughput will be provided in DBVS Campaign Reports.	
18.	Roughly how does the DBVS energy requirement for the dryer, compare to that of the vitrification container?		D-CA-003 indicates that the dryer requires 1.7 MBTU/hr/dryer batch or 498 kW/dryer batch to produce a dried waste product meeting specification. At 8 dryer batches/ICV and 8 hrs/dryer batch, 31.9 MW-hrs/ICV is consumed. The DBVS electrical system is sized for an electrical power consumption of 940 kW. Each ICV has a melt time of 139 hrs, or 131 MW-hrs/ICV. Note however that recent large-scale tests conducted (i.e., Test 38A) show a peak power consumption of ~ 700 kW; this would equate to ~ 97 MW-hrs/ICV.	Closed
19.	Confirm if hydraulic oil tank chilled water heat exchanger P&ID F-145579-33-A-0101 (D5-D6) is co-current as shown; or is it counter current? Please confirm that this heat exchanger as purchased/specified is co-current. Why is the recirculation line that goes through the Filter 33-NO2-110 (see C5) shown as originating at the Pump 33-D61-108 rather than at line 1-OH-33-0211?		Shown as co-current. 33-D61-108 pumps cooling fluid to the hydraulic motor case on the dryer hydraulic motor. Line shown is just a bleed off the pump being routed back to the heat exchanger/reservoir via the wash plate solenoid control for hydraulic pump when not turning the dryer shaft. Vendor drawings for dryer HPU will clarify. Heat exchanger is counter current. Shown incorrectly on P&ID. We will update the P&ID with latest vendor information when available.	Closed
20.	Is there a viewing window/sight glass or camera in the dryer that is already on site and is planned to be used [P&ID145579-33-A-0100 (D4)]; if so, what is the visibility range? Is the discharge port visible by these means? This feature would be useful in the event the discharge port area plugs up. Is there a sight glass on the wall of the dryer? Please provide information on the CCTV when available.		CCTV is planned for Dryer ISO container. Vendor info on the camera has not yet been received. Plugging of the discharge port will not necessarily be viewable from the outside of the dryer. Plugging will be avoided via continuous agitation of the dryer product while emptying the dryer. Sight glass and light port are located on top of manway. View of discharge port may be partially shielded / shadowed by 14"	Closed

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			diameter shaft. Can provide requested info on the CCTV when available.	
21.	Is condensate pump 33-D61-016 (C3) operated batch wise? How frequently is it turned on? Should the Valve 33-V-030 and -083 be normally closed to allow accumulation of condensate in the Condensate Tanks ? If Valve 33-V-030 and -083 are always open, it is not clear how the condensate removal system works. Please explain.		Condensate pump is operated batch-wise. It operates between a low level switch that is set at 8" above the bottom of the tank (~ 100 gal. of liquid) and a high level switch that is set at 6" below the top of the tank (~ 470 gal. of liquid). Average condensate generation rate is ~ 3 gpm over an 8 hr dryer batch cycle time. Condensate pump 33-D61-016 is a 30 gpm pump. This means the pump can turn on & off a maximum of 4 times/dryer batch. Condensate/liquid from the ring seal on the vacuum pump is continuously available to the pump through 33-V-030 and -083. The pump switches on at LAH-107/LAH-131. LAL-106 switches the pump off. Pump is not always on. o.k. if -083 is left open—LV-131 is controlled by the level switch. DAA, DAB (LSH, LSL) interlocks with the motor control on the pump. O.k. for V-030 to be open with check-valve upstream.	Closed
22.	P&ID # F-145579-33-A-0101 (C2) no provision for a flush out drain connection is shown for Tank 33-D74-033 (as is shown for Tank 33-D74-015).		Flush-out water provided through LV-130, drain through 33-V-083.	Closed
23.	The air inlet to the dryer for a steady sweep is shown through the HEPA filter 33-NO2-017 in P&ID # F-145579-33-A-0100 (E4 –E5). Why is the valve between HEPA and the dryer shown NC?	X	The dryer does not have sweep air, rather it operates at a vacuum of 26 inches of Hg. This valve opens to relieve vacuum when needed prior to discharge of the dried waste. .	Closed
24.	Does the Sintered Metal Filter have a steam jacket or is it just insulated?		Steam jacket.	Closed
25.	p. G2-11, 2nd to last bullet; Please provide Test Plan A006.TPLN.001 (bench and pilot scale testing plan).		See Appendix H2, p. H2-15. DBVS.TPLN.002 is provided in the design report; it was previously released under the document number A006.TPLN.001.	Closed
26.	p. G2-19, last sentence of section 3.2.1.2; please provide Data Sheet 143643-D-DS-001.1 (Characteristics and requirements for the dryer and condensate recovery system).	X	See data sheet attached to D-SP-001 in Appendix G2, pg. G2-67.	Closed

REVIEW COMMENT RECORD (RCR)

1.	2. Review No.
3. Project No. N/A	4. Page 7 of 8

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
27.	p. G2-24 section 3.3.1.1.8; We've been given to understand that now the dryer is being provided by the Buyer (CHG). In that case when will the need for brazed plow head scrapers be determined.		Comment withdrawn	Closed
28.	p. G2-26item d.; text indicates four ports for liquid waste charging. P&ID # F-145579-32-A-0100 (D4-D5) shows only three ports. Confirm if the dryer that will be used meets the meets the specifications in 3.3.1.1		Correct. Three 4" ports are being used for liquid waste discharge into the dryer. The other 4" port is being used for SMF dust recycle to the dryer. This configuration will adequately distribute liquid waste throughout the chamber in the dry-batch operational mode and allow for SMF dust recycle to the dryer. Spec change warranted on next logical revision of spec.	Closed
29.	p. G2-27; The Chiller capacity is given as 207 tons but there is no entry for the Fluid flow rate.		Comment withdrawn	Closed
30.	Are there ports for spray nozzles to supply water or other fluid to flush out the dryer; and an outlet to remove the flush water?	X	Rinse and drain ports are provided on dryer, see 33-A-0100, Zone D6 & 3; and C5 respectively; also specified in D-SP-001, Section 3.3.1.1.9.k and j.	Closed
31.	p. G2-423, Section 3.1, 2nd para; Please provide the design of the "hemispherical valve" that will be used to discharge dried waste from the dryer.		The design is provided at pg. H2-110.	Closed
32.	p. G2-425, Figure 3-1; The Steam condensate pump is shown in the steam inflow line instead of the outflow. The Push Button Stations shown appear to be operated from inside the DCRS enclosure. What are the requirements for entry into the DCRS enclosure?		Steam condensate pump should be shown on the outflow side of the steam loop. Will revise Figure 3-1 at next revision of D-SP-006. Note that DBVS-SK-P004 shows the pump correctly on the outflow side. Push button stations would be operated in maintenance mode only, within site of the equipment being operated. Normal operations would not be conducted from the pushbutton stations. The DCRS is not entered during normal operations.	Closed
33.	p. G2-427, Table 3-1; CP-301 and CP-302; Within the DCRS enclosure is there any section of pipe carrying waste solution that is not double contained? If so, secondary containment of liquid waste must be provided along with leak detection and removal capability at a sump.		Secondary containment is provided by the Dryer ISO container. See disposition to Comment #10 for description of secondary containment for piping in Dryer enclosure.	Closed
34.	p. G2-429, Table 3-1, Secondary containment method/design for the		The sketch is provided in Appendix A of the specification on pg. G2-573.	Closed

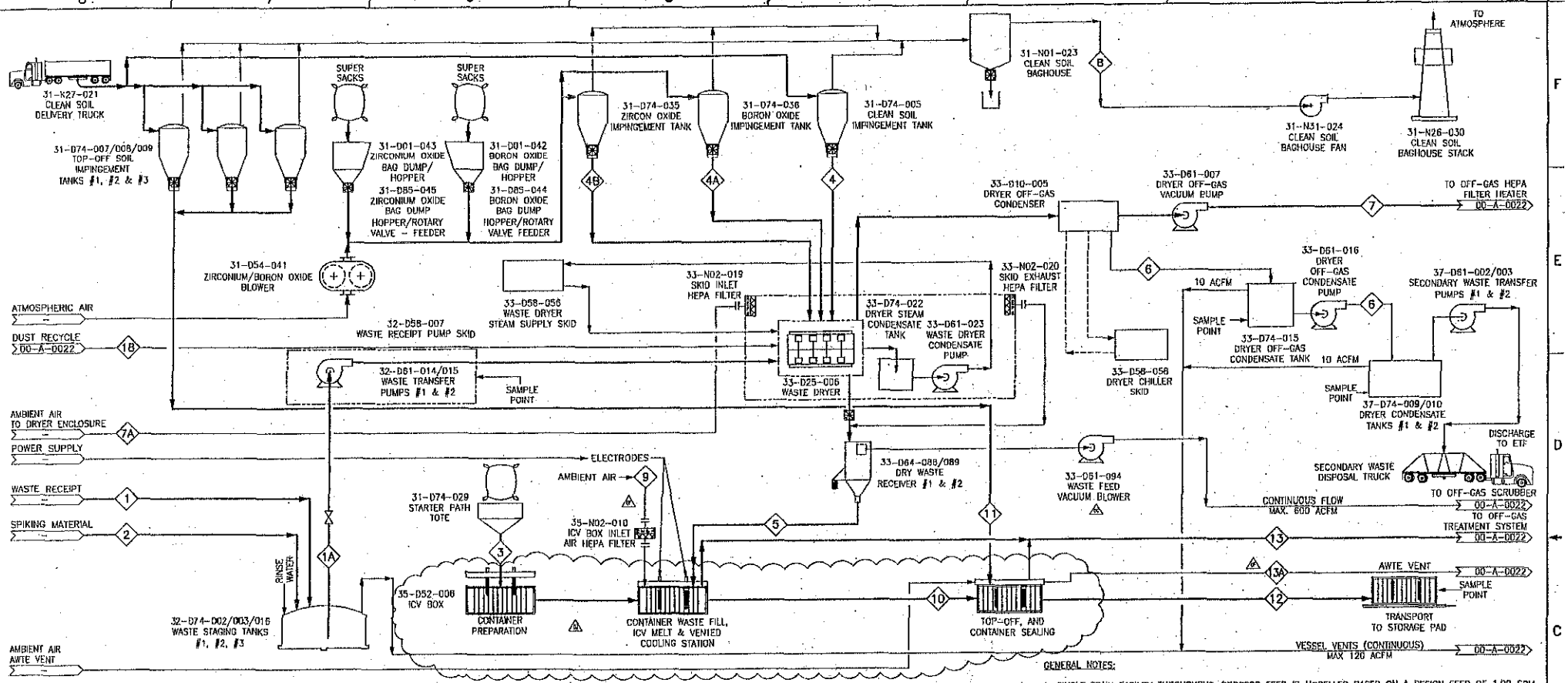
REVIEW COMMENT RECORD (RCR)

1.	2. Review No.
3. Project No. N/A	4. Page 8 of 8

12. Item	13. Comment(s)/Discrepancy(s) (Provide technical justification for the comment and detailed recommendation of the action required to correct/resolve the discrepancy/problem indicated.)	14. Reviewer Concurrence Required	15. Disposition (Provide justification if NOT accepted.)	16. Status
	filter dust at CP-315 is unclear because Appendix A containing Sketch DBVS-SK-P004 was not found.			
35.	p. G2-433 Table 3-1, the Rupture Disk "Maximum Normal Condition" is given as 5 psig. The Dwg 145579-33-A-0100 specifies that the rupture disk is set at 5 psig. It would appear that there should be an alarm (for operator intervention) at the maximum normal pressure and the disk rupturing point should be specified as being higher than the alarm point. Also, since the "normal" operating dryer pressure is 26" vacuum, will the rupture disk be sound at this negative pressure? For disposition refer to comment #2 in the companion RCR of the Dryer Design Package (both comments are similar).		33-PAH-029 provides the capability to alarm at less than 5 psig (see Zone D3). See p. G2-590 for rupture disk data sheet. Vacuum pressure specified at -26 in. Hg @ 250 deg. Rupture disks that provide positive 5 psi protection for vessels that operate at vacuum are available—see for example Fike Corp. Note that the mixer-dryer is never intended to operate at a pressure above atmospheric. The purpose of the rupture disc is to protect the dryer shell in the event of a leak from the steam jacket (15 psig/250 F) into the dryer. The dryer temperature & pressure is monitored and alarmed and provides a rapid response to this condition. If the steam leak is small, the dryer vacuum pump may have enough capacity to prevent a noticeable increase in pressure. If it is large, then the over-pressure condition will happen to rapidly for the operators to respond. The rupture disk is directional – i.e. it is rated for 5 psig in a certain direction only. See comment #2 on companion RCR	Closed
36.	p. G2-479, Section 3.3.1.7; It is stated , "A component data sheet for the dryer vent filter is provided in Appendix C", however, Appendix C contained no pages.		The data sheet can be found in Appendix C of the specification on pg. G2-581.	Closed

Attachment 2
05-ED-085

Revised Drawings for the Secondary Waste System



STREAM No.		1	2	1A	3	4	4A	4B	5	6	7	7A	8	9	10	11	12	13	13A	18
STREAM NAME	UNITS	WASTE RECEIPT	SPIKING FLOW	WASTE FLOW	STARTER PATHS	SOIL	B203 ADDITION	ZrO2 ADDITION	ICV FEED	DRYER CONDENSATE	DRYER AIR	DRYER VENT AIR	OFF GAS AIR	ICV AIR	HOT ICV PRODUCT	TOP UP SOIL	COOLED ICV PRODUCT	ICV OFF GAS	AWTE VENT AIR	DUST RECYCLE
PHASE		LIQUID	LIQUID	LIQUID	SOLID	SOLID	SOLID	SOLID	SOLID	LIQUID	GAS	GAS	GAS	GAS	SOLID	SOLID	SOLID	GAS	GAS	SOLID
CONTINUOUS MASS FLOWRATE	lb/hr	703		703	16	329	23.3	32.6	614	480	13	2566	851	350	497	66	497	513	350	5
CONT. VOL. FLOW RATE (LIQ/GAS)	GPM/ACFM	1.09		1.09						0.98	4.2	600	199	80				280	80	
BATCH VOLUME	USG/ACF	1648		1648						1483	2027	7230000	2400000	962168				3382388	962168	
BATCH MASS	lb	17671		17671	3300	6272	686	820	15420	12055	6345	315859	171097	70323	93260	13315	93760	103209	70323	125
BATCH TRANSFER TIME	Hr	1.14		1.14	0.5	0.25	0.25	0.25	1	8	8	201	5	139	201	4	201	139	139	139
BATCH VOLUME FLOW	USGPM/ACFM	24		24						3.1	13	600	1000	115				406	115	
BATCH MASS FLOW	lb/hr	15458		15458	6600	33088	2344	3281	15420	1507	42	2566	4277	506	467	3329	467	743	506	7.2
DESIGN FACTOR	DIMENSIONLESS	1		1	1	1	1	1	1	1.1	1	1	1	1	1	1	1	1	1	1
DESIGN VOLUME FLOW	USGPM/ACFM	24		24						3.4	13	600	1000	115				406	115	
DESIGN MASS FLOW	lb/hr	15458		15458	6600	33088	2344	3281	15420	1658	42	2566	4277	506	467	3329	467	743	506	7.2
SpG		1.29		1.29	2.32	2.40	1.81	6.70	2.69	0.68	0.001	0.001	0.001	0.001	2.55	2.40	2.7	0.0005	0.001	2.54
SpG (BULK SOLIDS ONLY)					1.50	1.43	1.03	1.55	1.45						2.55	1.43	2.7			1.50
PRESSURE	in. WG	n/a		n/a	n/a	n/a	n/a	n/a	n/a	n/a	-80.07			-2.24	n/a	n/a	n/a	-2.45	-2.57	n/a
TEMPERATURE	°F	82		82	77	77	77	77	83	122	212	77	77	77	2372	77	122	879	77	572
H2O LIQUID	lb/hr	469.5		469.5	0.41	16.5			6.1	479.6										
H2O GAS	lb/hr																	5.5		
FEED Na	lb/hr	62.6		62.6	0.2	6.5			70						69.2		69.2	0.7		0.7
SO2 GAS	ppmV																	1231		
NOx GAS	ppmV																	119238		
HOT GAS	ppmV																	119		
137Cs	Ci/hr	1.5E+00	0.0E+00	1.5E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.5E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.5E+00	0.0E+00	1.5E+00	1.5E-02	0.0E+00	1.5E-02
99Tc	Ci/hr	1.2E-02	0.0E+00	1.2E-02	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.2E-02	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.2E-02	0.0E+00	1.2E-02	8.2E-04	0.0E+00	8.2E-04
1RU	Ci/hr	9.0E-04	0.0E+00	9.0E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	9.0E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	9.0E-04	0.0E+00	9.0E-04	9.0E-08	0.0E+00	9.0E-08
129I	Ci/hr	2.3E-05	0.0E+00	2.3E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.05E-05	2.05E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.0E-08	0.0E+00	2.05E-08	1.84E-05	0.0E+00	1.84E-05

GENERAL NOTES:

1. SINGLE TRAIN FACILITY THROUGHPUT: PROCESS FEED IS MODELLED BASED ON A DESIGN FEED OF 1.09 GPM. A TOTAL OPERATING EFFICIENCY OF 70 % SHOULD BE APPLIED TO ACHIEVE A 0.76 GPM PRODUCTION RATE WITH A 20.0 WT % Na2O GLASS LOADING IN THE GLASS PRODUCT.
2. FLOW IN STREAM 2 IS VARIABLE; A TESTING MATRIX WILL DETERMINE THE AMOUNT AND COMPOSITION OF SPIKING MATERIAL TO BE ADDED IN THE INDIVIDUAL TESTS.
3. VALVES ARE ONLY SHOWN TO INDICATE PROCESS INTENT.
4. FEED DATA BASED ON SECTIONS 3.1.2.1.1.1 AND 3.1.2.1.1.2 IN RPP-17403 REV 2.
5. RADIONUCLIDE CONTENT WAS BASED ON TABLE 3-3 IN SECTION 3.1.2.1.1.3 OF RPP-17403 REV 2.

LINES LEGEND:

- MAJOR PROCESS STREAM
- MINOR PROCESS STREAM
- INTERMITTENT FLOWS

REV	REVISION DESCRIPTION	Date	By	CHK'D	APP'D	ENGR APP'D
CJ	REMOVED PROPRIETARY BLOCK	19/SEPT/05	JSM			
BN	ISSUE FOR CH2 APPROVAL AND 90% REPORT	19 MAY 05	SB	TH	KH	TH
BQ	ISSUED FOR CLIENT APPROVAL & 90% REPORT	24 MAR 05	RKB	AC	KH	TH
BF	ISSUED FOR CLIENT APPROVAL & 90% REPORT	15 MAR 05	SB	RC	KH	TH
BE	ISSUED FOR CLIENT APPROVAL & 90% REPORT	17 FEB 05	SB	LSC	KH	TH
BB	ISSUED FOR CLIENT APPROVAL & 90% REPORT	14 FEB 05	SB	LSC	KH	TH
BC	ISSUED FOR CLIENT APPROVAL & 90% REPORT	21 JAN 05	SB	LSC	KH	TH
BA	GENERAL REVISIONS, ISSUED FOR CLIENT COMMENT	16 DEC 04	SB	LSC	KH	TH
AZ	GENERAL REVISIONS, ISSUED FOR INTERNAL REVIEW	19 NOV 04	SB	LSC	KH	TH
D	FOR CONSTRUCTION	20 AUG 04	SB	LSC	KH	TH
C	FORMERLY F-145545-00-A-0021, FOR APPROVAL	26 JULY 04	SB	LSC	KH	TH
B	FINAL ISSUE	14 APR 04	SB	LSC	KH	TH
A	ISSUED FOR CLIENT COMMENT	10 MAR 04	SLS		KH	TH

DWG NO	TITLE	REF NUMBER	TITLE
DRAWING TRACEABILITY LIST		REFERENCES	
		NEXT USED ON	

NO	DESCRIPTION	BY	CHK'D	APP'D	DATE
REVISIONS					

NAME	SIGNATURE	DATE
DESIGNED		
DRAWN		
ENGINEER OF RECORD		
RESPONSIBLE MANAGER		
PROJECT MANAGER		
CONTRACTOR APPROVAL		

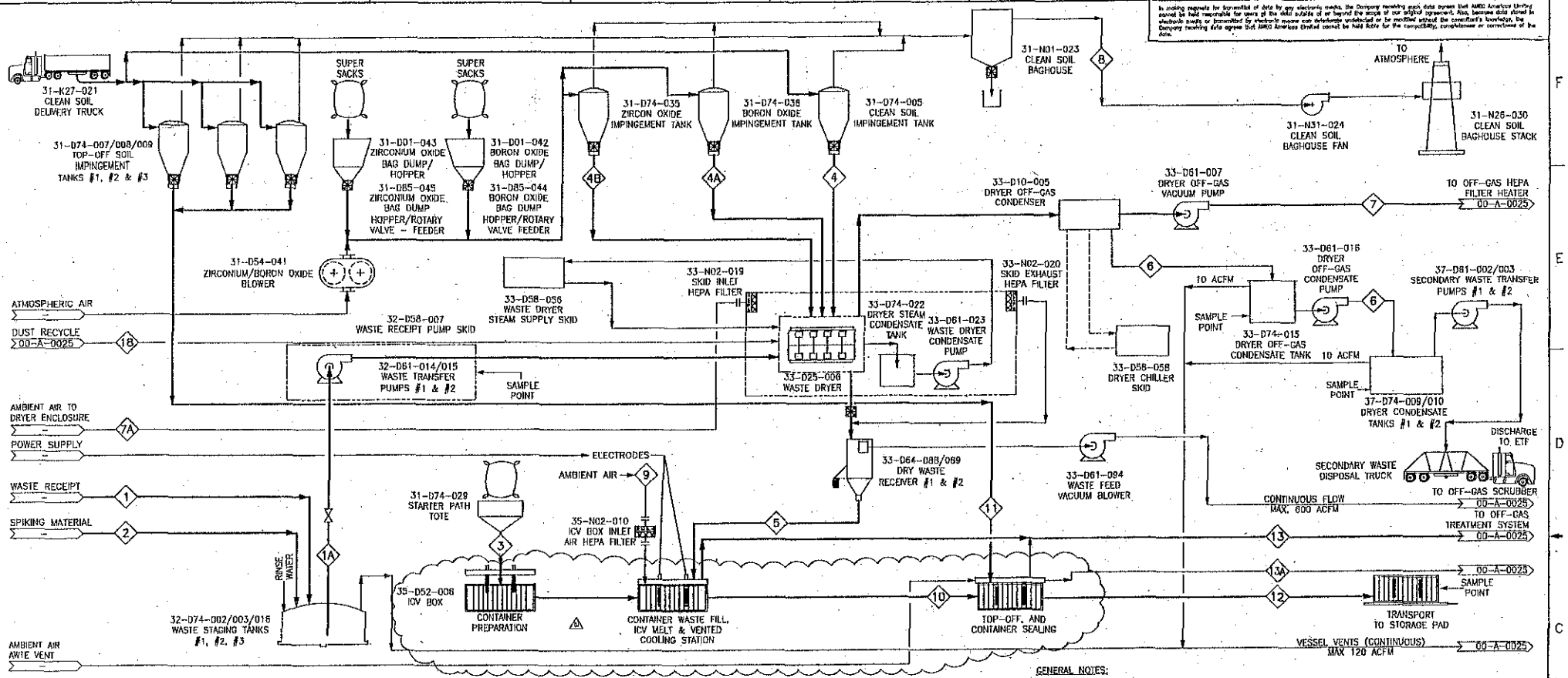
F-145579-00-A-0021 | 0J

U.S. DEPARTMENT OF ENERGY
Office of River Protection

amec

FULL DBVS
FEED PREPARATION & MELT
PROCESS FLOW DIAGRAM

SIZE	SCALE	WEIGHT	REV
F	NTS		



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2. FLOW IN STREAM 2 IS VARIABLE; A TESTING MATRIX WILL DETERMINE THE AMOUNT AND COMPOSITION OF SPIKING MATERIAL TO BE ADDED IN THE INDIVIDUAL TESTS.
3. VALVES ARE ONLY SHOWN TO INDICATE PROCESS INTENT.
4. FEED DATA BASED ON SECTIONS 3.1.2.1.1.1 AND 3.1.2.1.1.2 IN RPP-17403 REV 2.
5. RADIONUCLIDE CONTENT WAS BASED ON TABLE 3-3 IN SECTION 3.1.2.1.1.3 OF RPP-17403 REV 2.

LINES LEGEND:

- MAJOR PROCESS STREAM
- MINOR PROCESS STREAM
- INTERMITTENT FLOWS

STREAM NO.		1	2	1A	3	4	4A	4B	5	6	7	7A	8	9	11	12	13	13A	18
STREAM NAME	UNITS	WASTE RECEIPT	SPIKING FLOW	WASTE FLOW	STARTER PATH	SOIL	D203 ADDITION	ZrO2 ADDITION	ICV FEED	DRYER CONDENSATE	DRYER AIR	DRYER VENT AIR	OFF-GAS AIR	ICV AIR	TOP-UP SOIL	COOLED ICV PRODUCT	ICV OFF GAS	AWTE VENT AIR	DUST RECYCLE
PHASE		LIQUID	LIQUID	LIQUID	SOLID	SOLID	SOLID	SOLID	SOLID	LIQUID	GAS	GAS	GAS	GAS	SOLID	SOLID	GAS	GAS	SOLID
DESIGN VOLUME PER BLOCK	USG/BLOCK	13170		13170															
DESIGN MASS PER BLOCK	lb	141371		141371	3300	66178	4987	5562	123355	98439	2537	518659	171097	74923	13318	93789	103209	70323	1004
SpG		1.29		1.29	2.32	2.40	1.51	5.20	2.69	0.98	0.0012	0.0011	0.0012	0.0012	2.40	2.85	0.0005	0.0012	2.54
SOLIDS BULK DENSITY							1.60	1.80											
PRESSURE	in WG	n/a		n/a	n/a	n/a	n/a	n/a	n/a	n/a	-60.07	0	0	-2.54	n/a	n/a	-2.46	2.6	n/a
TEMPERATURE	°F	60		60	77	77	77	77	63	122	212	77	77	77	77	122	875	77	572
H2O LIQUID	lb	94305		94305	83	3306	0	0	1234	98438							0		
H2O GAS	lb																1313		
FEED Rb	lb		12581	12581	32	1390			14031							12516	161		149
SO2 GAS	ppmV																1231		
NOx GAS	ppmV																119238		
H2O GAS	ppmV																119		
137Cs	Ci	3.1E+02		3.1E+02	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.1E+02	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.1E+00	0.0E+00	0.0E+00	3.1E+00
99Tc	Ci	2.4E+00		2.4E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.5E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.4E-00	1.2E-01	0.0E+00	1.2E-01
TRU	Ci	1.8E-01		1.8E-01	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.8E-01	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.8E-05	0.0E+00	0.0E+00	1.8E-05
129I	Ci	4.5E-03		4.5E-03	0.0E+00	0.0E+00	0.0E+00	0.0E+00	4.1E-03	4.1E-03	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	4.1E-04	3.7E-03	0.0E+00	3.7E-03

REV	REVISION DESCRIPTION	DATE	BY	CHKD	APP'D
DH	REMOVED PROPRIETARY BLOCK	08/30/05	JBM	JBM	PAC
DH	ISSUE FOR EHZ APPROVAL AND BOX REPORT	12 MAY 05	SB	TH	KH
DG	ISSUED FOR CLIENT APPROVAL & BOX REPORT	24 MAR 05	RNB	RC	KH
DF	ISSUED FOR CLIENT APPROVAL & BOX REPORT	15 MAR 05	SB	RC	KH
DE	ISSUED FOR CLIENT APPROVAL & BOX REPORT	17 FEB 05	SB	LSC	KH
DD	ISSUED FOR CLIENT APPROVAL & BOX REPORT	14 FEB 05	SB	LSC	KH
DC	ISSUED FOR CLIENT APPROVAL & BOX REPORT	21 JAN 05	SB	LSC	KH
DB	GENERAL REVISIONS, ISSUED FOR CLIENT COMMENT	18 DEC 04	SB	LSC	KH
DA	GENERAL REVISIONS, ISSUED FOR INTERNAL REVIEW	23 NOV 04	SB	LSC	KH
D	FOR CONSTRUCTION	20 AUG 04	SB	LSC	KH
C	FORMERLY F-145563-00-A-0024, FOR APPROVAL	28 JULY 04	SB	LSC	KH
B	FINAL ISSUE	14 APR 04	SB	LSC	KH
A	ISSUED FOR CLIENT COMMENT	10 MAR 04	SJC		KH

DRAWING TRACEABILITY LIST

DWG NO	TITLE	REF NUMBER	TITLE
		NEXT USED ON	REFERENCES

REVISIONS

F-145579-00-A-0024 OJ

amec

PROJECT: 145579-FINAL DBVS DESIGN

NAME

U.S. DEPARTMENT OF ENERGY
Office of River Protection

FULL DBVS
FEED PREPARATION & MELT
SINGLE BLOCK PFD

SIZE F | SCALE NTS | SHEET

Attachment 3
05-ED-085

Independent Qualified Registered Professional Engineer Design Assessment Report No. DR-009, Revision 1, Review of Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package, RPP-24544, Revision C, Section 2.2, Waste Dryer System

Independent Qualified Registered Professional Engineer Support to Demonstration Bulk Vitrification Project

CH2M Hill Requisition # 114648

IQRPE Design Assessment Report No. DR-009, Rev. 1

Review of

Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package, RPP-24544, Revision C

Section 2.2, Waste Dryer System (90 Percent Design)

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October 10, 2005

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1.0 INTRODUCTION

The Washington State Department of Ecology (Ecology) has issued a permit for the Demonstration Bulk Vitrification System (DBVS) that mandates the use of an Independent Qualified Registered Professional Engineer (IQRPE) to perform a third-party independent review of the design of Washington Department of Ecology sensitive portions of the DBVS project. TechnoGeneral Services Company (TGS) has prepared this IQRPE Design Assessment Report in conjunction with Dana Engineering, Inc. (DEI), at the request of CH2M Hill Hanford Group, Inc. (CH2M HILL), the project co-operator. TGS is the IQRPE of record for this project

1.1 Project Description

The DBVS is a demonstration waste treatment plant operated under a Research, Development and Demonstration (RD&D) Permit issued by Ecology. The RD&D Permit is issued to the U.S. Department of Energy, Office of River Protection (DOE-ORP) and CH2M HILL. The DBVS plant will be located at the 200 West Area of the Hanford Site. The DBVS is being designed, constructed, and operated by AMEC, an engineering/services company from Vancouver, British Columbia, under contract to CH2M HILL. AMEC is tasked to comply with the RD&D Permit. Figure 1 is a three-dimensional graphic view of the DBVS project.

The DBVS is designed to process a liquid salt solution of low-activity mixed waste (LAW) originating from Tank 241-S-109. Tank 241-S-109 is located adjacent to the DBVS facility. The LAW is to be converted into solid glass form by drying the LAW, mixing the LAW in dried form with soil, and melting it with an electric current. The project is intended to demonstrate the viability of immobilizing LAW from the tank farm utilizing a proprietary AMEC vitrification system. The demonstration is to involve treating up to 600,000 gal of waste in 18 months, producing up to 50 In-Container Vitrification (ICV^{TM}) melt boxes of stabilized vitrified waste.

About 13,170 gal of LAW are to be processed in each melt box. A detailed description of the process is provided in Attachments AA and BB of the RD&D Permit.

1.2 Design Review Requirements

Many of the components of the DBVS will handle dangerous or mixed waste and are regulated by Washington Department of Ecology in the RD&D Permit. The RD&D Permit requires an IQRPE review of the design of these components prior to installation.

The Compliance Schedules, Sections IV.A.8 and V.I of the RD&D Permit, define the design documents to include drawings, specifications, calculations and other information as deemed necessary to support the design. The RD&D Permit identifies 7 systems, including the foundations system that will have design packages prepared for IQRPE review. CH2M HILL is providing the IQRPE with design review packages as AMEC completes the design.

As a basis for the IQRPE certification, a review is performed on a final version of the document "Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package", RPP-24544 as prepared by AMEC and reviewed and approved by CH2M HILL. Each design review package includes a body of text that explains the purpose and scope of the DBVS and describes the overall

process as well as the specific system addressed in the design package. Included as supporting information (appendices) are calculations, site maps, drawings, sketches, piping and instrumentation drawings (P&ID), process flow diagrams (PFD), waste characteristics, technical specifications for materials and equipment, and miscellaneous supporting data. Each design review package will be a revision of the RPP-24544 specific to the system addressed in the package. CH2M HILL is not requiring AMEC to seal/stamp final design documents per WAC standards for any DBVS work, other than the Site Improvements work (foundations and site work). Documents such as drawings, calculations, and specifications included in the design review package that are marked as final and have signatures for the preparer, checker, and approver, will be reviewed by the IQRPE as a complete document. All other documents will be reviewed as preliminary or supportive information.

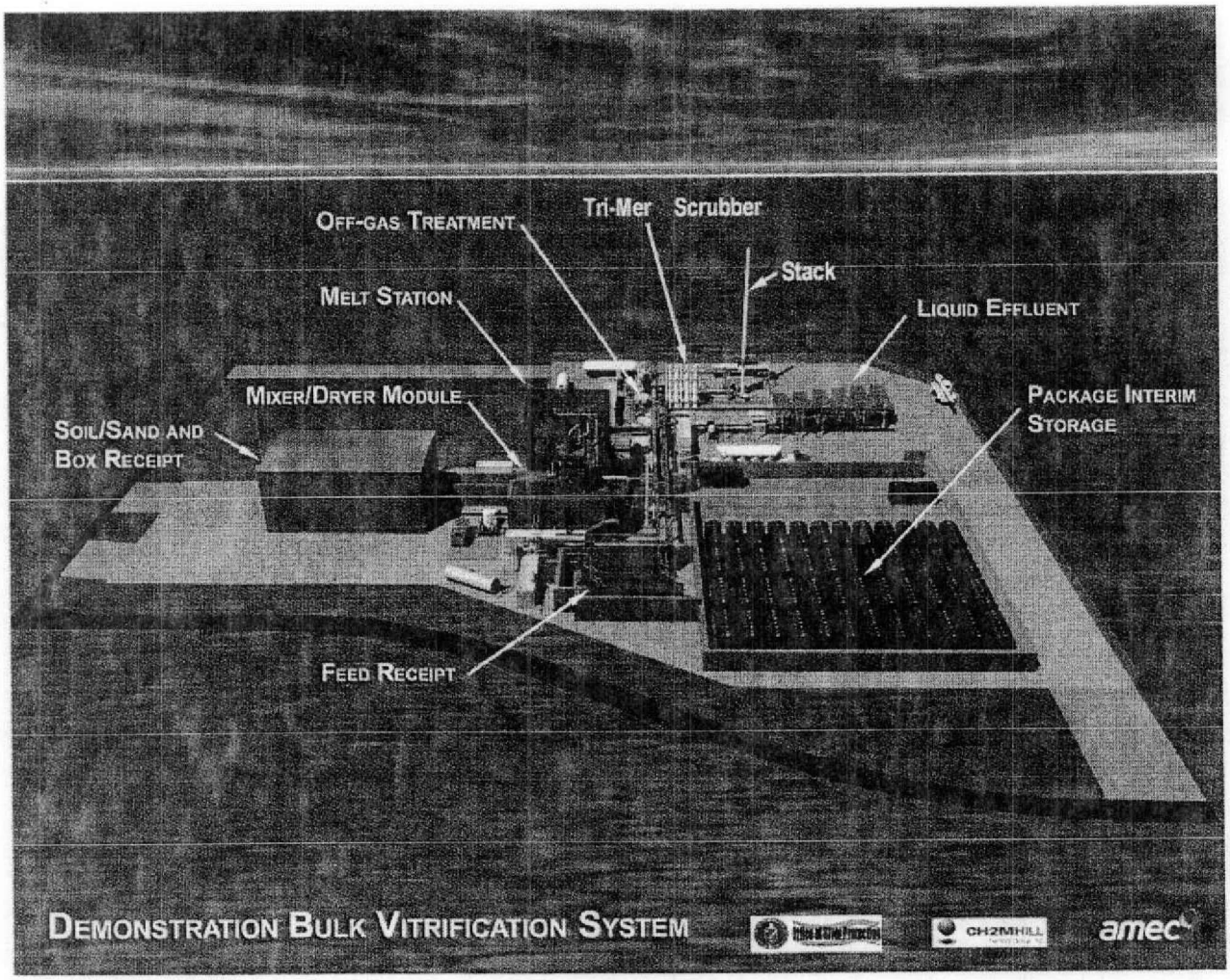


Figure 1. Demonstration Bulk Vitrification System Site Three-Dimensional View

Preliminary design data was submitted and reviewed by the IQRPE reviewer as part of this certification, but only in an effort to familiarize the reviewer with the design until receipt of the final version.

The second system identified for IQRPE design review is the Waste Dryer System, Section 2.2 of RPP-24544, Rev. C, hereafter referred to as Design Package 2.2. The primary functions of the Waste Dryer System are to:

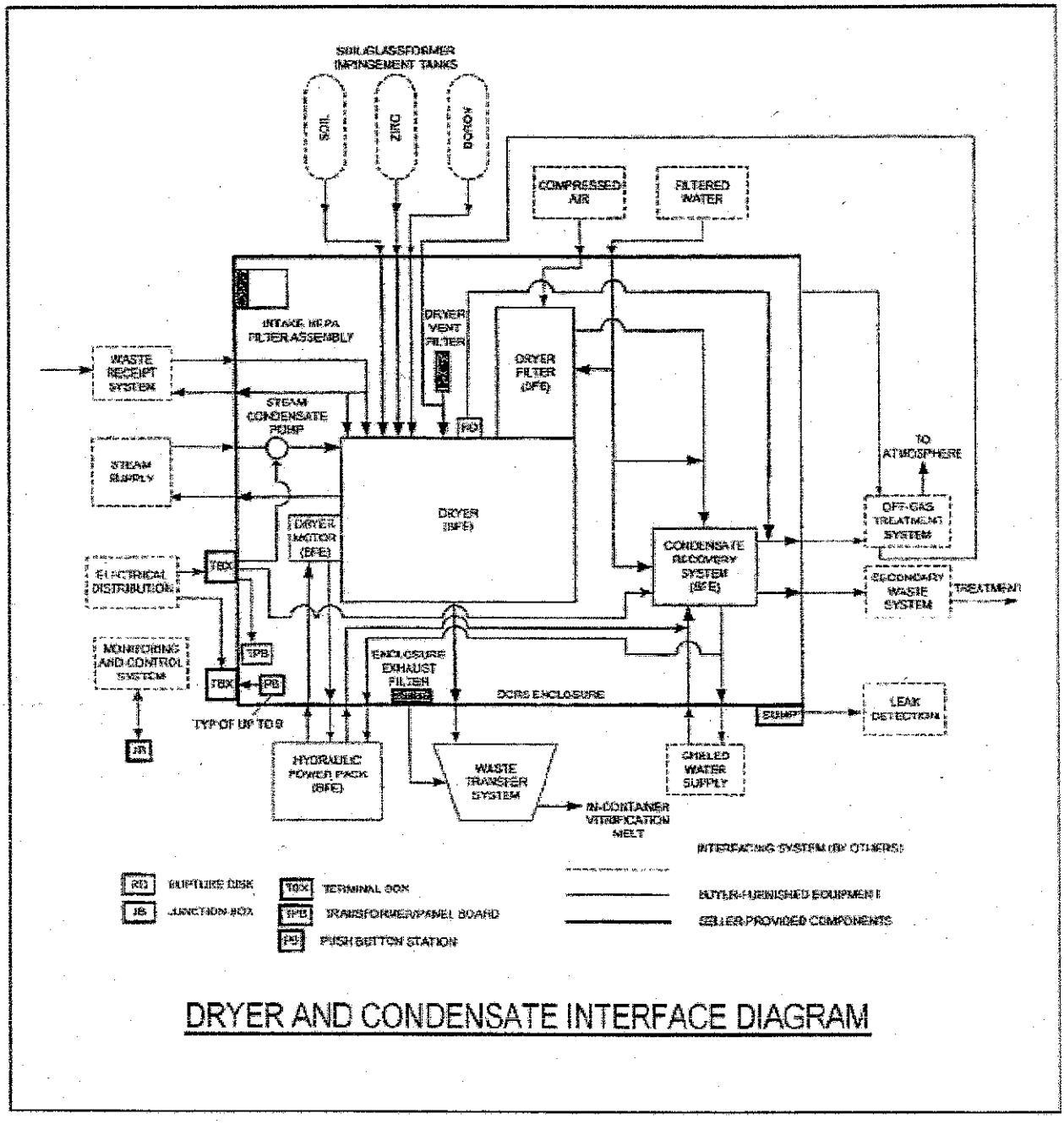
- Receive waste for processing from the liquid waste staging tanks via the waste transfer pump skid,
- Mix liquid waste with process additives, to be added after the waste is mixed with the clean soil and dried(clean soil, zirconium oxide, and boron oxide) in a steam jacketed dryer,
- Evaporate water from the mixture using heat provided by a steam supply system which provides steam to the dryer steam jacket,
- Process gases from the dryer through a condenser to collect water and other species, (5) processes the condensate to the secondary waste system,
- Vent non-condensable gases to the Offgas Treatment System (OGTS), and
- Transfer dried waste mixture to the In-Container Vitrification (ICV) System via the Dried Waste Handling System for vitrification.

The following systems interface with the Waste Dryer System but are outside the scope of the Waste Dryer System and are not included in the scope of this IQRPE review:

- Compressed air and instrument air systems
- Filtered water system, Waste sampling
- Waste transfer system
- Liquid waste staging system
- Process Additives System (provides soil, zirconium oxide and boron oxide to the dryer),
- Dried waste handling system (transfers the dried waste from the dryer to the ICV System)
- OGTS (treats vented gases from the dryer before emission to the environment).

1.3 Waste Dryer System Design Overview

This certification of the Waste Dryer System is based on the information presented in Design Package 2.2. The design package includes multiple calculations, specifications, and drawings, as listed in Attachment A, *IQRPE Disposition of Reviewed Calculations, Specifications and Drawings.* TGS is providing one IQRPE design review report for the Waste Dryer System. Figure 2 shows interfaces between the Dryer and Condensate recovery system and other interfacing systems.



DRYER AND CONDENSATE INTERFACE DIAGRAM

Figure 2 Dryer and Condensate Interface Diagram

The Waste Dryer System includes the following major components:

- Waste Dryer, Dryer Enclosure and HVAC units, and Condensate Recovery System (Specifications 143643-D-SP-001 and 145579-D-SP-006)
- Dryer Chiller Pump Skid and chiller Unit (Specifications 145579-D-SP-005 and Data Sheet 143643-D-DS-039.1)
- Steam Supply System (Specification 145579-D-SP-007)
- Dryer Support Structure and Piping Systems (Drawings F-145579-00-B-0008 and 0009)

The following subsections outline the major subsystems included as part of the Waste Dryer System. Piping and instrumentation diagrams (P&ID) for these subsystems are shown on the following drawings, contained in Attachment D:

- F-145579-33-A-0100 Bulk Vitrification Waste Dryer System
- F-145579-33-A-0101 Bulk Vitrification Waste Dryer Vacuum System
- F-145579-33-A-0104 Bulk Vitrification Waste Dryer Chilled Water System
- F-145579-33-A-0105 Bulk Vitrification Waste Dryer Steam Supply System

The following P&ID's are included in the Waste Dryer System design review package which interface with, but are not a part of the Waste Dryer System:

- F-145579-31-A-0100 Rev J Bulk Vitrification Clean Soil Handling System
- F-145579-31-A-0101 Bulk Vitrification Glass Formers Handling System
- F-145579-32-A-0100 Bulk Vitrification Waste Transfer Pump System

1.3.1 Dryer and Condensate Recovery System Overview (Specifications 143643-D-SP-001 and 006)

The dryer is designed to receive waste through nozzles located on top of the dryer. Glass-forming additives are added through nozzles on top of the dryer. Heat and vacuum are used to dewater the waste feed/soil mixture. Heat is applied to the dryer wall with a steam jacketed shell heat transfer process using low pressure steam (design 15 psig @ 250F operating). Contents in the Waste Dryer are mixed with rotating plows under a high vacuum (design operating @ 26 in. Hg). The plows are arranged in the dryer such that the waste is mixed by directing waste from the ends of the dryer towards the center. The vacuum facilitates the dewatering process by promoting low temperature evaporation and withdrawal of vapor from the head space (design evaporation temperature @ 140deg F). Calculation 145579-D-CA-003 "Dryer Energy, Steam, and Chilled Water Demand Analysis was reviewed by the IQRPE which calculates energy usage of the dryer unit based on the operational requirements for the melting process for determining sizing of the boiler and chiller.

Evaporated moisture is drawn by the vacuum pump through a sintered metal filter mounted on the Waste Dryer to remove particulates before the vapor reaches the condenser unit. Particulates captured in the sintered metal filter are returned to the dryer drum via back pulsing the filter with compressed air. Condensable gases are captured in the Condensate Recovery System by a condenser cooled with chilled water supplied by the dryer chiller pump and tank skid, which recirculates from the chiller unit and a condensate collection tank. The condensate is periodically pumped from the tank to the secondary waste storage tanks. Non-condensables are transferred from the vacuum pump to the Offgas Treatment System (OGTS).

The dryer, filter and Condensate Recovery System are contained in an enclosure. The enclosure provides secondary containment for both liquid and dried waste. The enclosure is designed to be ventilated via outside air drawn through an inlet HEPA filter. Ventilation air passes through the enclosure flows through the outlet HEPA filter to the negatively pressurized dried waste handling system. This system is further discussed in section 2.2.4, "Secondary Containment Design".

1.3.2 Dryer Chiller Pump Skid and Chiller Unit Overview (Specification 145579-D-SP-005 and Data Sheet 143643-D-DS-039.1)

The Waste Dryer Off-gas condenser heat exchanger receives cooled 50/50 percent glycol/water mixture from an air-cooled screw liquid chiller unit. The unit is comprised of a chiller compressor, evaporator, economizer and chilled water pump skid. The chiller unit has a design nominal cooling capacity of 230 tons with a design cooling fluid inlet temperature of 70° F and a design exit temperature of 50° F. Circulation of the cooling fluid between chiller unit and the Condensate Recovery System is accomplished using one operating dryer chiller pump (one spare) which receives chilled water from the Chiller Surge Tank. Calculation 145579-D-CA-033 "DBVS Waste Dryer Heating and Cooling Load Calculations" was reviewed by the IQRPE for inputs to the CHVAC Commercial Software calculation output.

1.3.3 Steam Supply System Overview (Specification 145579-D-SP-007)

The steam for the dryer is provided by a packaged Steam Supply system installed in a separate enclosure. The assembled Steam Supply System is comprised of a boiler, blow-down separator, duplex feed system, softener, chemical feed, and associated piping and hoses within the enclosure. A separate diesel fuel tank and fuel delivery system supplies the boiler. The steam supply has a specified operating pressure of 15 psig at a capacity of 1,700,000 Btu/hr.

1.3.4 Dryer Support Structure and Piping Systems Overview

The Dryer and Condensate Recovery system (DCRS) is located on a support structure. Details for the structural steel are provided on Drawings F-145579-00-B-0008 and -00-B-0009. Details for anchoring and installation of the system on the support structure are detailed in the Dryer Support Structure Calculation 145579-B-CA-012, Rev 1, which has also received an independent IQRPE review per section 2.2.1 of this report.

Waste is designed to be transferred between the DCRS and the Waste Receipt System via Hose in Hose Transfer Lines (HIHTLs). Liquid secondary waste is transferred to the Secondary Waste System via HIHTLs. Preliminary routing for lines to and from the DCRS , including those for the

steam supply and chilled water units, are shown on Drawings F-145579-00-P-0005, -00-P-0006, -00-P-0007, -00-P-0010, and -00-P-0011. Typical pipe support details are shown on Drawings F-145579-00-P-0001, 00-P-0002, -00-P-0003, and -00-P-0004.

1.4 Scope of IQRPE Design Assessment

This IQRPE design report number is DR-009. This IQRPE design assessment includes a comprehensive review of the Design Package 2.2 in accordance with the requirements of the DBVS RD&D Permit IV.A.8.b.i through IV.A.8.b.viii, IV.A.8.c.i, and V.I.2.a through V.I.2.f, and V.I.3.a through V.I.3.f. Exceptions are listed in Section 2.2 below. The documents included in this review and the level at which each document was reviewed are summarized in Attachment A.

The following items are not covered by the WAC dangerous waste regulations or the RD&D Permit for the facility, and are therefore outside of the scope of this certification:

- Plant utilities, including instrument and plant air supply lines and electrical power beyond the first upstream valve or uninterruptible power supply systems.
- Structural features not related to hazardous waste secondary containment.
- Architectural features not related to hazardous waste containment.
- Lighting systems.
- System design features related to protection of the system due to vehicular traffic.
- Electrical or signal lines beyond the first upstream field termination box (FTB), motor control center (MCC), or instrument control panel (ICS). Specifications for electrical feed, including wiring, local hand switches, terminations, breakers, and other equipment or instruments located in motor control centers were reviewed. Specifications for instrument cabling and terminations were reviewed only between locally mounted devices and field termination boxes and/or local instrumentation and control panels.
- Radiation monitoring or detection components that may be mounted at various locations throughout the system.
- Verification of functional logic for operation and control of the Waste Dryer System.

The IQRPE has not reviewed the Design Package 2.2 to the following design standards referenced in RPP-17403, "Function and System Design Requirements for the Demonstration Bulk Vitrification System" (see Section 4.0 References) because the Waste Dryer System Design Review Package does not address the following issues contained in RPP-17403:

- RPP-17403, section 3.1.2.1.1.3 and Table 3-3 requirements regarding waste feed radio nuclide properties, including all radioactive and radio nuclide property considerations.
- RPP-17403, section 3.1 requirements for the DBVS that the design:

- Ensure exposure of plant operating personnel to radioactive process streams (radiation) is as-low as reasonably achievable (ALARA). See also Sections 3.2.4 and 3.3.6.1.1.
- Minimize the production of secondary waste streams.
- Ensure that all process byproducts are safe for long-term storage or release into the environment.

- RPP-17403, section 3.3.1.6 requirements for the DBVS that the design include the capability for flushing components for decontamination.
- RPP-17403, section 3.3.6 requirements for the DBVS that the design related to the following:
  - Personnel Safety
  - Fire Protection
  - Non-Radioactive Airborne Emissions (Section 3.3.6.3.4)
  - Radioactive Airborne Emissions (Section 3.3.6.3.6)
- RPP-17403, section 3.3.8 (Decontamination and Deactivation) or Section 3.3.9 (Nuclear Safety) requirements for the DBVS.

Because the 90 percent design of the Waste Dryer System has been developed as a purchase specification, much of the 'design' activities have been designated the responsibility of the equipment vendor or Seller. Therefore, this information will not be available until fabrication of the equipment is underway and will require further IQRPE review as part of the construction certification package. Documentation to be reviewed by the IQRPE for inclusion with the construction certification package includes the deliverables listed in Attachment B.

2.0 DESIGN ASSESSMENT

The Waste Dryer System includes the following major components:

- Dryer and Condensate Recovery System (SP-001 and SP-006)
- Dryer Chiller Pump Skid and Chiller Unit (SP-005 and datasheet 143643-D-DS-039.1)
- Steam Supply System (SP-007)
- Dryer Support Structure (Drawings F-145579-00-B-0008, -0009)

See Figure 3, "Waste Dryer System Three-Dimensional View". Figure 3 shows a three-dimensional representation of these components at the DBVS site. The following subsections identify the basis and methods used to complete this IQRPE design certification.

The IQRPE has segregated the design assessment into subsections of the following categories of concern as presented in the WAC regulations:

- Structural Design Standards
- Waste Compatibility
- Pressure Control
- Secondary Containment
- Ancillary Equipment Design
- Corrosion Assessment

At the end of each subsection the IQRPE may include exceptions to the assessment for a particular part of the design. An IQRPE exception, as defined in this report, represents either a lack of specific information on part of the design that will need to be provided, or exceptions shall be cited in meeting the permit and WAC standards which must be sufficiently addressed in the Final Installation Package.

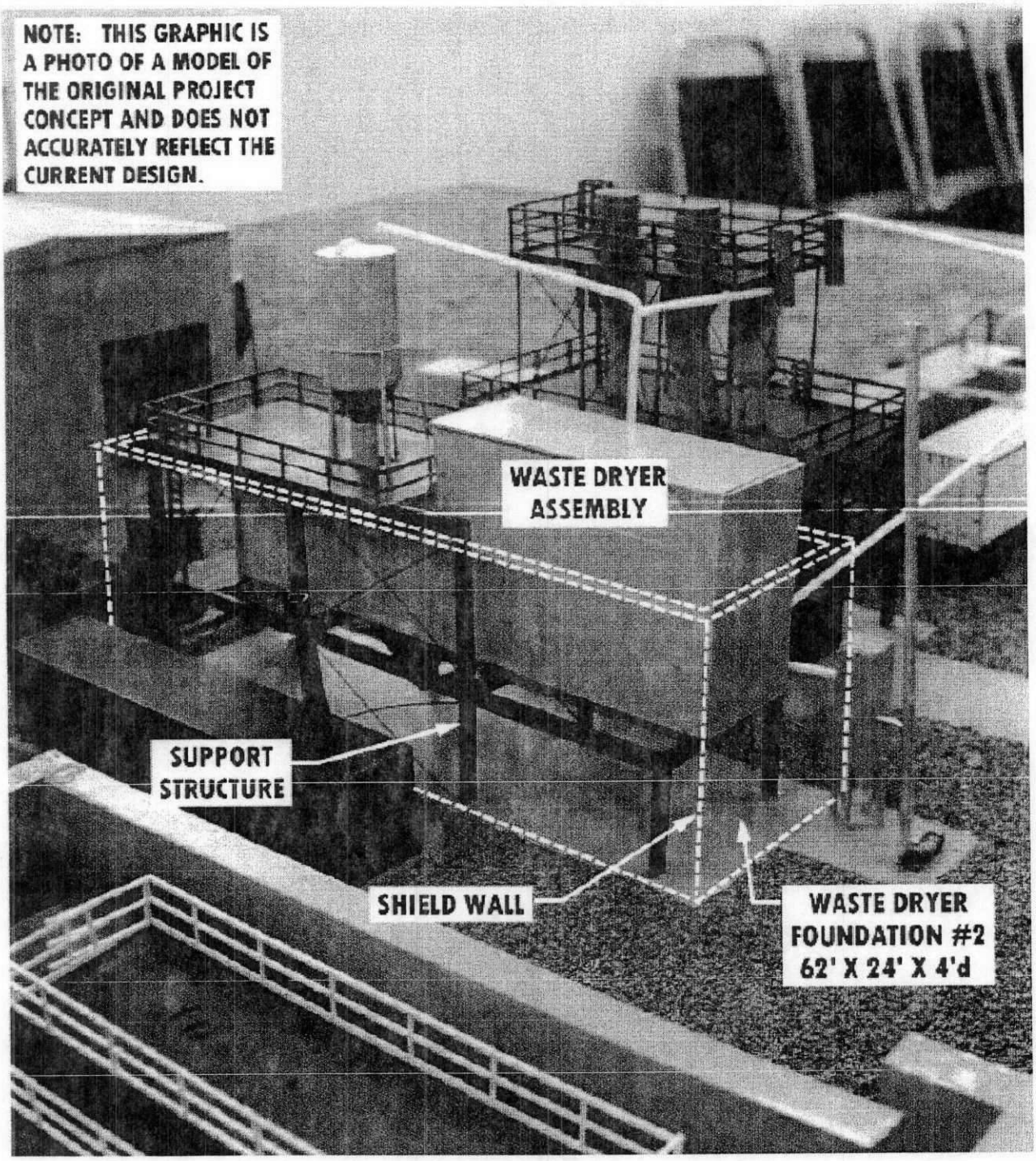


Figure 3 Waste Dryer System Three-Dimensional View

2.1 Codes, Standards and Regulations

The codes, standards, and regulations specifically used during the preparation of this certification are referenced as necessary throughout this report.

A complete list of codes, standards, and regulations that have been incorporated into the Technical Specification packages is included as Attachment C to this report.

The IQRPE concurs with the use of the codes, standards, and regulations that have been designated in the Technical Specifications.

2.2 Basis of Design

The Waste Dryer System is anticipated to operate for a minimum service life of 18 months while handling LAW from Tank S-109. Equipment has been specified with a design life of 5 years. The DCRS is specified to receive batches of liquid salt solution from the Waste Receipt System, mix the liquid salt solution with soil plus additives and evaporate enough water in the dryer under vacuum to provide a suitable dried waste product. The DCRS is also specified to condense the evaporated water and transfer it to the Secondary Waste System and to discharge the dried waste to the dried waste transfer system. Waste processed in the Waste Dryer System combines liquid waste with formulated soils mixtures, as summarized in Tables 1 and 2 below.

Table 1. Waste Dryer System Primary Operating Characteristics

[1] Specification 145579-D-SP-006 Rev 2 Table 3-3

Operating Characteristic	Range
Salt solution content	Nominal 5 Molar Sodium concentration
Waste Chemical Composition	Per Table 3-3 of Specification 143643-D-SP-001 and Data Sheet 143643-D-DS-001.1
Waste supernate liquid density[1]	1.2 to 1.3 g/mlL
Waste viscosity[1]	10 cP Max at 77 F
Waste pH range[1]	8 to 13
Waste temperature range as staged[1]	40 to 150°F

Table 2 Soil and Additives Formulation

(Ref: Spec 143643-D-SP-001, Rev 0 "Dryer and Condensate Recovery System)

Component	Reagent Formula	Mass (g)/kg of Soil Mixture
Hanford Soil (damp)	NA	868
Boron Oxide	B_2O_3	55
Zirconium Oxide	ZrO_2	77

2.2.1 Structural Design Standards

Ecology (1995) requires that an IQRPE certify that the proposed tank system will have a sufficient structural integrity and is acceptable for storing and treating dangerous waste in accordance with WAC 173-303-640(3)(a). This assessment must show that the foundation, structural support, seams, connections, and pressure controls are adequately designed and that the tank system has sufficient structural strength, compatibility with the wastes to be stored or treated, and corrosion protection to ensure that it will not collapse, rupture, or fail in accordance with WAC 173-303-640(3)(a).

The following subsections highlight the IQRPE Structural Design review for Waste Dryer Support Structure as well as each of the major Waste Dryer System subsystems. Specific exceptions to this IQRPE certification report as they relate to the structural review are included as a final subsection.

2.2.1.1 Waste Dryer Support Structure

The IQRPE performed an independent assessment of the Waste Dryer Support Structure-structural calculations, drawings and attachment point loads and reactions. Structural design standards and criteria were reviewed to ensure that they clearly identified and referenced applicable codes, industry standards and recommended practices.

IQRPE independent structural modeling utilized a Rapid Interactive Structural Analysis (RISA) code developed by Los Alamos Technical Associates, Inc. (LATA), which was configured for Waste Dryer System geometric, mathematical and physical structural properties. The approach using the RISA model provided an independent assessment of the AMEC's approach which used a STAAD-Pro structural calculation. The IQRPE review of the waste dryer support structure implemented an independent modeling of the structure in lieu of performing a line-by-line checking of the submitted calculation 145579-B-CA-012, Rev 2. The output was then evaluated for effects on structural members due to structural, equipment and grating weights, as well as resultant seismic and dynamic reaction forces. Where discrepancies existed, the IQRPE structural P.E. conferred with the Seller's Structural P.E. to ensure the differences would be properly rectified, so that the design would satisfy all structural specification and code requirements.

Load conditions were taken from the Seller's calculation 145579-B-CA-012, Rev 2, and compared with framing configurations in drawing F-145579-00-B-0008, Rev F and drawing F-145579-00-B-0009, Rev F. Where discrepancies between drawings and calculations were discovered, the drawings were used as the governing criteria since the drawings reflect the intended fabrication design. AMEC has since revised and corrected calculations to match submitted drawings.

Part of the Design Package 2.2 includes the structural steel supporting structure for the Waste Dryer System, referred to hereinafter as the Waste Dryer Support Structure. It is a major design element of this project and special attention was paid to the review of the calculations for this structure. TGS utilized the structural engineering expertise of subcontractors Parker Messana and Associates (PMA) and Los Alamos Technical Associates (LATA) to help assess this design.

PMA performed a structural IQRPE assessment of the steel support structure using a computer model developed by LATA. The PMA assessment included a review of input and output data from AMEC's STAAD Pro computer model for the steel support structure. The STAAD Pro data was reviewed and compared to the results of an independent RISA-3D structural model prepared by LATA set up using the same parameters used for the STAAD Pro model. Both models were based on AMEC's calculations 145579-B-CA-012 Rev 1, and later updated to reflect the revised calculation 145579-B-CA-102 Rev 2. PMA specifically reviewed the AMEC's manual calculations and seismic calculations, per 1997 UBC code requirements, AISC 9th Edition steel specification requirements. PMA also reviewed AMEC's bracing and connection designs and the AMEC structural Steel Drawings. Hand calculated and verified seismic forces were reviewed and compared to the computer analysis input data and output data. Results of the structural independent review showed that seismic loading was consistent and results of both computer programs were comparable with exceptions listed in applicable "Exceptions" of this report.

PMA found that connection details on the drawings and calculations were incomplete and notified the engineer. The 1997 UBC Section 1633.2.3 requires the engineer to design and detail connections on his documents and not to assign this responsibility to others. This violation was corrected by the Seller. The RISA model indicated several dryer support beams appeared to be overstressed, primarily from load cases including seismic forces. PMA received comments from LATA and contacted the AMEC engineer for his response and resolution. These issues were resolved by the addition of connection details and correction of loading discrepancies.

Figure 4 contains a RISA 3D Sample Output Graphic, which represents a simplification of actual RISA output results.

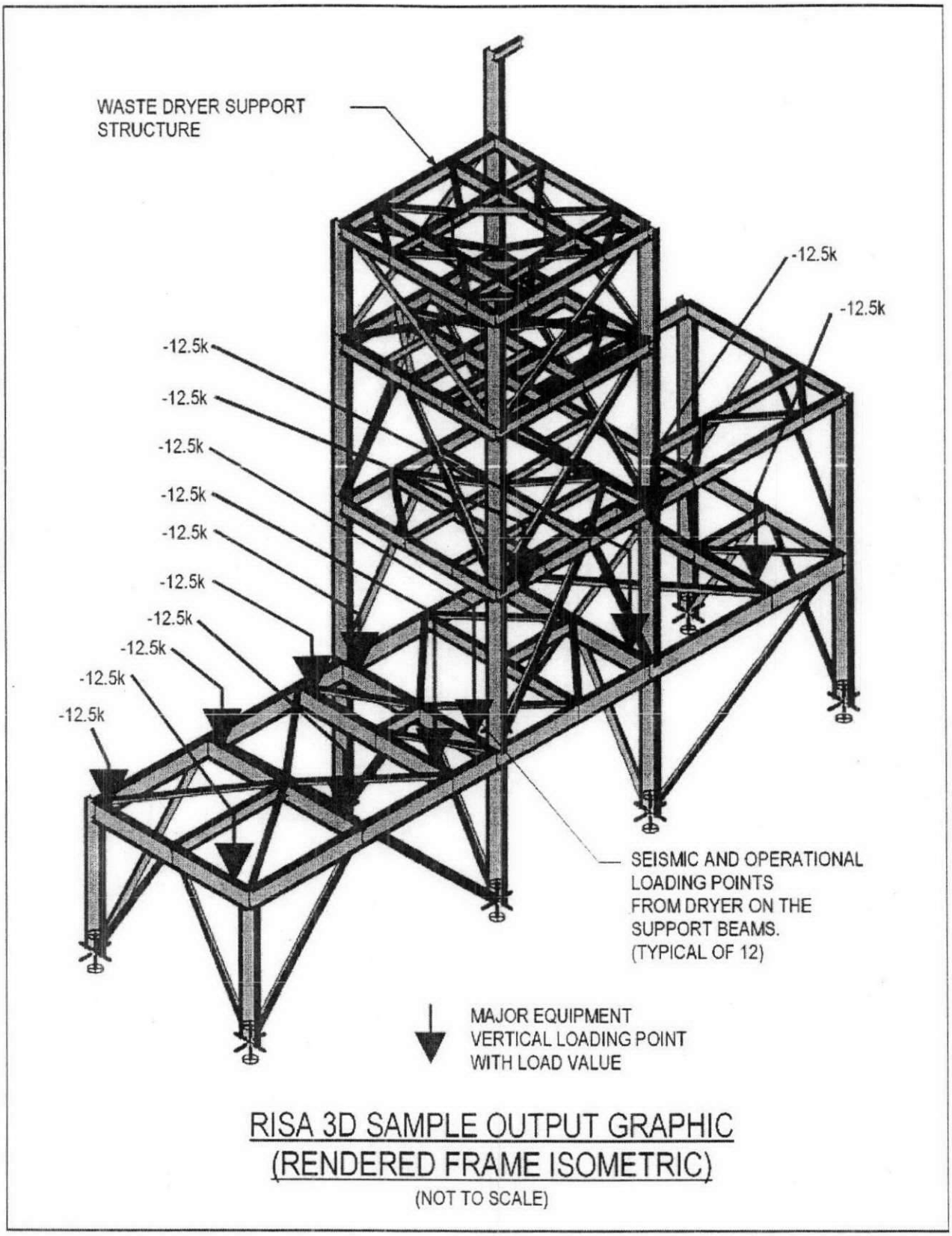


Figure 4 Rapid Interactive Structural Analysis (RISA) Sample Output

2.2.1.1.a Independent Modeling Results and Calculation Review

The magnitudes of the equipment loads were preliminary within the submitted calculation and are preliminary within the independent model since final equipment loads were not available from the vendors. Load distribution and application varied with the independent model and the submitted calculation in two areas. First, uniform live and dead loads were distributed to the secondary framing members within the independent model instead of applied directly to the main framing members as in the submitted calculation. Second, the dryer and associated equipment are contained within an independent enclosure. This enclosure is considered to be capable of carrying all the equipment loads since the enclosure will be lifted into place onto the support structure with the internal equipment installed. Following IQRPE review and comment, the submitted calculation was revised by AMEC to reflect the change from lateral load distribution from the enclosure to 12 locations, corresponding to structural cross framing on the structural and vertical load distribution, to only 4 points. The revised calculation eliminated eccentric moments on secondary members. The independent RISA model has considered both lateral and vertical load distributions to occur at all intersection structural cross framing, where there are 6 intersecting cross members for 12 locations.

Results from the independent model shows that the framing members and arrangements are now adequately designed to support the design loads.

2.2.1.1.b Other Structural Review Considerations

Other structures in the Waste Dryer System including the Dryer Chiller pump skid, Chiller Unit and Steam Supply System structures are not designated to store or treat dangerous waste, and therefore did not receive an IQRPE review in compliance with WAC standards.

Where possible, the IQRPE reviewed the Waste Dryer System report to ensure that the following activities were incorporated into the Technical Specifications as part of the design basis:

- Design parameters used in structural calculations are clearly indicated and labeled on clarifying sketches.

- Seismic considerations, which are appropriate to the seismic risk zone (UBC 1997, Seismic Zone 2B) are accounted for in the structural calculations.

- The foundation underlying the Waste Dryer System will support the load of a full tank plus the secondary containment structure per the requirements of WAC 173-303-640(3)(a)(v)(A). This was certified by the IQRPE as part of DR-002.

- The foundation underlying the Waste Dryer System has been designed to prevent failure due to settlement, compression, and uplift per the requirements of WAC 173-303-640(4)(c)(II). This was certified by the IQRPE as part of DR-002.

- The design plans require that homogeneous, porous, non-corrosive backfill material be placed below and around tank system foundations and underground piping to provide uniform structural support and prevent excessive settlement. This was certified by the IQRPE as part of DR-002.

- The tank systems have been designed to withstand the effects of frost heave per the requirements of WAC 173-303-640(3)(a)(v)(C). This was certified by the IQRPE as part of DR-002.

The following subsections highlight the IQRPE Structural Design Standard review for each of the major Waste Dryer System subsystems, and also identify specific exceptions to this IQRPE certification report as they relate to the structural review.

2.2.1.2 Dryer and Condensate Recovery System (SP-001 and SP-006)

This Technical Specification was reviewed to ensure that provisions for the proper loads, supports, and design basis had been incorporated. With the exception of those issues listed in Section 2.2.1.5 below, the appropriate structural considerations have been made.

2.2.1.3 Dryer Chiller Pump Skid and Chiller Unit (SP-005 and Data Sheet 143643-D-DS-039.1))

This Technical Specification was not reviewed to ensure that provisions for the proper loads, supports, and design basis had been incorporated, since the Chiller Pump Skid and Chiller Unit are not designated to store or treat dangerous waste and do not require IQRPE for review of structural calculations per WAC requirements.

2.2.1.4 Steam Supply System (SP-007)

This Technical Specification was not reviewed to ensure that provisions for the proper loads, supports, and design basis had been incorporated, since the Steam Supply System is not designated to store or treat dangerous waste and does not require IQRPE for review of structural calculations per WAC requirements.

2.2.1.5 Resolved IQRPE Structural Design Concerns

IQRPE Certification exceptions to the structural review are as follows:

1. AMEC calculation 145579-B-CA-012, Rev 1 did not comply with the 1997 UBC Section 2214.6.3.1 requirement for minimum forces in bracing connections. AMEC's use of the ASD compressive buckling strength of the brace as the maximum force that can be transmitted to the brace by the system, was an incorrect interpretation of Section 2214.6.3.1 subsection 3 of the code. The checker noted that revision 2 of the calculations corrected this issue by using subsection 2, omega times the force in the brace due to design seismic forces in combination with gravity loads.

2. AMEC Drawing No. F-145579-00-B-0001, Rev G, Structural Steel, General Notes, 6.1.2, indicated that "The design of the connections shall be the responsibility of the fabricator….". This practice is prohibited by the 1997 UBC Section 1633.2.3 which states that "Connections that resist design seismic forces shall be designed and detailed on the drawings." AMEC has corrected this by designing connections and detailing them on the drawings.

3. AMEC Drawing No. F-145579-00-B-002, Rev D, Figures 1-3 through 1-8, indicated examples and typical connection concepts, but lacked sufficient detail in terms of weld size, weld length, plate thickness, dimensions & bolting to meet the 1997 UBC Section 1633.2.3 requirements. AMEC corrected this on revised drawing F-145579-00-B-002, Rev E.

4. AMEC Drawing No. F-145579-00-B-0009, Rev F, Structural Steel Elevations and Details, indicated the correct "required design force" for the connections using omega times the "seismic service force in the brace" criteria. (220% of the design service load in the brace); however, the referenced forces indicated for the braces are not "required service design forces" and lack the 150% increase required by Section 2214.6.4 of the 1997 Uniform Building Code for chevron bracing. This is potentially confusing, since it is inconsistent with the criteria used for the listed connection forces. It was recommended that brace forces shown on the drawings be revised to "required service design force" similar to the indicated connection forces. AMEC corrected the notation on the revised drawing F-145579-00-B-0009, Rev G.

5. AMEC Drawing F-145579-00-B-0009, Rev F, Structural Steel Elevations and Details, Section D, lacked weld length, weld size, side plate thickness, gusset plate to column weld information and other information necessary to comply with 1997 UBC Section 1633.2.3. AMEC corrected this on the revised drawing F-145579-00-B-0009, Rev G.

6. Although calculations were made to justify the adequacy of a non-building structure using mixed x-bracing, inverted chevron bracing, non-symmetrical bracing and no bracing at all creating a soft story, this type of system and the use of chevron bracing in seismic zones, especially for hazardous classification structures is not generally advised. The 1999 SEAOC blue book comments on this in Section C704.9. It should also be noted that non-building structures typically lack the damping characteristics of buildings, since they lack siding, diaphragms and other components that contribute to energy dissipation. Thus they are generally more susceptible to seismic damage than a similar type building would be. These issues were reviewed with AMEC and it was determined that piping and equipment interferences with bracing determined the type of bracing that was utilized. Since AMEC showed code compliance with their calculations, the design was determined to be adequate.

7. AMEC calculation 145579-B-CA-012, Rev 2 provides the technical basis for the structural design of the DBVS waste dryer support structure along with Drawing No. F-145579-00-B-0008, Rev F and Drawing No. F-145579-00-B-0009, Rev F. In lieu of performing a line-by-line review of the calculation, an independent model was created within RISA 3D Version 5.0d using loading conditions identified within calculation 145579-B-CA-012, Rev 2 and framing arrangements depicted on Drawing No. F-145579-00-B-0008, Rev F and Drawing No. F-145579-00-B-0009, Rev F.

8. AMEC Drawing No. F-145579-00-B-0009, Rev F, showed inconsistent views between Elevation on BL 'Dc', Elevation on BL 'Db', Elevation on BL 'D2', and Elevation on BL 'D1". This was corrected on AMEC Drawing F-145579-00-B-0009, Rev G.

These issues were identified by the IQRPE review and have been resolved.

2.2.1.6 Structural Design Exceptions

There are no exceptions to the IQRPE certification of the structural design assessment.

2.2.2 Waste Compatibility

Ecology (1995) requires that an IQRPE certify that the proposed tank system has been designed of materials compatible with the waste to be stored or treated. Information regarding the waste properties to be stored and treated in the Waste Dryer System is included in the RCRA RD&D Permit, Attachment BB, Section 6.2.3 and Tables 6-2 through 6-6. The Campaign Plans will describe spiking materials and their concentrations, if any, to be added to the waste feed for each ICV. Whenever the potential exists for appreciable increased risk of corroding or causing a leak or rupturing DBVS waste contracting components, an independent qualified corrosion engineer must evaluate the extent of this risk. WAC 173-303-640(3)(a) requires that the proposed materials for the waste dryer system be evaluated for compatibility with the wastes to be stored or treated. WAC 173-303-640(5)(a) requires that the proposed dangerous wastes or treatment reagents may be placed into the proposed waste dryer system without causing the tank or vessel system to rupture, leak, corrode, or otherwise fail.

The IQRPE reviewed the waste property information in conjunction with the design specifications. Properties of the waste stream have been identified in applicable technical specifications for compatibility to the assembled system (see Table 1, Section 2.2 of this report). Waste design compatibility aspects which have been specified include piping and equipment material selection, wall thickness corrosion allowances, enclosure insulation, enclosure freeze protection, and HEPA filtration of potentially contaminated ventilation exhaust and airborne contamination.

The following subsections highlight the IQRPE Waste Compatibility review for each of the major Waste Dryer System subsystems and specific exceptions to this IQRPE certification report as they relate to the Waste Compatibility review.

2.2.2.1 Dryer and Condensate Recovery System (SP-001 and SP-006)

Although specific proposed waste property constituents have been outlined, the degree of corrosion to be expected as a result of the interaction between the waste and proposed construction materials is not a trivial matter. To a large degree, corrosion rates can be expected to be minimal due to the reported pH range (8-13). However, testing will need to be completed to verify this conclusion.

PNNL is conducting bench scale testing to evaluate processing and also to provide observations for corrosion/erosion of materials. It will be imperative to collect corrosion measurements during this testing. Later, during actual system operations it recommended that the use of corrosion coupons be employed to yield valuable information as to the corrosive nature of the process fluid in contact with the proposed containment materials.

The IQRPE concurs that this 90 % design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640(3)(a) and (5)(a), subject to final IQRPE review of results from PNNL materials bench scale testing.

2.2.2.2 Dryer Chiller Pump Skid and Chiller Unit (SP-005 and Data Sheet 143643-D-DS-039.1)

This Technical Specification was not reviewed to ensure that provisions for waste compatibility have been incorporated into the specifications, since the Chiller Pump Skid and Chiller Unit are not designated to store or treat dangerous waste and do not require IQRPE for review of for waste compatibility per WAC requirements.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.2.3 Steam Supply System (SP-007)

This Technical Specification was not reviewed to ensure that provisions for waste compatibility have been incorporated into the specifications, since the Steam Supply System is not designated to store or treat dangerous waste and does not require IQRPE for review of for waste compatibility per WAC requirements.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.2.4 Waste Compatibility Exceptions

IQRPE Certification exceptions to the waste compatibility review are as follows:

- Prior to final acceptance of the proposed construction materials, results of the bench scale testing compatibility with the waste will need to be reviewed by the IQRPE. Corrosion measurements may indicate that the proposed materials are not compatible with the waste products.

Refer to Attachment E, Corrosion Engineering Review, for additional discussion on waste compatability.

2.2.3 Pressure Control System

Ecology (1995) requires that an IQRPE certify that the proposed tank system has been designed with appropriate pressure control systems. Pressure control system information to be submitted by the Seller and reviewed by the IQRPE at a later date is listed in Attachment B.

The following activities have been conducted in the review of the design standards for the Waste Dryer System:

- The Technical Specifications include an acceptable preliminary piping and instrumentation system that will allow for adequate pressure control, per the requirements of WAC 173-303-640(3)(a).

- The Technical Specifications include the following basis for component selection and design basis of pressure control:
  - Vessel operating and design pressures and temperatures
  - Process and relief required flow rates
  - Relief piping size and ratings
  - Pressure ratings of equipment
  - Locations of pressure relief vents and other pressure controls
  - The pressure control system discharge locations

The following subsections highlight the IQRPE Pressure Control System review for each of the major Waste Dryer System subsystems, and also identify specific exceptions to this IQRPE certification report as they relate to the pressure control system review.

2.2.3.1 Dryer and Condensate Recovery System (SP-001 and SP-006)

The Dryer vessel is specified for full vacuum operation. The vessel is to be operated at 26 inches Hg with a maximum of 75 psig external design pressure. The vessel is structurally designed for 5 psig internal pressures, while the steam jacket is specified and stamped per the ASME B&PV Code, Section VIII. A rupture disc on the Dryer vessel is specified at a fixed relief pressure of 5 psig @ and relieves to the dryer offgas system. The rupture disc is also specified to accommodate up to a maximum worst case temperature of 250 deg F. Vendor data for the rupture disc will be evaluated by the IQRPE upon receipt of the Dryer skid design. The 6" relief pipe is adequately sized.

The steam jacket around the pulse back filter is designed to operate at a maximum of 75 psig and is specified to ASME B&PV Code Section VIII. Condensate from the pulse back filter drains through a steam trap to the Waste Dryer Steam Condensate Tank. Presently the pulse back filter steam jacket does not have relief valve protection and this is recommended for consideration be added by the IQRPE and confirmed with the final design.

The Waste Dryer Steam Condensate Tank 33-D74-022 is not shown with overpressure relief protection. Failure of an inlet steam trap would result in application of full steam pressure to the tank. The IQRPE recommends that overpressure protection to this tank be considered to be added and confirmed with the final design.

The Waste Dryer and Condensate Recovery System Enclosure is protected against overpressure due to a pathway for reverse air inherent in the existing design of the ambient air HVAC supply enclosure inlet HEPA filter housing design.

The Waste Dryer Off-gas Condensate Tank 33-D74-015 and Waste Gas Vacuum Off-gas Condenser Tank were evaluated for acceptance per ASME Section VIII, NC-7000 to not having specific overpressure protection. The IQRPE acknowledges that operating and design maximum pressures are low (<20 psig or vacuum), and additional relief protection is not required.

Overpressure of the Waste Gas Dryer vacuum pump did not receive IQRPE review, since the Technical Specification for supply of the Waste Gas Dryer Vacuum Pump shall be a purchase specification that places the responsibility for the final design of the system components on the Seller and was not included in the Waste Dryer System Design Review Package, and is therefore recommended to be confirmed with the final design.

The Waste Dryer and Condensate Recovery System piping and fittings have been specified such that protection from overpressure is maintained. Specific selection of pipe sizes, wall thickness, pipe pressure ratings and material selection corresponding to individual pipe numbers was not reviewed by the IQRPE since of final design piping line class sheets were not available. IQRPE recommends confirmations with the final design.

The Waste Dryer Hydraulic drive system is included in scope for the Dryer System per specification 143643-D-SP-001. Hydraulic tank 33-D74-077 shown on F-145579-33-A-0101 does not show an atmospheric vent nor overpressure protection. Relief protection is required for the hydraulic tank, unless this is designated and shown to be an atmospheric vented tank. Overpressure protection of hydraulic pumps and piping is included in the design.

The Waste Dryer Hydraulic Recirculation pump discharge and return are shown with no throttle valves, thus not requiring overpressure protection. If valves are added anywhere in supply or return piping to the Waste Dryer Motor Case, such as for isolation capabilities of FI-137, then overpressure protection of the hydraulic circuit should be added to the design.

2.2.3.2 Dryer Chiller Pump Skid and Chiller Unit (SP-005 and Data Sheet 143643-D-DS-039.1)

Chilled water overpressure protection at the Waste Dryer Condenser and the Waste Dryer Offgas Condenser did not receive IQRPE review, since condenser data sheets were not included in the Waste Dryer System Design Review Package. Completed Waste Dryer Condenser and the Waste Dryer Offgas Condenser data sheets should be provided and verified by IQRPE with the final design, showing that the condenser design pressure (chilled water side) exceeds the maximum pressure potential available per the chilled water pump shutoff head pressure.

In addition to the above paragraph, this Technical Specification was reviewed to ensure that provisions for waste compatibility have been incorporated into the specifications. The Dryer Chiller Pump Skid and Chiller Unit are not designated to store or treat dangerous waste.

IQRPE review of the Waste Dryer Condenser and the Waste Dryer Offgas Condenser final design data sheets for compliance with the DBVS RD&D Permit and WAC 173-303-640, must be sufficiently addressed in the Final Installation Package.

2.2.3.3 Steam Supply System (SP-007)

This Technical Specification was reviewed to ensure that provisions for pressure control have been incorporated into the specifications. The Steam Supply System is not designated to store or treat dangerous waste.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.3.4 Pressure Control System Exceptions

Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place the responsibility for the final design of the system components on the Seller; thus a complete review of the final pressure control system has not been completed at this time.

Exceptions cited below by the IQRPE in meeting the final design requirements of the DBVS RD&D Permit and WAC 173-303-640, must be sufficiently addressed in the Final Installation Package.

- Pressure relief protection should be added to the compressed air accumulator which feeds the pulse back filter. The upstream mechanical pressure control valve (PCV) does not constitute adequate pressure protection, since PCV's can fail open, and the accumulator design pressure (58psig) is considerably less than the compressed air discharge pressure (150 psig).

- Waste Dryer Condenser and the Waste Dryer Offgas Condenser data sheets should be verified when vendor information is available, to show that these condenser design pressures exceed the maximum chilled water pump shutoff head pressure.

- Completed Waste Dryer Condenser and the Waste Dryer Offgas Condenser data sheets should be provided as part of the installation assessment report, and verified by IQRPE with the final design, showing that these condenser design pressures (chilled water side) exceed the maximum chilled water pump shutoff head pressure.

2.2.4 Secondary Containment System

Ecology (1995) requires that an IQRPE certify that the proposed tank system has been designed with appropriate secondary containment system. Secondary containment for tank systems that store, accumulate, or treat dangerous waste must be designed and installed to meet the requirements of WAC 170-303-640(4)(b). A review of the secondary containment system is normally part of the IQRPE review. Because the Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place the responsibility for the final design of the system components on the Seller, a complete review of the secondary containment system has not been completed.

Secondary containment system information to be submitted by the Seller and reviewed by the IQRPE at a later date is listed in Attachment B.

The following has been considered in the review of the design standards for the Waste Dryer System:

- The system is designed to prevent any migration of wastes or accumulated liquid out of the secondary containment system to the soil, groundwater, or surface water at any time during the use of the tank system.

- The system is capable of detecting and collecting releases and accumulated liquids until the collected material is removed.

- The system is specified of materials that are compatible with the wastes to be placed in the tank system.

- The system has been specified to have sufficient strength to withstand stresses due to static head during a release, pressure gradients, climatic conditions, nearby vehicle traffic, and other stresses resulting from daily operations.

- The system will be placed on a foundation or base that will support the secondary containment system, provide resistance to pressure gradients above and below the system and prevent failure due to excessive settlement, compression, or uplift.

- The system will be provided with a leak detection system that will detect the failure of either the primary or secondary containment structure or the presence of any release of dangerous waste or accumulated liquid in the secondary containment system within 24 hours (or at the earliest practicable time if the owner or operator can demonstrate to Ecology that existing leak detection technologies or site conditions will not allow detection of a release within 24 hours.)

- The system will be sloped or otherwise designed or operated to drain and remove liquids resulting from leaks, spills, or precipitation.

The following subsections highlight the IQRPE Secondary Containment System review for each of the major Waste Dryer System subsystems and specific exceptions to this IQRPE certification report as they relate to the secondary containment system review.

2.2.4.1 Dryer and Condensate Recovery System (SP-001 and SP-006)

The Waste Dryer is specified to contain seals designed to preclude leakage of contaminated materials. Included are three installed spare seals, a secondary sealed enclosure built around the dryer shaft seal to contain any potential leak; a gravity drain through a drain line; and seals in potential contact with liquid salt-solution specified for compatibility with the liquid salt-solution properties as specified.

The DCRS skid assembly confinement system (enclosure) is specified to provide secondary confinement for the dryer, sintered metal filter, and condensate recovery skid. The DCRS enclosure is also specified to provide a leak detector sump so the leak detector can sense a minimal amount of liquid waste "in the unlikely event of a leak". The sump is specified to have a pump out port that is valved and capped or plugged for removal of any liquid contained in the DCRS skid assembly. The DBVS detectable leak volume for the Waste Dryer system is calculated in Calculation 145579-D-CA-030 and was reviewed by the IQRPE. The DCRS enclosure floor is specified with a stainless steel floor pan, extending to the walls of the DCRS container assembly, and to a height enabling the pan to hold 8 inches of water. The floor pan seams are specified to be seal welded and water tight,

or the floor and floor pan may be one in the same. The enclosure is specified to meet requirements of Series 1 freight containers in accordance with applicable ISO standards, designed to contain leakage. Enclosure drainage is specified to drain from walls to the floor to a floor sump via a floor drain as shown on drawing DBVS-SK-M109.

The enclosure personnel access door has been specified as elastomeric-gasket sealed, leak-tight metal marine-type personnel door. Enclosure inlet and outlet piping connections have been specified to mate with HIHTL connections as shown on drawings DBVS-SK-M103 and 109. The enclosure has been specified to air leak test acceptance criteria in accordance with ISO 1496-2. The enclosure lid is specified to be gasketed with a continuous sealing surface between the lid or module contact surfaces, designed to be assembled without detrimentally affecting the sealing surface. Interior walls, doors and ceiling of the enclosure are specified to be lined with 300 series stainless steel sheeting with seams designed to prevent leakage into the walls, designed to accept decontamination sprays.

The Waste Dryer System enclosure is designed to be ventilated with outside air drawn through an inlet HEPA filter, passing through the enclosure and flowing out the outlet HEPA filter to a negatively pressurized dried waste handling system.

The inlet HEPA filter to the Enclosure is also not intended for reverse flow. Thus if the enclosure becomes over-pressurized, it is postulated that the barrier of the inlet HEPA filter could possibly be breached to the environment, however, a search of the WAC indicates this failure would not result in loss of secondary containment. Sources of positive pressure in the Enclosure include the steam and compressed air systems..

Specification 006 describes butterfly valves used to balance the enclosure outlet HEPA filter air flow, using a manual preset damper. Calculation CA-033 requires a 650 cfm air flow to maintain an internal enclosure temperature not to exceed 115 deg F. Actual ventilation air flow rate depends on the setting of the manual HEPA dampers as well as a fluctuating exhaust duct system resistance caused from variable flows of Waste Dryer material processed through the solids chute connected with the HVAC. Thus accurately controlling cooling air flow through Dryer Enclosure equipment spaces is susceptible to poor air flow control, and thus poor air temperature control. This is design approach is not recommended for the following reasons:

- Inability to accurately control HEPA exhaust air flows and temperatures.
- Connecting a ventilation system to a contaminated process solids stream that has the potential for off-normal reverse flow pressure transient of contaminated materials or dust, possibly breaching the secondary confinement HEPA confinement barrier through a HEPA filter that is not designed for back flow prevention.
- Difficulty in adjusting manual balancing dampers located in a normally sealed secondary confinement cubicle. Variable solids flow in the Waste Dryer outlet chute would require variable adjustments of HVAC air flows, which cannot be accomplished using pre-set manual dampers.
- HEPA air flow exhaust into the negatively pressurized Waste Dryer discharge chute compromises the operational ability to increase negative suction pressures to enhance movement of contaminated Dryer waste solids, which may become necessary.

Because the Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place the responsibility for the final design of the system components on the Seller, a complete review of the secondary containment system has not been completed.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640; with the exception of items noted above, which must be sufficiently addressed in the Final Installation Package.

2.2.4.2 Dryer Chiller Pump Skid and Chiller Unit (SP-005 and Data Sheet 143643-D-DS-039.1)

These Technical Specifications were reviewed to ensure that provisions for secondary containment have been incorporated into the specifications. The Dryer Chiller Pump Skid and Chiller Unit are not designated to store or treat dangerous waste.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.4.3 Steam Supply System (SP-007)

This Technical Specification was reviewed to ensure that provisions for secondary containment have been incorporated into the specifications. The Steam Supply System is not designated to store or treat dangerous waste.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.4.4 Secondary Containment System Exceptions

Because the Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place the responsibility for the final design of the system components on the Seller, a complete review of the secondary containment system has not been completed.

The IQRPE concurs that this design basis meets the requirements of the DBVS RD&D Permit and WAC 173-303-640; with the exception of items noted below, which must be sufficiently addressed in the Final Installation Package.

1. The waste dryer system receives waste for processing from the liquid waste staging tanks via the waste transfer pump skid. P&ID F-147779-33-A-0100 Bulk Vitrification Waste Dryer shows a sump instrumented with liquid level alarm. The liquid waste line is a Hose-In-Hose-Transfer-Line (HIHTL) from the staging tanks via the transfer pump skid. If a leak occurs in the liquid waste line inside the waste dryer enclosure, there are no overfill prevention controls or devices as required "at a minimum" in WAC 173-303-640(5)(b) to prevent overfill or spills. The current design of a leak detector activating an alarm annunciating in the control trailer, places reliance on control operator action to shut down the waste transfer pump to avoid sump overflow. "Operator action" is not

described as included "at a minimum" subparagraphs (i), (ii), (iii) of WAC 173-303-640(5)(b) as means of minimum controls to prevent spills.

2. Design features for prevention of contamination of sealing liquid for the small tank for the liquid ring vacuum pump should be addressed. This tank 33-D74-033 is being added to the RD&D permit table IV.1 based on comments from Ecology. It will be managed as a RCRA-regulated tank. Compliance of the tank with requirements and confirmation of the above, will be verified by the IQRPE during the installation assessment.

    a. The IQRPE review did not specifically review radiation monitors, however, an interlock from RIT-019 (or possible future fixed head air sampler) shown on P&ID F-145579-33-A-0100 to the liquid waste staging tank system could possibly mitigate a leak into the waste dryer system enclosure.

    b. The Enclosure HVAC design presents a strong potential for lack of adequate cooling flow and temperature control of the Waste Dryer and Condensate System Enclosure during hot summer conditions. Environmental upper operating limits of equipment and instrumentation inside the enclosure may be challenged. Enclosure cooling is dependent upon the operating status of downstream valves, filters and vacuum pump in the dried waste receiver system.

2.2.5 Ancillary Equipment Design

Ecology (1995) requires that an IQRPE certify that the proposed tank system has been designed with appropriate ancillary equipment (piping, fittings, flanges, valves and pumps) in accordance with the requirements of WAC 170-303-640(3)(f) and (4)(f). A review of the ancillary equipment design is normally part of the IQRPE review. Because the Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place responsibility for the final ancillary configurations and the purchase of all piping, fittings, flanges, valves, pumps, instrumentation, valves, and electronics on the Seller, a complete review of the ancillary equipment design cannot be completed until final 100% design information is available for IQRPE review.

Ancillary equipment design information to be submitted by the Seller and reviewed by the IQRPE at a later date is listed in Attachment B.

The following observations were made during the review of ancillary equipment design standards for the Waste Dryer System:

- Ancillary equipment inside Dryer System secondary containment cannot be visually inspected for leaks on a daily basis.

- Secondary containment has been provided for flanges, joints, and valves and other connections regardless of whether or not they are welded to the piping and visually inspected for leaks on a daily basis.

- Secondary containment has been provided where pumps and valves transfer dangerous wastes between tanks regardless of whether they are seamless and can be visually inspected on a daily basis.

- Tank system ancillary equipment is designed to be supported and protected against damage and excessive stress due to excessive settlement, vibration, expansion or contraction. (Note that equipment to be supplied by the Seller is not yet available for IQRPE review).

- Overfill prevention equipment (includes automatic shutoff controls, high liquid level sensing and high level alarms) has been specified, to warn the operator and/or to shutdown transfer pumps when tank system capacity is reached.

The following subsections highlight the IQRPE Ancillary Equipment Design review as applied to the specifications, P&IDs, and data sheets; and also identifies specific exceptions to this IQRPE certification report as they relate to the ancillary equipment design review.

2.2.5.1 P&ID Review

All P&IDs were reviewed for the following basic considerations:

- Appropriate location of pressure, temperature, and flow sensing equipment.
- Necessary piping, valve, and instrumentation labeling.
- Proper positioning of instrumentation to prevent undue influence from upstream equipment.
- Necessary isolation valves to allow instrumentation maintenance.
- Identification of preliminary interlocks.
- Designation of valves as fail-open or fail-close.
- Location of check valves or back-flow preventers.
- General designation of appropriate alarms and recorded information.
- Overpressure protection

2.2.5.2 Data Sheet Review

Data sheets are generally incomplete or missing and are required for the 100% IQRPE design review. This review shall include:

- Appropriate materials of construction

- Appropriate functionality

- Hazard classification requirements

2.2.5.3 Instrument Loop Diagram Review

IQRPE review of instrument loop diagrams included identification of the appropriate wiring and terminations at the local instruments, junction boxes, termination panels, and MCS.

2.2.5.4 Ancillary Equipment Exceptions

Because the Technical Specifications prepared for the Waste Dryer System IQRPE/RCRA Design Review Package are purchase specifications that place the responsibility for the final design of the system components on the Seller, a complete review of the secondary containment system has not been completed.

No ancillary equipment exceptions were cited by the IQRPE in meeting the final design requirements of the DBVS RD&D Permit and WAC 173-303-640.

2.2.6 Corrosion Assessment

Ecology (1995) requires that an IQRPE certify that the proposed tank system has been designed of materials compatible with the waste to be stored or treated. Information regarding the waste properties to be stored and treated in the Waste Dryer System is included in Technical Specification 145579-D-SP-006 *Dryer and Condensate Recovery System Skid* Tables 3-3 and 3-4 and also in the RCRA RD&D Permit, Attachment BB, Section 6.2.3 and Tables 6-2 through 6-6.

The IQRPE reviewed the waste property information in conjunction with the design specifications. Properties of the waste stream have been identified in applicable technical specifications for compatibility to the assembled system (see Table 1, Section 2.2 of this report). Waste design compatibility aspects which have been specified include piping and equipment material selection, wall thickness corrosion allowances, enclosure insulation, enclosure freeze protection, and HEPA filtration of potentially contaminated ventilation exhaust and airborne contamination.

Although specific proposed waste property constituents have been outlined, the degree of corrosion to be expected as a result of the interaction between the waste and proposed construction materials is not a trivial matter. To a large degree, corrosion rates can be expected to be minimal due to the reported pH range (8-13), however, testing will need to be completed to verify this conclusion.

The following subsections highlight the IQRPE Waste Compatibility review for each of the major Waste Dryer System subsystems and specific exceptions to this IQRPE certification report as they relate to the Waste Compatibility review.

2.2.6.1 Dryer and Condensate Recovery System (SP-001 and SP-006)

In accordance with Technical Specifications 143643-D-SP-001 Rev. 0 Dryer and Condensate Recovery System and 145579-D-SP-006 Dryer and Condensate Recovery System Skid, the following precautions have been made to minimize instances of a corrosion related failure and subsequent release of waste product:

1. The use of stainless steel and coated carbon steel materials.

2. Corrosion allowances for the specified materials, including additional wall thickness for metals in contact with the waste solution.

3. Maximum 5 year system design life.

4. Bench scale dryer testing to be performed by the Pacific Northwest National Laboratory in support of the DBVS.

As part of the bench scale testing, it is imperative that corrosion related data is collected concerning the interaction of the waste products and proposed construction materials. Although waste characteristics have been presented (Specification 145579-D-SP-006 Table 3-3) including range of fluid pH and temperatures, actual corrosion rates will need to be quantified as part of the testing process.

As currently specified, protective coating information including material selection, surface preparation, environmental controls, application procedures, and inspection requirements have been left to the discretion of the Seller. This information is to be provided to the Buyer for review and approval prior to fabrication; however, for materials in contact with the waste fluid, project specific coating specifications should be developed and issued with the design package. This will ensure that the protective coatings will be compatible with the materials and environments to which they are exposed. In addition, provisions should be made for 3rd party coating inspection to be completed.

2.2.6.2 **Steam Supply System** (SP-007)

The portion of the Steam Supply System requiring corrosion control consideration in accordance with WAC-173-303-640 includes the diesel fuel tank.

The diesel fuel tank (33-D74-063, drawing F-145579-00-D-0028) used to supply fuel to the boiler system will be located above grade. A properly specified coating system should be applied to the exterior of the tank to provide a degree of protection against atmospheric corrosion. If the tank is to be used for more than five years, consideration should be given to providing cathodic protection to the tank surfaces in contact with the support pad.

2.2.6.3 **Dryer Chiller Pump Skid and Chiller Unit** (SP-005 and Data Sheet 143643-D-DS-039.1)

Specification 145579-D-SP-005 describes the requirements of the Dryer Chiller Pump Skid. The components associated with this portion of the Waste Dryer System are not subject to the requirements of WAC 173-303-640 in accordance with Waste Compatibility.

Additional corrosion review comments concerning DBVS Waste Dryer System are included as Attachment E, "Corrosion Engineering Review".

2.2.6.4 **Corrosion Assessment Exceptions**

The following observations have been made in the review of the design standards for the Waste Dryer System:

1. Prior to final acceptance of the proposed construction materials, results of the bench scale testing will need to be reviewed. Corrosion measurements may indicate that the proposed materials are not compatible with the waste products.

2. The final design should provide for the installation of corrosion coupons installed directly into the waste product stream at appropriate locations. This will provide information as to the corrosion resistance of various alloy materials to the waste fluid.

3. Coating specifications should be developed for external surfaces of materials which will be in contact with the waste products.

4. 3rd party coating inspection should be completed at specific hold points as described in the coating specifications.

2.2.7 Recommended Inspection Schedule

Waste Dryer System inspections as listed below are recommended during construction and assembly of the Waste Dryer System before it is placed into operation.

2.2.7.1 Construction Inspections

Adequate tank and system design will not necessarily ensure dangerous waste system installation. "Guidance for Assessing and certifying Tank Systems that store and treat Dangerous Waste (Ecology Publication 94-114, June 1994) describes "Inspecting Tank System Installations" in Chapter 4. The Waste Dryer System contains systems which receive and process dangerous waste from tanks; therefore this publication is determined applicable to the Waste Dryer System.

The integrity of a tank system is determined to a great extent by the quality of the installation. Disciplined inspections to established acceptance criteria are recommended to be conducted at the site throughout the scheduled construction to verify that specified construction requirements are satisfied in accordance with the approved design specifications, drawings and regulatory requirements. Construction inspections are recommended to be spot checked to ensure due diligence, and are not a substitute for a thorough execution of the Quality Assurance/ Quality Control program. DBVS Construction Inspections should be comprehensive, including civil, structural, mechanical, electrical, controls and instrumentation construction inspections. Accurate records must be kept and recorded in a IQRPE inspectors' database to properly track Inspections, Findings, Resolutions and Acceptance by the IQRPE and Buyer. The IQRPE is recommended to perform inspection walkdowns and coordinate with IQRPE inspectors to inspect and document ongoing and completed construction. Written statements by the IQRPE should be provided, attesting that the Waste Dryer System and interconnecting subsystems have been constructed in accordance with specified requirements, as per WAC 173-303-810 (13)(a).

Before placing Waste Dryer Systems into service, which store or process hazardous waste, the associated equipment skids will be inspected by an IQRPE for structural damage and proper installation. The qualified independent inspector or IQRPE will also review the vendor inspection and testing reports, as they are available. Applicable IQRPE fabrication and construction inspections include the following:

- Evaluation of the welds to verify no cracking or lack of fusion.

- Confirmation that no punctures, scrapes of protective coating, cracks, corrosion, or other structure damage are present.

- Review of "tightness testing" (hydrostatic, leak tests, and secondary confinement enclosure leak tests, duct leakage tests and results) to verify no leaks are present through visual inspection and pressure testing, and that pressure or vacuum meets leak test acceptance criteria specified over the test period.

- Review ductwork pressure tests to the relatively high specified pressure (minus 30" W.G.) requirements to ensure integrity is maintained and damage prevented during testing.

- Review of Construction Acceptance Tests including equipment functional checkout tests, valve actuation tests, electrical continuity tests, valve limit switch tests, motor bumping tests, instrumentation functionality tests, interlock and control circuit loop tests.

- Review of a fully integrated pre-operational acceptance test, conducted by representatives of the Buyer, to verify correct operability of all interlocks, wiring, electrical components, instruments, logic, valves and equipment, for both "normal" and "off-normal" conditions, prior to the start of stimulant.

- Verification of the protection of ancillary equipment against physical damage and stress.

- Critical dimension inspections of the DCRS skid assembly within specified tolerances.

- Review of Factory Acceptance Test procedures and test results prior to shipment, including but not limited to electrical circuits and device operation, proper instrumentation operation, valve actuation checkouts.

- Erection and field assembly of Waste Dryer System.

- Installation of secondary containment enclosure.

- Proper filter installations.

- Installation of cathodic protection systems if applicable.

- Installation inspection that conforms to consensus-recognized standards including the documentation of findings and corrective actions documented in a post-inspection report.

- Visual inspections and filtration testing of HVAC filter housing assemblies in accordance with the requirements of ASME N510 (SP-006).

- Review of approved non-destructive procedures and testing results from the following field construction NDT examinations: visual weld examinations, radiography, liquid dye penetrant tests, ultrasonic inspections.

2.2.7.2 Recommended Inspection Exceptions

IQRPE Certification exceptions to the recommended inspection assessment review are as follows:

- The recommended inspection activities described in this section are based on the design basis operating life, operating conditions, and waste characteristics outlined in the Design Basis

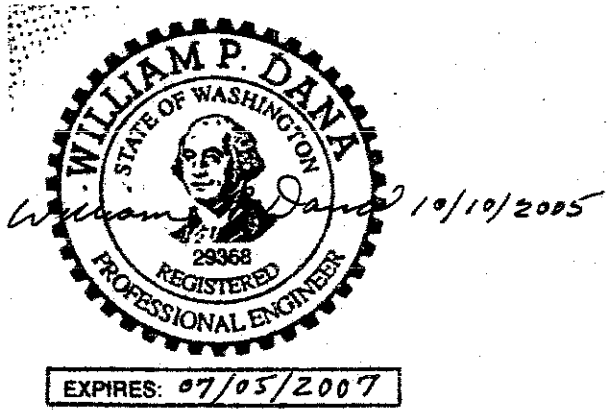
Report. Should any of these parameters change (for example: extended operating life, increased operating temperatures, lower waste Ph), the inspection schedule must be re-evaluated by the IQRPE.

3.0 DESIGN REVIEW ASSESSMENT CERTIFICATIONS

The Waste Dryer System IQRPE/RCRA Design Review Package, RPP-24544, Revision C for System 2.2, has been reviewed by the IQRPE and, with the exceptions listed herein, was assessed to be in compliance with the applicable sections of WAC 173-303-640 and the RD&D Permit for the DBVS as stated in Section 1.4 of this report. These results are based on a review of the applicable codes, standards, and documents. The certifications below are in accordance with the requirements of WAC 173-303-640(2)(b) and 173-303-810(13)(a).

Report Lead IQRPE:

I certify under penalty of the law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine or imprisonment for knowing violations.



10/10/2005

Report Reviewed by:

Robert L. Goodman, PE — 10 Oct 05.

Karl M. Walterskirchen, PE — Date

Chief Engineer, TGS

4.0 REFERENCES

WAC 173-303-640 Tank System Used to store or Treat Dangerous Waste, February, 2005

WAC 173-303-810 General Permit Conditions, February, 2005

WA Dept of Ecology Publication 94-114, Guidance for Assessing and Certifying Tank Systems that Store and Treat Dangerous Waste, June 1994

WA Dept of Ecology Publication 95-420 Guidance for Assessing Dangerous Waste Secondary Containment Systems, June 1994

CH2M Hill Hanford Group, Inc. Statement of Work, Requisition 114648, "Independent Qualified Registered Professional Engineer support to Demonstration Bulk Vitrification System Project"

RPP-24544. 2004. Demonstration Bulk Vitrification System IQRPE/RCRA Design Review Package, Revision 0. February 21, 2005

WA Dept of Ecology Permit No. WA 7890008967, Permit for Dangerous and/or Mixed Waste Research, development and Demonstration

RPP-17403. 2004 "Function and System Design Requirements for the Demonstration Bulk Vitrification System." CH2M Hill Hanford Group, Inc. Revision 2.

HNF-SD-GN-ER-501, Rev. 1B, "Natural Phenomena Hazards, Hanford Site, South Central Washington."

RD&D Permit DOE/ORP-2003-23, Rev 1 May 2004 Section 6 "Waste Analysis Plan"

AISC Manual of Steel Construction- Allowable Stress Design, 9th edition

ASHRAE Fundamentals Handbook, 2001

ASME Boiler & Pressure Vessel Code, Section VIII Pressure Vessels, Section IX Welding

ASME B31.3 Process Piping

ASME N510, Testing of Air Treatment Systems

ASNT SNT-TC-1A, Recommended Practice for Nondestructive Testing

ISO 668, 1161, 1496-2, Series 1 Freight containers

UBC 1997 Uniform Building Code

STAAD-Pro structural Software

Rigid Interactive Structural Analysis (RISA) 3D, Rev 5D Software

1999 Structural Engineers Association of California (SEAOC) Recommended Lateral Force Requirements and Commentary

ASTM A999/A 999M, Standard Specification for General Requirements for Alloy and Stainless Steel Pipe, American Society of Testing and Materials, West Conshokocken, Pennsylvania

Nickel Development Institute, Design, Water Factors Affecting Service- Water Piping Materials, NiDI Technical Series No. 10043, Toronto, Ontario

NORSOK Standard L-CR-004, Common Requirements- Piping Fabrication, Installation, Flushing and Testing, Norway

ATTACHMENT A

WASTE DRYER SYSTEM

IQRPE DISPOSITION OF CALCULATIONS, SPECIFICATIONS, AND DRAWINGS

ATTACHMENT A

WASTE DRYER SYSTEM

IQRPE DISPOSITION OF CALCULATIONS, SPECIFICATIONS, AND DRAWINGS

Document Number	Document Title	Comments
Calculations		
145579-B-CA-012 Revision 2 Appendix A2	Waste Dryer Support Structure	This calculation was reviewed and independently modeled and checked. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-B-CA-004 Revision B Appendix A2	Full DVBS Process Mass Balance Conversion	This calculation was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-B-CA-003 Revision D Appendix A2	Dryer Energy, Steam and Chilled Water Demand Analysis	This calculation was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-B-CA-033 Revision A Appendix A2	DBVS Waste Dryer Enclosure Heating and Cooling Load Calculations	This calculation was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-B-CA-030 Revision C Appendix A2	DBVS Detectable Leak Volume for the Waste Dryer System	This calculation was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
B-145579-31-F-0008 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-008	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-31-F-0009 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-009	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-31-F-0508 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-508	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-31-F-0509 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-509	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-31-F-0608 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-608	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-31-F-0609 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 31-Y-609	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0003 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-F-003	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0004 Revision B (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-Y-004	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0008 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-W-008	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
B-145579-33-F-0010 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 32-Y-010	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0013 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-Y-013	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0018 Revision D (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-L-018	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0033 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-Y-033	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0137 Revision B (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 33-Y-037	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-33-F-0038 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 32-T-202	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
B-145579-32-F-0308 Revision C (Appendix C2)	Bulk Vitrification Instrumentation Loop Diagram 32-L-308	A preliminary review of this drawing was conducted. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. This drawing will need to be revised using Vendor-supplied instrument data during the detailed design.
DBVS-SK-M109 Revision A (Appendix C2)	Bulk Vitrification DCRS General Arrangement	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-B-0001 Revision G (Appendix C2)	Bulk Vitrification Structural Steel General Notes- Sheet 1	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-B-0002 Revision D (Appendix C2)	Bulk Vitrification Structural Steel General Notes- Sheet 2	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
F-145579-00-B-0003 Revision F (Appendix C2)	Bulk Vitrification Structural Steel Typical Details- Sheet 1	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-B-0004 Revision D (Appendix C2)	Bulk Vitrification Structural Steel Typical Details- Sheet 2	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-B-0008 Revision F (Appendix C2)	Bulk Vitrification Dryer Structural Steel plans & Details	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-B-0009 Revision F (Appendix C2)	Bulk Vitrification Dryer Structural Steel plans & Details	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-D-0011 Revision D (Appendix C2)	Bulk Vitrification Waste Receipt & Dryer Area G.A. Plan	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-D-0028 Revision D (Appendix C2)	Bulk Vitrification Area Waste Receipt & Dryer Area Sections- A,B,C, & D	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-D-0029 Revision C (Appendix C2)	Bulk Vitrification Area Waste Receipt & Dryer Area Section- Area Section E	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-D-0030 Revision C (Appendix C2)	Bulk Vitrification Area Waste Receipt & Dryer Area Section- Area Section F	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-D-0031 Revision B	Bulk Vitrification Area Waste Receipt & Dryer Area Section- Area Section G	This drawing was reviewed by the IQRPE and used to independently check structural calculations for the Dryer Support Structure. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
F-145579-00-P-0005 Revision C (Appendix C2)	Bulk Vitrification Dryer Piping Layout	This drawing was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-00-P-0001 Revision C (Appendix C2)	Bulk Vitrification Typical Pipe Support Details Sht 1 of 4	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0002 Revision C (Appendix C2)	Bulk Vitrification Typical Pipe Support Details Sht 2 of 4	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0003 Revision C (Appendix C2)	Bulk Vitrification Typical Pipe Support Details Sht 3 of 4	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0004 Revision C (Appendix C2)	Bulk Vitrification Typical Pipe Support Details Sht 4 of 4	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0005 Revision E (Appendix C2)	Bulk Vitrification Dryer Piping Layout	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0006 Revision D (Appendix C2)	Bulk Vitrification Dryer Effluent Piping Layout	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0007 Revision D (Appendix C2)	Bulk Vitrification Offgas Treatment Piping Layout	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0010 Revision D (Appendix C2)	Bulk Vitrification Dryer Piping Sections	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-P-0011 Revision D (Appendix C2)	Bulk Vitrification Dryer Effluent Piping Section	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
H-14-106789 Revision 1 (Appendix C2)	Bulk Vitrification Civil Site Improvements Plan	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
ECN 722466 Revision 0 (Appendix C2)	DBVS- Electrical Equipment Foundation- Plans & Sections	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing
H-14-106793 Revision 0 (Appendix C2)	Bulk Vitrification Waste Dryer Foundation Plan & Section	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System foundation was reviewed in DR-001.
H-14-106794 Revision 0 (Appendix C2)	Bulk Vitrification Receipt Area Foundations- Plans & Sections	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System foundation was reviewed in DR-001.
F-145579-00-A-0099 Revision G (Appendix D2)	Bulk Vitrification P&ID "Typicals" Legend	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-00-A-0100 Revision K (Appendix D2)	Bulk Vitrification P&ID Symbol Legend	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing..
F-145579-00-A-0102 Revision B (Appendix D2)	Bulk Vitrification Facility/Process Air Distribution P&ID Sht. 1	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-31-A-0100 Revision K (Appendix D2)	Bulk Vitrification Facility Clean Soil Handling System P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-31-A-0101 Revision E (Appendix D2)	Bulk Vitrification Glass Formers Handling System P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-32-A-0100 Revision 0B (Appendix D2)	Bulk Vitrification Waste Transfer Pump P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-33-A-0100 Revision L (Appendix D2)	Bulk Vitrification Waste Dryer P&ID	This drawing was reviewed in its entirety. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-33-A-0101 Revision M (Appendix D2)	Bulk Vitrification Waste Dryer Vacuum P&ID	This drawing was reviewed in its entirety. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.

Waste Dryer System Drawings		
Document Number	**Document Title**	**Comments**
F-145579-33-A-0104 Revision F (Appendix D2)	Bulk Vitrification Waste Dryer Chilled Water System P&ID	This drawing was reviewed in its entirety. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-33-A-0105 Revision F (Appendix D2)	Bulk Vitrification Waste Dryer Steam Supply System P&ID	This drawing was reviewed in its entirety. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
F-145579-33-A-0106 Revision C (Appendix D2)	Bulk Vitrification Waste Feed Dryer to Box P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-36-A-0099 Revision F (Appendix D2)	Bulk Vitrification Offgas Dust Removal P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.
F-145579-37-A-0101 Revision 0A (Appendix D2)	Bulk Vitrification Secondary Waste Storage P&ID	This drawing was used for information purposes only. The IQRPE certification for the Waste Dryer System does not address the specific content of this drawing.

Technical Specifications		
Document Number	**Document Title**	**Comments**
145643-D-SP-001 Revision 0 (Appendix G2)	Dryer and Condensate Recovery System	This specification was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-D-DS-039.1 Revision 1 (Appendix G2)	Technical Data Sheet: Air Cooled Screw Liquid Chiller Equipment No.- 33-D58-058	This specification was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-D-SP-005 Revision 1 (Appendix G2)	Dryer Chiller Pump Skid	This specification was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-D-SP-006 Revision 2 (Appendix G2)	Dryer and Condensate Recovery System Skid	This specification was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
145579-D-SP-007 Revision 0 (Appendix G2)	Steam Supply System	This specification was reviewed by the IQRPE. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.

Supporting Information		
Document Number	**Document Title**	**Comments**
Corrosion Review (Appendix H2)	Technical Specifications: A Corrosion Review: *Dryer and Condensate Recovery System* (143643-D-SP-001) and *Dryer and Condensate Recovery System Skid* (145579-D-SP-006)	An IQRPE Corrosion Specialist has performed an assessment of the corrosion resistance of the Waste Dryer System. The assessment included an independent design review with consideration to previous corrosion review comments and responses contained in Appendix H2. The IQRPE corrosion specialist has prepared a signed and stamped corrosion assessment per Attachment E to this report. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report.
Typical Leak Detector Data Sheet (Appendix not identified)	Sample: 33-LSH-018	This data sheet was reviewed in its entirety. Specific IQRPE review activities and any exceptions are described in Section 2.2 of this report. Because the data sheet is preliminary, it will require additional IQRPE review when final.
Process Flow Diagrams (Appendix E)	**MISSING FLOW DIAGRAMS**	**Appendix E Process Flow Diagrams are not contained in the DBVS Waste Dryer System Design Review Package. The flow diagrams are required for the IQRPE 100% final design certification.**

ATTACHMENT B

WASTE DRYER SYSTEM DESIGN DELIVERABLES TO BE REVIEWED WITH THE CONSTRUCTION CERTIFICATION PACKAGE

ATTACHMENT B

WASTE DRYER SYSTEM DESIGN DELIVERABLES TO BE REVIEWED WITH THE CONSTRUCTION CERTIFICATION PACKAGE

Submittal Number	Submittal Title
DRYER AND CONDENSATE RECOVERY SYSTEM	
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Outline drawing including weights and dimensions
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Mechanical shaft seal drawing and any proposed alternatives
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	List of pump materials of construction (with wetted parts noted)
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Test Plan
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Technical brochures on purchased components
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Dryer mass and energy balance calculation
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Equipment dimensional drawings
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Electrical wiring diagrams
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Control wiring diagrams
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Pipe support detail drawings
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Motor specifications and datasheet
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Bill of materials
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	System assembly instructions
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Gearbox maintenance
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Operation and maintenance manuals
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Welding procedures; procedure qualification and welder procedure qualification records
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	AWS CWI certificate
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Insulation system
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Protective coating specifications
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Recommended spare parts and frequency of replacement

Submittal Number	Submittal Title
143643-D-DS-001 Appendix A, Bidder's Drawing & Data Commitments	Final test results

AIR COOLED SCREW LIQUID CHILLER	
143643-D-DS-039.1 Appendix A, Bidder's Drawing & Data Commitments	Completed data sheets
143643-D-DS-039.1 Appendix A, Bidder's Drawing & Data Commitments	Outline drawings and layout drawings indicating weights and dimensions
143643-D-DS-039.1 Appendix A, Bidder's Drawing & Data Commitments	Technical brochures on purchased components
143643-D-DS-039.1 Appendix A, Bidder's Drawing & Data Commitments	Electrical schematics, wiring diagrams and nameplate information
143643-D-DS-039.1 Appendix A, Bidder's Drawing & Data Commitments	Set of installation and maintenance manuals c/w technical literature for all equipment and devices

DRYER CHILLER PUMP SKID	
145579-D-SP-005 Appendix A, Bidder's Drawing & Data Commitments	Completed data sheet
145579-D-SP-005 Appendix A, Bidder's Drawing & Data Commitments	100% Design and Fabrication Package including: Drawings Calculations Completed equipment data sheets Vendor cut sheets/technical brochures
145579-D-SP-005 Appendix A, Bidder's Drawing & Data Commitments	Test plan/Test procedure
145579-D-SP-005 Appendix A, Bidder's Drawing & Data Commitments	System assembly instructions
145579-D-SP-005 Appendix A, Bidder's Drawing & Data Commitments	Operation and maintenance manuals

DRYER AND CONDENSATE RECOVERY SYSTEM SKID	
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Completed data sheets
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Outline drawing including weights and dimensions
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	List of pump materials of construction (with wetted parts noted)
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Test plan
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Technical brochures on purchased components
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Equipment dimensional drawings
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Electrical wiring diagrams
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Control wiring diagrams
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Pipe support detail drawings

Submittal Number	Submittal Title
DRYER AND CONDENSATE RECOVERY SYSTEM SKID (cont.)	
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Pipe support detail calculations
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	ISO container modification structural calculation
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Motor specs and datasheet
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Bill of matierials
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	System assembly instructions
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Operation and maintenance manuals
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Welding procedures, procedure qualification records, and welder procedure qualification records
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	AWS CWI certificate
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Insulation system
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Protective coating specifications
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	FAT procedures
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Fabrication red line changes
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Final test results
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	Certified test material reports
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	CoC's and MTR's
145579-D-SP-006 Appendix A, Bidder's Drawing & Data Commitments	As built drawings

ATTACHMENT C

CODES, STANDARDS, AND REGULATIONS INCORPORATED INTO TECHNICAL SPECIFICATION PACKAGES

ATTACHMENT C

CODES, STANDARDS, AND REGULATIONS INCORPORATED INTO TECHNICAL SPECIFICATION PACKAGES

10 CFR 830	"Nuclear Safety Management," *Code of Federal Regulations*, as amended.
29 CFR 1910	"Occupational Safety and Health Standards," *Code of Federal Regulations,* as amended.
40 CFR 264	"Standards for Owners and Operators of Hazardous Waste Treatment, Storage, and Disposal Facilities," subpart J. *Code of Federal Regulations*, as amended.
47 CFR 15	"Radio Frequency Devices," *Code of Federal Regulations*, as amended.
DOE/RL-92-36	*Hanford Site Hoisting and Rigging Manual,* U.S. Department of Energy, Richland, Washington.
AATCC Test Method 27	*Water Resistance: Hydrostatic Pressure Test,* American Association of Textile Chemists and Colorists, Research Triangle Park, North Carolina.
AISC Allowable Stress Design	*Manual of Steel Construction – Allowable Stress Design*, Ninth Edition, American Institute of Steel Construction, Chicago, Illinois.
AISC Load and Resistance Factor Design	*Manual of Steel Construction – Load and Resistance Factor Design.* Third Edition, American Institute of Steel Construction, Chicago, Illinois.
ANSI/ASME B1.20.1	*Pipe Threads, General Purpose (Inch).* American National Standards Institute, New York, New York.
ANSI/AWWA D100	*AWWA Standard for Welded Steel Tanks for Water Storage,* American Water Works Association, Denver, Colorado.
ANSI C63.16	*American National Standard Guide for Electrostatic Discharge Test Methodologies and Criteria for Electronic Equipment,* American National Standards Institute, Washington, D.C.

ANSI FCI 70-2	*Control Valve Seat Leakage,* Fluid Controls Institute, Inc., Cleveland, Ohio.
ANSI/HI 3.1-3.5	*American National Standard for Rotary Pumps for Nomenclature, Definitions, Applications and Operation,* Hydraulic Institute, Parsippany, New Jersey.
ANSI/HI 3.6	*American National Standard for Rotary Pump Tests*, Hydraulic Institute, Parsippany, New Jersey.
ANSI/IESNA RP-7	*Lighting Industrial Facilities*, Illuminating Engineering Society of North America, New York, New York.
ANSI Y14.1	*Drawing Sheet Size and Format*, American National Standards Institute, Inc. New York, New York.
ANSI Y14.5M	*Dimensioning and Tolerancing,* American National Standards Institute, New York, New York.
API 620	*Design and Construction of Large, Welded, Low-Pressure Storage Tank, Tenth Edition*, American Petroleum Institute, Washington, D.C.
ASCE 4-98	*Seismic Analysis of Safety-Related Nuclear Structures*, American Society of Civil Engineers, Reston, Virginia.
ASCE 7-98	*Minimum Design Loads for Buildings and Other Structures,* American Society of Civil Engineers, Reston, Virginia.
ASHRAE Fundamentals Handbook	*2001 ASHRAE Handbook – Fundamentals,* American Society of Heating, Refrigerating, and Air Conditioning Engineers, Atlanta, Georgia.
ASME B&PV Code Sections VIII and IX	*ASME Boiler and Pressure Vessel Code,* American Society of Mechanical Engineers, New York, New York.
ASME B16.5	*Pipe Flanges and Flanged Fittings,* American Society of Mechanical Engineers, New York, New York.
ASME B16.9	*Factory-Made Wrought Steel Buttwelding Fittings,* American Society of Mechanical Engineers, New York, New York.

ASME B16.11	*Forged Fittings, Socket Welding and Threaded,* American Society of Mechanical Engineers, New York, New York.
ASME B18.2.1	*Square and Hex Bolts and Screws Inch Series,* American Society of Mechanical Engineers, New York, New York.
ASME B18.2.2	*Square and Hex Nuts,* American Society of Mechanical Engineers, New York, New York.
ASME B31.3	*Process Piping,* American Society of Mechanical Engineers, New York, New York.
ASME NQA-1, 1994	*Quality Assurance Program Requirements for Nuclear Facilities,* American Society of Mechanical Engineers, New York, New York.
ASME PCC-1	*Guidelines for Pressure Boundary Bolted Flange Joint Assembly,* American Society of Mechanical Engineers, New York, New York.
ASNT SNT-TC-1A	*Recommended Practice,* American Society of Nondestructive Testing, Columbus, Ohio.
ASTM A36/A36M	*Standard Specification for Carbon Structural Steel, American Society of Testing and Materials,* New York, New York.
ASTM A53/A53M	*Standard Specification for Pipe, Steel, Black and Hot-Dipped, Zinc-Coated, Welded and Seamless,* American Society of Testing and Materials, New York, New York.
ASTM A105/A105M	*Standard Specification for Carbon Steel Forgings for Piping Applications,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A106	*Standard Specification for Seamless Carbon Steel Pipe for High-Temperature Service,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A108	*Standard Specification for Steel Bars, Carbon, Cold-Finished, Standard Quality,* American Society for Testing and Materials, West Conshohocken, Pennsylvania

ASTM A182/A182M	*Standard Specification for Forged or Rolled Alloy Steel Pipe Flanges, Forged Fittings, and Valves and Parts for High Temperature Service*, American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A193/A193M	*Standard Specification for Alloy-Steel and Stainless Steel Bolting Materials for High-Temperature Service,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A194/A194M	*Standard Specification for Carbon and Alloy Steel Nuts for Bolts for High Pressure and High Temperature Service or Both,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A234/A234M	*Standard Specification for Piping Fittings of Wrought Carbon Steel and Alloy for Moderate and High Temperature Service,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A240/A240M	*Standard Specification for Chromium and Chromium-Nickel Stainless Steel Plate, Sheet, and Strip for Pressure Vessels and for General Applications,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A269	*Standard Specification for Seamless and Welded Austenitic Stainless Steel Tubing for General Service,* American Society of Testing and Materials, New York, New York.
ASTM A276	*Standard Specification for Stainless Steel Bars and Shapes,* American Society of Testing and Materials, New York, New York.
ASTM A307	*Standard Specification for Carbon Steel Bolts and Studs, 60,000 PSI Tensile Strength*, American Society for Testing and Materials, West Conshohocken, Pennsylvania.
ASTM A312/A312M	*Standard Specification for Seamless and Welded Austenitic Stainless Steel Pipes*, American Society for Testing and Materials, West Conshohocken, Pennsylvania

ASTM A325	*Standard Specification for Structural Bolts, Steel, Heat Treated, 120/105 ksi Minimum Tensile Strength,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A354	*Standard Specification for Quenched and Tempered Alloy Steel Bolts, Studs, and other Externally Threaded Fasteners,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A403/A403M	*Standard Specification for Wrought Austenitic Stainless Steel Piping Fittings*, American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A480/A480M	*Standard Specification for General Requirements for Flat-Rolled Stainless and Heat-Resisting Steel Plate, Sheet, and Strip,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A500	*Standard Specification for Cold-Formed Welded and Seamless Carbon Steel Structural Tubing in Rounds and Shapes,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A563a	*Standard Specification for Carbon and Alloy Steel Nuts,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM A569	*Standard Specification for Steel, Carbon (0.15 Maximum, Percent) Hot-Rolled Sheet and Strip Commercial,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM C518	*Standard Test Method for Steady-State Thermal Transmission Properties by Means of the Heat Flow Meter Apparatus,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM D380	*Standard Test Methods for Rubber Hose*, American Society for Testing and Materials, West Conshohocken, Pennsylvania.
ASTM D991	*Standard Test Method for Rubber Property-Volume Resistivity of Electrically Conductive and Antistatic Products,* American Society for Testing and Materials, West Conshohocken, Pennsylvania.

ASTM D1621	*Standard Test Method for Compressive Properties of Rigid Cellular Plastics,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM D1622	*Standard Test Method for Apparent Density of Rigid Cellular Plastics,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM D5162	*Standard Practice for Discountability (Holiday) Testing of Nonconductive Protective Coating on Metallic Substrates,* American Society for Testing and Materials, West Conshohocken, Pennsylvania.
ASTM E84	*Standard Test Method for Surface Burning Characteristics of Building Materials,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM E96	*Standard Test Methods for Water Vapor Transmission of Materials,* American Society for Testing and Materials, West Conshohocken, Pennsylvania
ASTM E285	*Standard Test Method for Oxyacetylene Ablation Testing of Thermal Insulation Materials,* American Society for Testing and Materials, West Conshohocken, Pennsylvania.
AWS D1.1/D1.1M	*Structural Welding Code* – Steel, American Welding Society, Miami, Florida
AWS D1.6	*Structural Welding Code* – Stainless Steel, American Welding Society, Miami, Florida.
AWS QC-1	*Standard for AWS Certification of Welding Inspectors*, American Welding Society, Miami, Florida.
HNF-2962	*A List of EMI/EMC Requirements,* Rev. O, Numatec Hanford Corporation for Fluor Daniel Hanford, Inc. Richland, Washington.
HNF-SD-GN-ER-501	*Natural Phenomena Hazards*, Hanford Site, Washington, Revision 1B, Westinghouse Hanford Company, Richland, Washington.

IEC 61000-4-2	*Electromagnetic Compatibility (EMC) – Part 4-2: Testing and Measurement Techniques – Electrostatic Discharge Immunity Test,* International Engineering Consortium, Chicago, Illinois.
IEEE C62.41.1	*IEEE Guide on the Surge Environment in Low-Voltage (1000 V and Less) AC Power Circuits,* Institute of Electrical and Electronics Engineers, New York, New York.
IEEE C62.41.2	*IEEE Recommended Practice on Characterization of Surges in Low Voltage (1000 V and Less) AC Power Circuits,* Institute of Electrical and Electronics Engineers, New York, New York
IEEE C37.90.2	*IEEE Standard for Withstand Capability of Relay Systems to Radiated Electromagnetic Interference from Transceivers,* Institute of Electrical and Electronics Engineers, New York, New York.
IEEE 141	*IEEE Recommended Practice for Electric Power Distribution for Industrial Plants,* Institute of Electrical and Electronics Engineers, New York, New York.
IEEE 142	*IEEE Recommended Practice for Grounding of Industrial and Commercial Power Systems,* Institute of Electrical and Electronics Engineers, New York, New York.
IEEE 242	*IEEE Recommended Practice for Protection and Coordination of Industrial and Commercial Power Systems,* Institute of Electrical and Electronics Engineers, New York, New York.
IEEE 519	*Recommended Practices and Requirements for Harmonic Control in Electrical Power Systems,* Institute of Electrical and Electronics Engineers, New York, New York.
IESNA HB-9	*IESNA Lighting Handbook,* 9th Edition, Illuminating Engineering Society of North America, New York, New York.
IP-2	The 2003 Hose Handbook, 7th Edition, Rubber Manufacturers of America, Washington, D.C.

ISO 668	*Series 1 Freight Containers Classification, Dimensions and Ratings,* International Organization for Standardization, Geneva, Switzerland.
ISO 1161	*Series 1 Freight Containers – Corner Fittings – Specification,* International Organization for Standardization, Geneva, Switzerland.
ISO 1496-2	*Series 1 Freight Containers – Specification and Testing – Part 2: Thermal Containers,* International Organization for Standardization, Geneva, Switzerland.
MSS SP-72	*Ball Valves with Flanged or Butt-Welding Ends for General Service,* Manufacturing Standardization Society of the Valve and Fittings Industry, Inc. Vienna, Virginia.
MSS SP-82	*Valve Pressure Testing Methods,* Manufacturing Standardization Society of the Valve and Fittings Industry, Inc. Vienna, Virginia.
NEMA MG-1	*Motors and Generators*, National Electrical Manufacturers Association, Rosslyn, Virginia.
NFPA 70	*National Electrical Code,* 2002 Edition, National Fire Protection Association, Quincy, Massachusetts.
SAE J429	*Mechanical and Material Requirements for Externally Threaded Fasteners,* Society of Automotive Engineers, Warrendale, Pennsylvania.
UBC, 1997	*1997 Uniform Building Code*, International Conference of Building Officials, Whittier, California.
UL-Listed	*Electrical Appliance and Utilization Equipment Directory*, Underwriters Laboratories, Inc., Northbrook, Illinois.
UL 142	*Standard for Safety-Steel Aboveground Tanks for Flammable and Combustible Liquids*, Underwriters Laboratories, Inc., Northbrook, Illinois.
UL 508A	*Standard for Industrial Control Panels,* Underwriters Laboratories, Inc., Northbrook, Illinois.

ATTACHMENT D

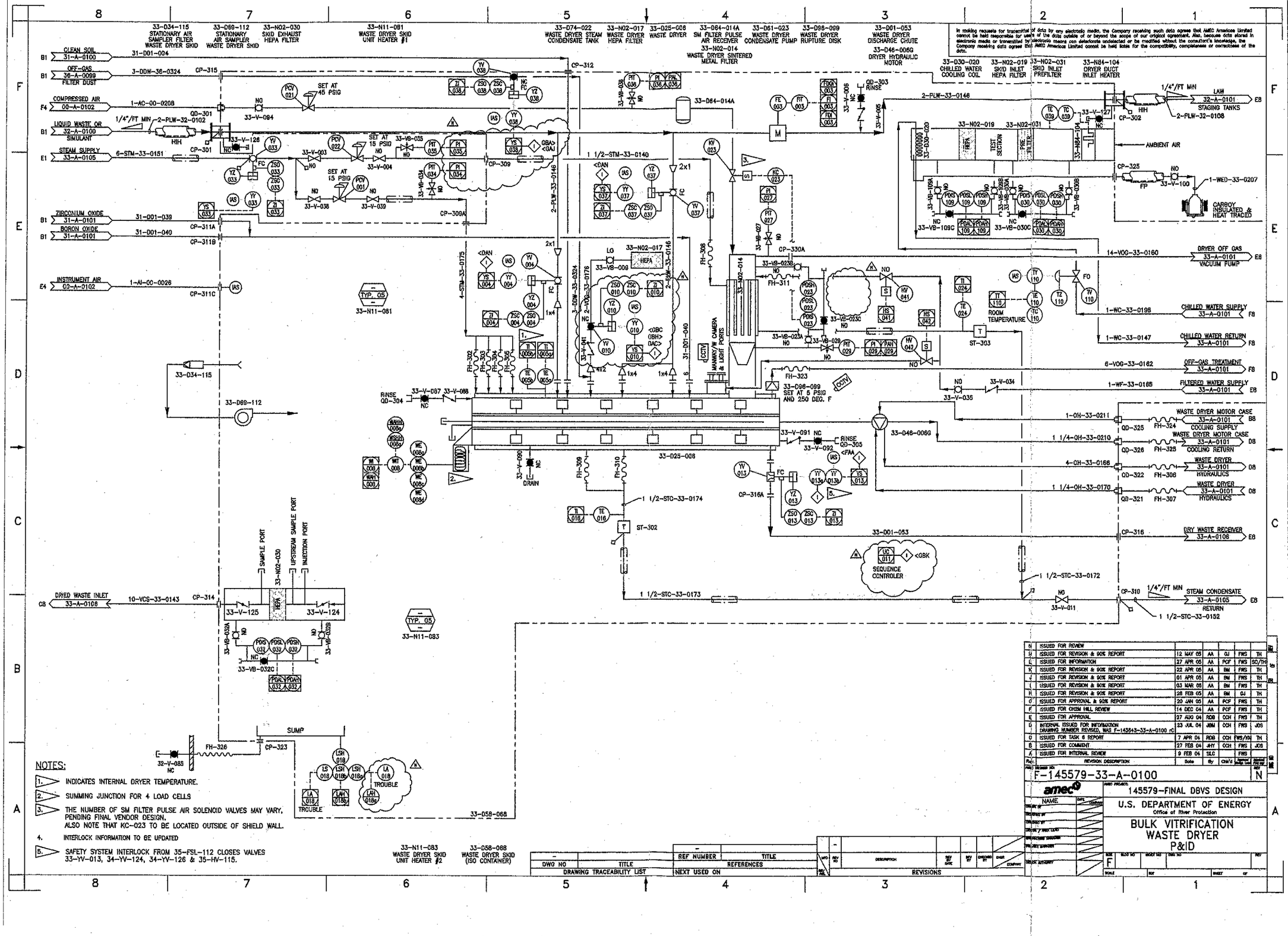
WASTE DRYER SYSTEM
PIPING AND INSTRUMENTATION DIAGRAMS

1. **Drawing F-145579-33-A-0100, Rev N, "Bulk Vitrification Waste Dryer P&ID"**

2. **Drawing F-145579-33-A-0101, Rev M, "Bulk Vitrification Waste Dryer Vacuum P&ID"**

APPENDIX E

Corrosion Engineering Review



NOTES:

1. INDICATES INTERNAL DRYER TEMPERATURE.
2. SUMMING JUNCTION FOR 4 LOAD CELLS
3. THE NUMBER OF SM FILTER PULSE AIR SOLENOID VALVES MAY VARY, PENDING FINAL VENDOR DESIGN. ALSO NOTE THAT KC-023 TO BE LOCATED OUTSIDE OF SHIELD WALL.
4. INTERLOCK INFORMATION TO BE UPDATED
5. SAFETY SYSTEM INTERLOCK FROM 35-FSL-112 CLOSES VALVES 33-YV-013, 34-YV-124, 34-YV-126 & 35-HV-115.

33-N11-083 WASTE DRYER SKID UNIT HEATER #2

33-058-068 WASTE DRYER SKID (ISO CONTAINER)

DRAWING TRACEABILITY LIST

DWG NO	TITLE

REFERENCES

REF NUMBER	TITLE

NEXT USED ON

REVISIONS								
NO	REV BY	DESCRIPTION	REV DATE	CHECKED BY	ENGR	COMPANY		

REV	REVISION DESCRIPTION	Date	By	Chk'd	Approved	Date	MGR
N	ISSUED FOR REVIEW						
M	ISSUED FOR REVISION & 90% REPORT	12 MAY 05	AA	GJ	FWS	TH	
L	ISSUED FOR INFORMATION	27 APR 05	AA	PCF	FWS	SO/TH	
K	ISSUED FOR REVISION & 90% REPORT	22 APR 05	AA	BM	FWS	TH	
J	ISSUED FOR REVISION & 90% REPORT	01 APR 05	AA	BM	FWS	TH	
I	ISSUED FOR REVISION & 90% REPORT	03 MAR 05	AA	BM	FWS	TH	
H	ISSUED FOR REVISION & 90% REPORT	28 FEB 05	AA	BM	GJ	TH	
G	ISSUED FOR APPROVAL & 90% REPORT	20 JAN 05	AA	PCF	FWS	TH	
F	ISSUED FOR CH2M HILL REVIEW	14 DEC 04	AA	PCF	FWS	TH	
E	ISSUED FOR APPROVAL	27 AUG 04	RDB	CCH	FWS	TH	
D	INTERNAL ISSUED FOR INFORMATION DRAWING NUMBER REVISED, WAS F-143643-33-A-0100 r2	23 JUL 04	JBM	CCH	FWS	JDS	
C	ISSUED FOR TASK 6 REPORT	7 APR 04	RDB	CCH	FWS/KM	TH	
B	ISSUED FOR COMMENT	27 FEB 04	JHT	CCH	FWS	JDS	
A	ISSUED FOR INTERNAL REVIEW	9 FEB 04	SLC		FWS		

F-145579-33-A-0100 N

amec

145579-FINAL DBVS DESIGN

U.S. DEPARTMENT OF ENERGY
Office of River Protection

BULK VITRIFICATION
WASTE DRYER
P&ID

F

33-D61-078 WASTE DRYER HYDRAULIC PUMP No.1

33-074-077 WASTE DRYER HYDRAULIC OIL TANK

33-D61-079 WASTE DRYER HYDRAULIC PUMP No.2

33-D61-080 WASTE DRYER HYDRAULIC PUMP No.3

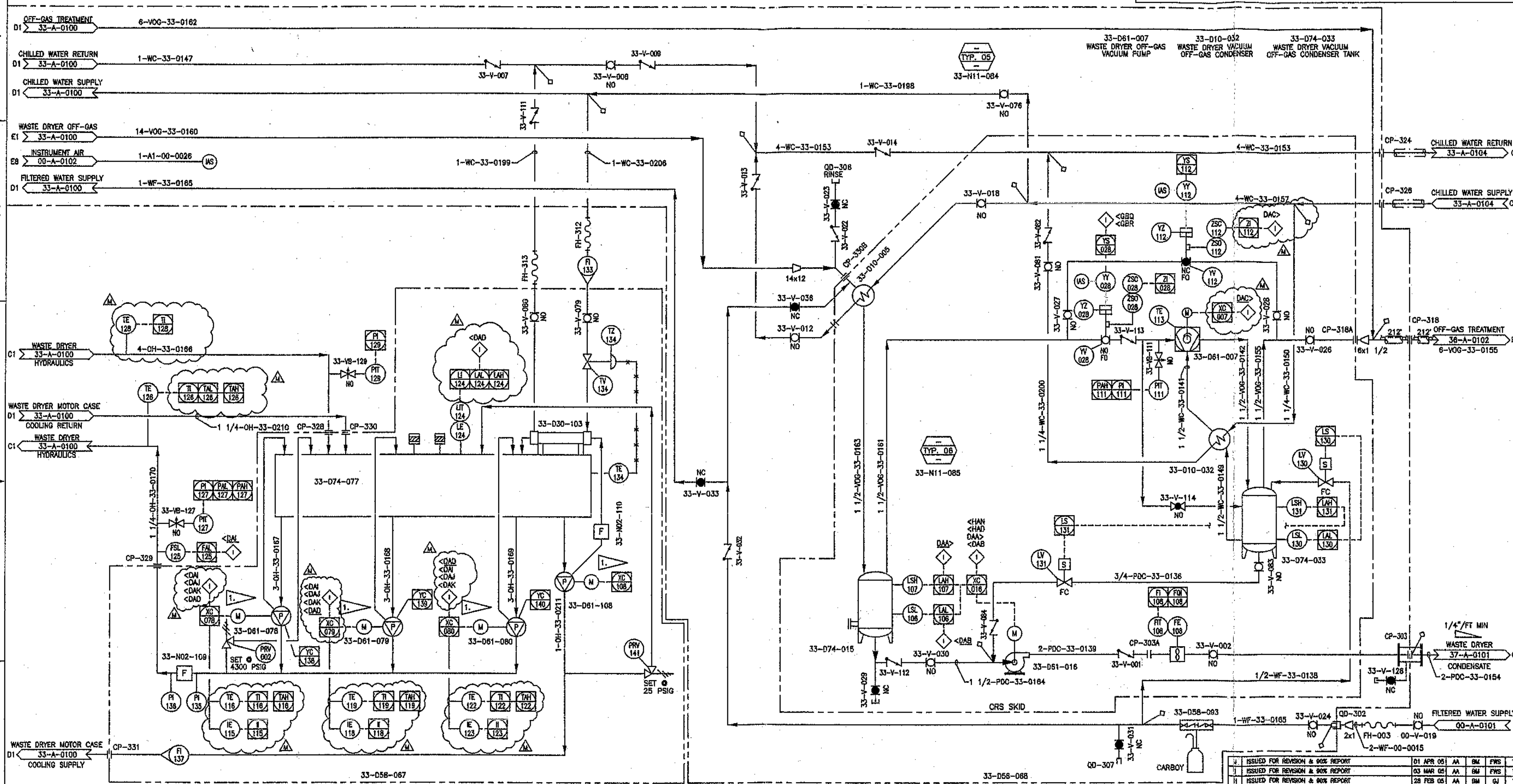
33-D30-103 WASTE DRYER HYDRAULIC OIL TANK CHILLED WATER HEAT EXCHANGER

33-074-015 WASTE DRYER OFF-GAS CONDENSATE TANK

33-D10-005 WASTE DRYER OFF-GAS CONDENSER

33-N11-084 WASTE DRYER UNIT HEATER #3

33-D61-016 WASTE DRYER OFF-GAS CONDENSATE PUMP



33-N02-109 HYDRAULIC OIL FILTER #1

33-D58-067 WASTE DRYER HYDRAULIC SKID (ISO CONTAINER)

33-D61-108 WASTE DRYER HYDRAULIC RECIRCULATION PUMP

33-N02-110 HYDRAULIC OIL FILTER #2

33-N11-085 WASTE DRYER AC UNIT #2

33-D58-068 WASTE DRYER SKID (ISO CONTAINER)

33-D58-093 WASTE DRYER SKID BACKFLOW PREVENTER

Rev.	REVISION DESCRIPTION	Date	By	Chk'd	Approved Design Lead	Approved Proj Mgr
M	ISSUED FOR REVIEW					
L	ISSUED FOR INFORMATION	27 APR 05	AA	PCF	FWS	SC/TH
K	ISSUED FOR REVISION & 90% REPORT	22 APR 05	AA	BM	FWS	TH
J	ISSUED FOR REVISION & 90% REPORT	01 APR 05	AA	BM	FWS	TH
I	ISSUED FOR REVISION & 90% REPORT	03 MAR 05	AA	BM	FWS	TH
H	ISSUED FOR REVISION & 90% REPORT	28 FEB 05	AA	BM	GJ	TH
G	ISSUED FOR CH2M HILL APPROVAL	28 JAN 05	AA	BM	FWS	TH
F	ISSUED FOR CH2M HILL REVIEW	14 DEC 04	AA	PCF	FWS	TH
E	ISSUED FOR APPROVAL	27 AUG 04	ROB	CCH	FWS	TH
D	INTERNAL ISSUED FOR INFORMATION DRAWING NUMBER REVISED, WAS F-143643-33-A-0101 rC	23 JUL 04	JBM	CCH	FWS	JDS
C	ISSUED FOR TASK 6 REPORT	7 APR 04	ROB	CCH	FWS/KN	TH
B	ISSUED FOR COMMENT	27 FEB 04	JHY	CCH	FWS	JDS
A	ISSUED FOR INTERNAL REVIEW	9 FEB 04	SLC		FWS	

AMEC DRAWING NO. F-145579-33-A-0101 REV M

amec

AMEC PROJECT: 145579-FINAL DBVS DESIGN

U.S. DEPARTMENT OF ENERGY
Office of River Protection

BULK VITRIFICATION
WASTE DRYER VACUUM
P&ID

NOTES:

1. HYDRAULIC PUMPS ARE CONTROLLED THROUGH A WASH PLATE SOLENOID AS PART OF THE PUMP W/A CONTROL SIGNAL FROM THE MCS
2. INTERLOCK INFORMATION TO BE UPDATED

DWG NO	TITLE
DRAWING TRACEABILITY LIST	

REF NUMBER	TITLE
REFERENCES	
NEXT USED ON	

REVISIONS

APR 1 1 2005

March 9, 2005

Northwest Corrosion Engineering

10995 Warfield Road, Sedro-Woolley, WA 98284
Phone: (360) 826-4570 Fax: (360) 826-6321

Mr. Karl Walterskirchen
TechnoGeneral Services Company
710 North 4th Avenue
Pasco, WA 99301

SUBJECT: Corrosion Engineering Review – DBVS Waste Dryer System Review, Package 2.2 Revision B February 8, 2005

Mr. Walterskirchen,

Documents pertaining to the Demonstration Bulk Vitrification System - Waste Dryer System, Package 2.2 Revision B February 8, 2005 were reviewed from a corrosion engineering perspective. Comments pertaining to the review are outline below.

1.0 Corrosion Review – Submitted by ChemMet LTD, Co., dated January 28, 2005.

1.1 Dryer and Condensate Recovery System (143643-D-SP-001)

Northwest Corrosion Engineering does not take any exceptions to the comments provided by Dr. Divine in his review of the Dryer and Condensate Recovery System (143643-D-SP-001).

1.2 Dryer and Condensate Recovery System Skid (145579-D-SP-006)

Northwest Corrosion Engineering does not take any exceptions to the comments provided by Dr. Divine in his review of the Dryer and Condensate Recovery System Skid (145579-D-SP-006).

1.3 Other Comments & Recommendations

Northwest Corrosion Engineering does not take any exceptions to the comments provided by Dr. Divine in the Other Comments & Recommendations of the ChemMet LTD corrosion review.

2.0 The following additional comments concerning Technical Specifications 143643 D-SP-001 and 145579-D-SP-006 are being provided by Northwest Corrosion Engineering.

2.1 143643-D-SP-001 Rev. 0 – Dryer and Condensate Recovery System

a. Section 3.3.6 Protective Coatings requires that "Protective coating specifications shall be submitted to the Buyer for review and approval before fabrication". A specific Amercoat Primer is not called out in section 3.3.6.2. Reliance has been placed upon the Seller to comply with manufacturer's

recommendations for materials, surface preparation, application procedures, environmental controls, etc. As protective coatings are used as the first line of defense against corrosion, it would be prudent to provide the Seller with coating specifications specific to the items to be coated. This will require the Seller to recognize and prepare for a specific set of coating instructions.

b. Provisions should be made to perform 3rd party coating inspection at the application location.

c. Section 4.3 Inspections and Tests paragraph 2 requires that water used for testing shall be tested for chlorides and rejected if chloride concentration is greater than 250 ppm for water temperature less than 149°F. To reduce the possibility of stress corrosion cracking, water used for hydrostatic testing of austenitic stainless steels should contain less than 200 ppm chlorides. After hydrostatic testing is complete, the materials should be immediately flushed with fresh water and dried by circulating air or wiping.

2.2 145579-D-SP-006 Rev. 2 – Dryer and Condensate Recovery System Skid

a. Section 3.3.6 Protective Coatings does not specify the coating products to use, application methods, environmental controls, or inspection criteria. At a minimum, all coating related work (including products, environmental constraints, surface preparation, coating application methods, and inspection criteria) should be reviewed and approved prior to application. Ideally, the Seller would be provided with a complete and thorough set of coating specifications that outline all coating related requirements.

b. Provisions should be made to perform 3rd party coating inspection at the application location.

c. Section 4.2 Inspections and Tests paragraph 2 requires that water used for testing shall be tested for chlorides and rejected if chloride concentration is greater than 250 ppm for water temperature less than 149°F. To reduce the possibility of stress corrosion cracking, water used for hydrostatic testing of austenitic stainless steels should contain less than 200 ppm chlorides. After hydrostatic testing is complete, the materials should be immediately flushed with fresh water and dried by circulating air or wiping.

d. Section 5.2 Preservation and Packaging requires that defects in the paint shall be touched up or repaired. Again, reliance is placed upon the Seller to complete this task without specific instruction on how to do so and any subsequent testing of touch ups or repairs. Stand-alone coating specifications would address these issues in a specific manner.

e. Drawing 056-001-2-010 Engineering Data Item 3 states the "Non stainless exterior is painted Amercoat 220 (color T.B.D.) 5 mil thickness." Information is not provided as to the required primer coat materials.

3.0 General Notes:

a. During bench scale testing, it will be imperative to collect corrosion measurements. The use of corrosion coupons and ultra-sonic thickness testing will yield valuable information as to the corrosive nature of the process fluid in contact with the proposed containment materials.

b. The final design should provide for the installation of corrosion coupons installed directly into the waste product stream. This will provide information as to the corrosion resistance of various alloy materials to the waste fluid.

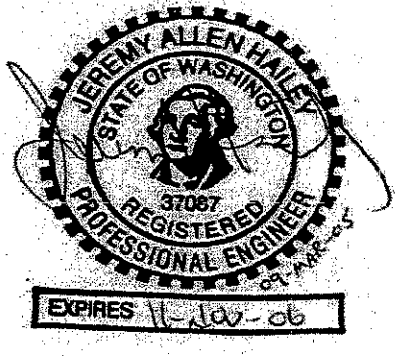
c. Preliminary research was completed to determine if standard industry recommended practices exist to guide hydrostatic pressure testing materials and procedures. Both ASTM and ASME standards provide guidelines as to test pressures and hold times, but specific information was not found that describes chloride concentration limits in the test media. Due to concerns related to stress corrosion cracking, both NORSOK Standards and the Nickel Development Institute recommend that hydrostatic testing and flushing of stainless steel piping be completed with test media containing less than 200 ppm chlorides.

d. Project specific coating specifications should be developed and issued with the design package. This will ensure that the protective coatings will be compatible with the materials and environments to which they are exposed. In addition, provisions should be made for 3rd party coating inspection to be completed. The inspection would take place at specific hold points as described in the coating specification.

The comments provided in this review are based upon the specific technical specifications as described at the 90% level of design.

Sincerely,
Northwest Corrosion Engineering

Jeremy A. Hailey, P.E.
NACE Corrosion Specialist, No. 5401



4.0 REFERENCES:

1. ASTM A 999/A 999M, *Standard Specification for General Requirements for Alloy and Stainless Steel Pipe*, American Society of Testing and Materials, West Conshohocken, Pennsylvania.
2. ASME B31.3, *Process Piping*, American Society of Mechanical Engineers, New York, New York.
3. Nickel Development Institute, *Design, Water Factors Affect Service-Water Piping Materials*, NiDI Technical Series No. 10043, Toronto, Ontario
4. NORSOK Standard L-CR-004, *Common Requirements – Piping Fabrication, Installation, Flushing, and Testing*, Norway

Attachment 4
05-ED-085

U.S. Department of Energy, Office of River Protection/
CH2M HILL Hanford Group, Inc. Certification Statement

The following certification is required by WAC 173-303-810(13) for all applications and reports submitted to Ecology.

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Roy J. Schepens 10/27/05

Owner/Operator — Date

Roy J. Schepens, Manager
U.S. Department of Energy
Office of River Protection

Edward D. Aromi Jr. 10/17/05

Co-operator — Date

Edward S. Aromi, Jr.
President and General Manager
CH2M HILL Hanford Group, Inc.