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ENGINEERING CHANGE NOTICE

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1. ECN 653812

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Proj. ECN

2. ECN Category (mark one) Supplemental <input type="checkbox"/> Direct Revision <input checked="" type="checkbox"/> Change ECN <input type="checkbox"/> Temporary <input type="checkbox"/> Standby <input type="checkbox"/> Supersedure <input type="checkbox"/> Cancel/Void <input type="checkbox"/>	3. Originator's Name, Organization, MSIN, and Telephone No. Leela M. Sasaki, Data Assessment and Interpretation, R2-12, 373-1027	4. USQ Required? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	5. Date 05/26/99	
	6. Project Title/No./Work Order No. Tank 241-C-101	7. Bldg./Sys./Fac. No. 241-C-101	8. Approval Designator N/A	
	9. Document Numbers Changed by this ECN (includes sheet no. and rev.) WHC-SD-WM-ER-473, Rev. 0-D	10. Related ECN No(s). ECNs: 625678, 625698, 612285, 649443	11. Related PO No. N/A	

12a. Modification Work <input type="checkbox"/> Yes (fill out Blk. 12b) <input checked="" type="checkbox"/> No (NA Blks. 12b, 12c, 12d)	12b. Work Package No. N/A	12c. Modification Work Complete N/A Design Authority/Cog. Engineer Signature & Date	12d. Restored to Original Condition (Temp. or Standby ECN only) N/A Design Authority/Cog. Engineer Signature & Date
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13a. Description of Change
 This ECN has been generated in order to update the document to reflect results of recent data/information evaluation.

13b. Design Baseline Document? Yes No

Replace pages:
 ES-5, ES-6, 5-5, 5-6, 6-1, 6-2, 7-1, and 7-2

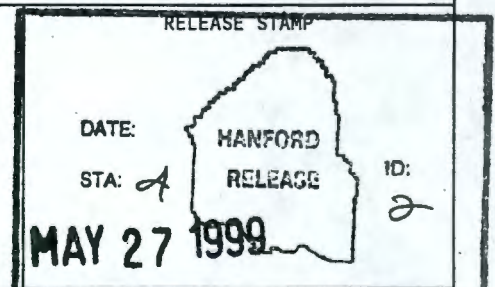
14a. Justification (mark one)

Criteria Change <input checked="" type="checkbox"/>	Design Improvement <input type="checkbox"/>	Environmental <input type="checkbox"/>	Facility Deactivation <input type="checkbox"/>
As-Found <input type="checkbox"/>	Facilitate Const <input type="checkbox"/>	Const. Error/Omission <input type="checkbox"/>	Design Error/Omission <input type="checkbox"/>

14b. Justification Details

A tank characterization report page change revision is required to reflect the results of recent evaluation of data/information pertaining to adequacy of tank sampling for safety screening purposes (Reynolds et al. 1999, Evaluation of Tank Data for Safety Screening, HNF-4217, Rev. 0, Lockheed Martin Hanford Corporation, Richland, Washington).

15. Distribution (include name, MSIN, and no. of copies)
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Tank Characterization Report for Single-Shell Tank 241-C-101

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U.S. Department of Energy Contract 8023764-9-K001


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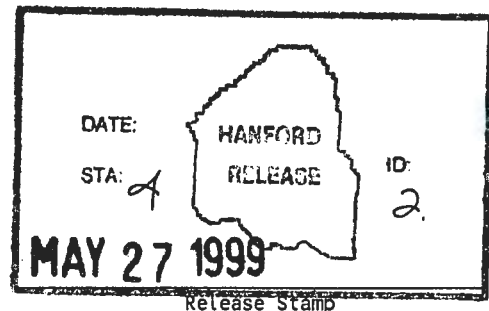
Key Words: Waste Characterization, Single-Shell Tank, SST, Tank 241-C-101, Tank C-101, C-101, C Farm, Tank Characterization Report, TCR, Waste Inventory, TPA Milestone M-44

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This report also summarizes two sampling events, an auger sample obtained in March 1995 and vapor samples obtained in September 1994. Total alpha activity, percent water, energetic properties, and vapor flammability were measured in accordance with WHC-SD-WM-SP-004, *Tank Safety Screening Data Quality Objective* (Babad and Redus 1994). In addition, Characterization Plant Engineering and Characterization Process Control requested that measurements of pH, total organic carbon, total inorganic carbon, and bulk density be performed on the auger samples.

Tank 241-C-101 was sufficiently sampled to meet the requirements of the safety screening data quality objective. The waste subsamples, as measured by differential scanning calorimetry, exhibited no exothermic reactions. The percent water ranged from 15.4 to 33.9 percent for the solids phase of the waste. Values less than 17 percent are below the minimum required by the Tank Safety Screening Data Quality Objective. Proper notifications concerning the low percent water results were made on May 3, 1995 (Sasaki 1995). The total alpha activity ranged from 0.955 to 1.18 $\mu\text{Ci/g}$, well below the maximum limit of 34.4 $\mu\text{Ci/g}$. The maximum total organic carbon value from the drainable liquid phase of the auger sample was 3,990 $\mu\text{g C/g}$, well below the limit of 30,000 $\mu\text{g C/g}$ specified in WHC-SD-WM-DQO-006, *Data Quality Objective to Support Resolution of the Organic Fuel Rich Tank Safety Issue* (Babad et al. 1994). The maximum weekly temperature readings in the tank since 1974 fluctuate between 13 °C (55 °F) and 44 °C (111 °F). The temperature readings indicate that the heat load in the tank is not excessive and is adequately dissipated. Vapor space analyses indicated flammable components at a concentration of 1.71 percent of the lower flammability limit, well below the notification

limit of 25 percent of the lower flammability limit. Details of the vapor sampling and analysis and its interpretation are included in a separate report.

5.4 COMPARISON OF ANALYTICAL AND HISTORICAL DATA

Because of the limited analytical requirements stipulated by the safety screening characterization (Babad and Redus 1994), few comparisons are possible between the analytical results from the 1995 sampling event and the historical transfers and estimated inventories. There are no TOC, pH or DSC data listed in the Historical Tank Content Estimate (Brevick et al. 1994); however, historical estimates for bulk density and percent water are available (see Table 2-5). Total alpha activity can also be estimated from the historical plutonium activity in Table 2-5. Table 5-2 compares the historical and analytical data for bulk density, water content, and total alpha. The analytical weight percent water value in Table 5-2 corresponds to the weight-weighted average of the results reported in Table 4-4 (transition 1) for the crust, upper half solids, and lower half solids, and drainable liquid samples. There was no Historical Tank Content Estimate (Brevick et al. 1994) available for the supernatant TIC, but the analytical result of 3,990 $\mu\text{g C/ml}$ can be compared with the uranium recovery waste supernatant prediction of 10,500 $\mu\text{g C/ml}$ in WHC-SD-WM-TI-629, *Hanford Defined Wastes: Chemical and Radionuclide Compositions* (Agnew 1995).

Table 5-2. Comparison of the Solids Analytical Results and Historical Tank Content Estimate Estimates.*

Analyte	Analytical result	HTCE result
Bulk density (g/ml)	1.79	1.45
Percent water (by weight)	33.8	61.1
Total alpha ($\mu\text{Ci/g}$)	1.09	0.512 (Pu only)

Note: 1 Ci = 3.7 E+10 Bq.

*C. H. Brevick, L. A. Gaddis, and W. W. Pickett, 1994, *Historical Tank Content Estimate for the Northeast Quadrant of the Hanford 200 East Areas*, WHC-SD-WM-ER-349, Rev. 0, ICF Kaiser Hanford Company, Richland, Washington.

5.5 EVALUATION OF PROGRAM REQUIREMENTS

This section details the data needs as defined in the Tank Safety Screening DQO (Babad and Redus 1994) and investigates whether tank 241-C-101 has been appropriately categorized concerning safety issues. The DQO establishes decision criteria or notification limits for concentrations of analytes of concern. If results from one of the primary analyses exceed any of the decision criteria, the tank is not classified as "safe" and further analyses are conducted to ensure the safety of the tank (Babad and Redus 1994). There are insufficient data available to assess impacts on operational, environmental, or process development programs.

5.5.1 Safety Evaluation

The primary analytical requirements identified in the Tank Safety Screening DQO (Babad and Redus 1994) are energetics, total alpha activity, moisture content, and flammable gas concentration. TOC was analyzed on the drainable liquid sample for tank 241-C-101 at the request of Characterization Process Control. The 1995 auger sampling event did not provide samples from two locations as stated by the tank characterization plan (Schreiber 1995). One riser was sampled rather than two, because of a lack of riser availability. However, the sampling and analysis for this tank was reviewed and found to be sufficient to satisfy the requirements of the Tank Safety Screening DQO (Reynolds et al. 1999). Table 5-3 lists the DQO-required analytes, their notification limits, and their analytical results.

The waste fuel energy value was determined by DSC. No exotherms were observed on the 1995 auger sample. Another indicator of fuel content is TOC concentration. The analytical TOC result for the drainable liquid was 1,260 $\mu\text{g C/ml}$, which is well below the Organics Safety Program limit of 30,000 $\mu\text{g C/ml}$ (Babad et al. 1994). The DSC and TOC results indicate that tank 241-c-101 waste does not contain excessive amounts of fuel.

Large amounts of moisture reduce the potential for propagating exothermic reactions in the waste. The percent water content of the waste was determined by TGA. All samples except the original sample of the crust material were above the notification limit of 17 percent. However, the implications for tank safety are probably minimal, given the endothermic DSC results. In addition, the average of the two crust sample analyses was above the notification limit indicating that the original crust analysis may be anomalous.

Another factor in assessing the safety of tank waste is the heat generation and temperature of the waste. Heat is generated in the tanks primarily from radioactive decay. No radiological results were obtained, but the Historical Tank Content Estimate of 11 W (38 British thermal units/hours [Btu/hr]) was well below the 40,000 Btu/hr threshold which separates high heat tanks from low heat tanks (Brevick et al. 1994). Thermocouple readings (Section 2.4.2) indicate that the radioactive decay heat in the tank is adequately dissipated throughout the year.

The potential for criticality can be assessed from the total alpha data. None of the individual subsamples from the 1995 auger sample contained alpha activity greater than 1.37 $\mu\text{Ci/g}$, and the mean result was 1.09 $\mu\text{Ci/g}$. This was well below the notification limit of 1 g/L (or 34.4 $\mu\text{Ci/g}$) as specified in the Tank Safety Screening DQO (Babad and Redus 1994) (see footnote b of Table 5-2).

Tank vapor samples were collected for this tank on September 1, 1994. Details of the sampling and analysis are documented in Huckaby (1995a) and are not reproduced here. The hydrogen, organic vapor fuel, and ammonia represent a combined total of 1.71 percent of the

6.0 CONCLUSIONS AND RECOMMENDATIONS

Tank 241-C-101 is a non-watch list tank and is an assumed leaker that was removed from service in 1976. The only recorded sampling events for tank 241-C-101 are a single segment auger sample taken in March of 1995 and tank vapor samples taken in September 1994. The auger sampling event was governed by the Tank Safety Screening DQO (Babad and Redus 1994). A second intended auger sample could not be taken because of an unavailable riser. Analysis of the auger sample taken was directed primarily at safety screening criteria TIC, TOC, pH, and bulk density were also measured to help interpret the origin of high CO₂ concentrations found in the vapor space. The chemical and radiochemical composition of the waste must be estimated solely from tank waste history. However, adequate data are available from the 1995 sampling and analysis event to support the current non-watch list status of this tank. The vapor sampling event supports the gas flammability question of the Tank Safety Screening DQO (Babad and Redus 1994).

The sampling and analysis of tank 241-C-101 was reviewed and found to be sufficient to satisfy the requirements of the Tank Safety Screening DQO (Reynolds et al. 1999). The analytical results fell within the safety screening criteria with the exception of an individual result for percent water. However, the rerun of this sample met the criteria. No exothermic reactions were exhibited by the DSC analysis, indicating that the fuel content of the tank is not excessive. The TOC content of the drainable liquid from the 1995 auger sample was found to be well below the safety program limit of 30,000 µg c/mL. In addition, the historical estimate of the tank heat load and tank temperatures do not indicate that excessive heat is being generated in the waste. The DSC results, low TOC results, and tank temperature readings indicate that the potential for runaway reactions in the waste is remote. The single low wt% water result is of low concern given the DSC, TOC, and temperature measurements. The tank vapor flammability, as determined by vapor sample analysis, was found to be 1.71 percent of the LFL, considerably below the safety screening limit.

The tank history indicates that the major waste types present are metal waste uranium recovery waste, and PUREX cladding waste. These waste types are known to have high aluminum, iron, sodium, sulfate, hydroxide, and nitrate. The major radionuclides are cesium and strontium. The water content and bulk density of the waste as estimated from the 1995 analytical data do not compare well with the Historical Tank Content Estimate (Brevick et al. 1994a). The chemical and radiochemical content estimates in the HTCE cannot be validated with the 1995 sample analysis results.

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