0050251 S

# ENGINEERING CHANGE NOTICE

Page 1 of 2

1. ECN № 622854

Proj. ECN

| 2. ECN Category (mark one) | 3. Originator's Name, Organization, MSIN, and Telephone No. | 4. USQ Required? | 5. Date |
|---|---|---|---|
| Supplemental [] <br> Direct Revision [X] <br> Change ECN [] <br> Temporary [] <br> Standby [] <br> Supersedure [] <br> Cancel/Void [] | M. J. Kupfer, LMHC, R3-75, 376-6631 | [] Yes [X] No | 9/30/98 |
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| | Tank 241-U-202 | NA | NA |
| | 9. Document Numbers Changed by this ECN (includes sheet no. and rev.) | 10. Related ECN No(s). | 11. Related PO No. |
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| 12a. Modification Work | 12b. Work Package No. | 12c. Modification Work Complete | 12d. Restored to Original Condition (Temp. or Standby ECN only) |
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| [] Yes (fill out Blk. 12b) <br> [X] No (NA Blks. 12b, 12c, 12d) | NA | NA <br> Design Authority/Cog. Engineer Signature & Date | NA <br> Design Authority/Cog. Engineer Signature & Date |

13a. Description of Change

13b. Design Baseline Document? [] Yes [X] No

This ECN revises the document to incorporate correct revision number and header.

14a. Justification (mark one)

| | | | | | | | |
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| Criteria Change | [] | Design Improvement | [] | Environmental | [] | Facility Deactivation | [] |
| As-Found | [X] | Facilitate Const | [] | Const. Error/Omission | [] | Design Error/Omission | [] |

14b. Justification Details

Incorrect revision was reported in the document header of the last ECN (6501000).

15. Distribution (include name, MSIN, and no. of copies)

| | | | |
|---|---|---|---|
| Central Files | B1-07 | K. M. Hodgson | R2-11 |
| DIMC | R1-41 | M. J. Kupfer | R3-75 |
| DOE Reading Room | H2-53 | M. D. LeClair (3) | R3-75 |
| TCSRC | R1-10 | J. Jo | R2-12 |
| K. M. Hall | R2-12 | | |

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# ENGINEERING CHANGE NOTICE



1. ECN (use no. from pg. 1): 622854

| 16. Design Verification Required | 17. Cost Impact | | | | 18. Schedule Impact (days) | |
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| | ENGINEERING | | CONSTRUCTION | | | |
| [] Yes | Additional | [] $ | Additional | [] $ | Improvement | [] |
| [X] No | Savings | [] $ | Savings | [] $ | Delay | [] |

19. Change Impact Review: Indicate the related documents (other than the engineering documents identified on Side 1) that will be affected by the change described in Block 13. Enter the affected document number in Block 20.

| | | | | | |
|---|---|---|---|---|---|
| SDD/DD | [] | Seismic/Stress Analysis | [] | Tank Calibration Manual | [] |
| Functional Design Criteria | [] | Stress/Design Report | [] | Health Physics Procedure | [] |
| Operating Specification | [] | Interface Control Drawing | [] | Spares Multiple Unit Listing | [] |
| Criticality Specification | [] | Calibration Procedure | [] | Test Procedures/Specification | [] |
| Conceptual Design Report | [] | Installation Procedure | [] | Component Index | [] |
| Equipment Spec. | [] | Maintenance Procedure | [] | ASME Coded Item | [] |
| Const. Spec. | [] | Engineering Procedure | [] | Human Factor Consideration | [] |
| Procurement Spec. | [] | Operating Instruction | [] | Computer Software | [] |
| Vendor Information | [] | Operating Procedure | [] | Electric Circuit Schedule | [] |
| OM Manual | [] | Operational Safety Requirement | [] | ICRS Procedure | [] |
| FSAR/SAR | [] | IEFD Drawing | [] | Process Control Manual/Plan | [] |
| Safety Equipment List | [] | Cell Arrangement Drawing | [] | Process Flow Chart | [] |
| Radiation Work Permit | [] | Essential Material Specification | [] | Purchase Requisition | [] |
| Environmental Impact Statement | [] | Fac. Proc. Samp. Schedule | [] | Tickler File | [] |
| Environmental Report | [] | Inspection Plan | [] | Other | [X] |
| Environmental Permit | [] | Inventory Adjustment Request | [] | | [] |

20. Other Affected Documents: (NOTE: Documents listed below will not be revised by this ECN.) Signatures below indicate that the signing organization has been notified of other affected documents listed below.

| Document Number/Revision | Document Number/Revision | Document Number Revision |
|---|---|---|
| NA | | |

21. Approvals

| | Signature | Date | | Signature | Date |
|---|---|---|---|---|---|
| Design Authority | | | Design Agent | | |
| Cog. Eng. M. J. Kupfer | M. J. Kupfer | 9-30-98 | PE | | |
| Cog. Mgr. K. M. Hodgson | K. M. Hodgson | 9-30-98 | QA | | |
| QA | | | Safety | | |
| Safety | | | Design | | |
| Environ. | | | Environ. | | |
| Other J. Jo R2-12 | J. Jo | 9-30-98 | Other | | |

DEPARTMENT OF ENERGY

Signature or a Control Number that tracks the Approval Signature

ADDITIONAL

# Tank Characterization Report for Single-Shell Tank 241-U-202

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Numatec Hanford Corporation, Richland, WA 99352
U.S. Department of Energy Contract DE-AC06-96RL13200

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Abstract: The best-basis inventory provides waste inventory estimates that serve as standard characterization source terms for the various waste management activities. To establish a best-basis inventory for single-shell tank 241-U-202, an evaluation of available information was performed. This work follows the methodology established in *Standard Inventories of Chemicals and Radionuclides in Hanford Site Tank Wastes*, HNF-SD-WM-TI-740, Rev. OA (Kupfer et al. 1997).

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Tank Characterization Report for Single-Shell Tank 241-U-202

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# APPENDIX C

# EVALUATION TO ESTABLISH BEST-BASIS INVENTORY FOR SINGLE-SHELL TANK 241-U-202

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# APPENDIX C

# EVALUATION TO ESTABLISH BEST-BASIS INVENTORY FOR SINGLE-SHELL TANK 241-U-202

An effort is underway to provide waste inventory estimates that will serve as standard characterization source terms for the various waste management activities (Hodgson and LeClair 1996). As part of this effort, an evaluation of available information for single-shell tank 241-U-202 was performed, and a best-basis inventory was established. This work, detailed in the following sections, follows the methodology that was established by the standard inventory task.

## C1.0 CHEMICAL INFORMATION SOURCES

Available chemical information for tank 241-U-202 include the following:

- Data from push mode cores taken in 1995 (Section 4.0). Only safety screening analyses were performed, therefore, the only data pertinent to this assessment were the total alpha and percent water assays.
- Data from two push mode cores taken in 1995 from tank 241-U-204, a tank with a closely related process history (Raphael and Tran 1995)
- Data from other tanks containing Reduction and Oxidation (REDOX) process (R)/REDOX cladding waste (CWR1) sludge, tanks 241-S-104 and 241-S-107 (DiCenso et al. 1994, Simpson et al. 1996).
- The inventory estimate for this tank generated from the Hanford Defined Waste (HDW) model (Agnew et al. 1997a), developed at Los Alamos National Laboratory (LANL).

## C2.0 COMPARISON OF COMPONENT INVENTORY VALUES

No sample-based inventory estimate is available for this tank. The HDW model estimates (Agnew et al. 1997a) for tank 241-U-202 are shown in Table C2-1 and C2-2. (The chemical species are reported without charge designation per the best-basis inventory convention.)

The HDW inventory estimates uses a solid waste volume of 15.1 kL (4 kgal), a supernatant volume of 3.8 kL (1 kgal), and an overall waste density of 1.62 g/mL. Note that the HDW model has been updated since the initial publication of this Tank Characterization Report (TCR); therefore, many of the values cited from the current version of the HDW model are not consistent with the version cited elsewhere in this TCR.

The calculation of a separate supernatant contribution will be excluded in the development and comparison of data-based inventory estimates because the inventory contributions from the supernatant (except for water) are typically within the calculated uncertainty. However, the total inventory estimate and volume (supernatant and sludge) from the HDW will be used as a basis for comparison.

Table C2-1. Hanford Defined Waste-Based Inventory Estimates for Nonradioactive Components in Tank 241-U-202.

| Analyte | HDW inventory estimate[a] (kg) | Analyte | HDW inventory estimate[a] (kg) |
|---|---|---|---|
| Al | 4,580 | $NO_3$ | 537 |
| Bi | 0 | OH | 10,700 |
| Ca | 73.3 | oxalate | 0 |
| Cl | 3.79 | Pb | 369 |
| Cr | 1.60 | $PO_4$ | 0 |
| F | 0 | Si | 8.55 |
| Fe | 139 | $SO_4$ | 12.2 |
| Hg | 12.4 | Sr | 0 |
| K | 0.91 | TIC as $CO_3$ | 110 |
| La | 0 | TOC | 0 |
| Mn | 0 | $U_{TOTAL}$ | 654 |
| Na | 2,730 | Zr | 0 |
| $NH_3$ | 0.0527 | $H_2O$ (wt%) | 33.9 |
| Ni | 0.91 | density (kg/L) | 1.62 |
| $NO_2$ | 667 | | |

HDW = Hanford Defined Waste
[a]Agnew et al. (1997a).

Table C2-2. Hanford Defined Waste Predicted Inventory Estimates for Radioactive Components in Tank 241-U-202.

| Analyte | HDW[a, b] inventory estimate (Ci) | Analyte | HDW[a, b] inventory estimate (Ci) |
|---|---|---|---|
| $^{90}Sr$ | 31.0 | $^{239}Pu$ | 24.4 |
| $^{137}Cs$ | 35.6 | $^{240}Pu$ | 3.43 |

HDW = Hanford Defined Waste

[a] Agnew et al. (1997a)

[b] The HDW model Rev. 4 reports inventories for 46 radionuclides. Only the four most significant are reported in this table. Radionuclides are decayed to January 1, 1994.

Table C2-3 shows the inventory derived from the 1995 core sample.

Table C2-3. Sample-Based Inventory of Tank 241-U-202.

| Analyte | Waste Concentration ($\mu$Ci/g) | Estimated Inventory [a] (Ci) |
|---|---|---|
| Total alpha | <0.00122 | <0.0242 |

[a] Based on a waste volume of 15.1 kL and the density of tank 241-U-204 waste (1.31 g/mL).

## C3.0 COMPONENT INVENTORY EVALUATION

The following evaluation of tank contents is performed in order to identify potential errors and/or missing information that would influence the sample-based and HDW model component inventories. The types and volumes of solids accumulated in tank 241-U-202 reported by various authors is compiled in Table C3-1.

### C3.1 CONTRIBUTING WASTE TYPES

The process history documents indicate the tank received mostly cladding waste from REDOX (CWR1) while the tank was active. Tank 241-U-202 went into service in 1956 receiving CWR1 from tank 241-U-110 through a diversion box (Agnew et al. 1997b). Before receiving CWR1, approximately 4,500 kL (1,190 kgal) of REDOX high-level (R) waste had been transferred through tank 241-U-110. The waste transferred to tank 241-U-202 may have

been a combination of CWR1 and R waste types. For the remainder of its service life (from 1956 to 1977) tank 241-U-202 stored CWR1 (Agnew 1997b).

Agnew et al. (1997a): CWR1
Hill et al. (1995): CW

CWR1 = REDOX process cladding waste (aluminum clad fuel–1952 to 1960)

CW = cladding waste

Current surveillance data (Hanlon 1997) provides estimated volumes for these waste types. Agnew et al. (1997a) uses these values for bases as well. There has been no change, such as salt well pumping, to alter the volumes. These are the values in Table C3-1 used to derive inventories.

Table C3-1. Waste Volumes for Tank 241-U-202.

| HDW[a] volumes | kL | kgal | Surveillance volumes[b] | kL | kgal |
|---|---|---|---|---|---|
| CWR1 | 15.1 | 4 | sludge | 15.1 | 4 |
| supernatant | 3.8 | 1 | supernatant | 3.8 | 1 |
| Total tank | 18.9 | 5 | Total tank | 18.9 | 5 |

HDW = Hanford Defined Waste
[a] Agnew et al. (1997a)
[b] Hanlon (1997).

## C3.2 ASSUMPTIONS

The following evaluation provides an engineering assessment of tank 241-U-202 contents. For this evaluation, the following assumptions and observations are made:

- Tank waste mass is calculated using the measured average density from similar tanks (1.62 g/mL) and the solids tank volume listed in Hanlon (1997). The Agnew et al. (1997a) estimates have the same overall density basis (1.62 g/mL).

- Only the CWR1 and R sludge waste streams contributed to solids formation.

- No comprehensive analytical data is available from tank 241-U-202.

- The sludge composition can be estimated by using sample-based concentrations from similar wastes (e.g. tanks 241-S-104, 241-S-107, and 241-U-204 [DiCenso et al. 1994, Simpson et al. 1995, and Raphael and Tran 1995]) for calculating the predicted engineering data set.

- No radiolysis of $NO_3$ to $NO_2$ is factored into this evaluation.

## C3.3 BASIS FOR CALCULATIONS USED IN THIS ENGINEERING EVALUATION

The general approach in this engineering assessment is to identify waste types and their approximate volumes within the tank of interest. The sources of information may include analytical data from samples taken from the tank of interest, analytical data from other tanks believed to contain waste types similar to those believed to be in the tank of interest, and data from models utilizing historical process records. The confidence level assigned to the best-basis inventory values then depends on the level of agreement among the various information sources. This approach is best suited for cases where extensive analytical data exist for multiple sampling events from a number of tanks containing similar waste types.

The CWR1 sludge concentrations used in this engineering assessment were developed with analytical data taken from tanks 241-U-204, 241-S-104, and 241-S-107. Some REDOX process waste may be intermixed in tank 241-U-202. However, the same situation applies in the tanks used to predict the R1 waste concentration. Thus, the waste is considered a mixture. Data were selected based on Agnew et al. (1997a) predicted sludge location.

The concentrations from each tank and the segments used in the calculation are shown in Table C3-2. In many cases, data from several sources were assessed and used, some data sets were selected in favor of others (usually when evidence of bias or high variability was observed), and some of the average values include detection limit values, where additional data suggest the detection limits are high. The mean from each specified set of tank data was averaged to obtain the projected concentration for each analyte for the sludge. The HDW model values for CWR1 sludge are also listed in Table C3-2 for comparison with the data-derived values.

Table C3-2. Mean Sludge Composition Estimate for 241-U-200 Tanks. (2 Sheets)

| Analyte | Tanks (segments) | | | Average concentration[d] (μg/g) | HDW model CWR1 concentration[e] (μg/g) |
|---|---|---|---|---|---|
| | 241-S-104[a] (all) (μg/g) | 241-S-107[b] (bottom 3) (μg/g) | 241-U-204[c] (average) (μg/g) | | |
| Al | 117,000 | 56,400 | 221,000 | 132,000 | 171,000 |
| B | 26.6 | 49 | <DL | 38 | NR |
| Bi | <45.7 | NR | 1,200 | <623 | 0 |
| Ca | 247 | 234 | 1,260 | 580 | 2,730 |
| Cl | 3,200 | 1,860 | 100 | 1,720 | 141 |
| Cr | 2,350 | 1,180 | 391 | 1,310 | 59.8 |
| F | 145 | 150 | 4,000 | 1,430 | 0 |
| Fe | 1,720 | 1,160 | 2,720 | 1,870 | 5,200 |
| K | 300 | 457 | 220 | 326 | 33.9 |
| Mn | 1,150 | 83 | 82 | 438 | 0 |
| Na | 121,000 | 60,400 | 18,200 | 66,500 | 102,000 |
| Ni | 56 | 206 | 3,940 | 1,400 | 33.7 |
| $NO_2$ | 25,900 | 34,300 | 3,000 | 21,100 | 24,900 |
| $NO_3$ | 191,000 | 57,600 | 12,000 | 86,900 | 20,000 |
| Pb | 29.6 | 33 | 7,300 | 2,450 | 13,800 |
| $PO_4$ | <2,190 | 1,630 | 2,150 | <1,990 | 0 |
| Si | 1,330 | 1,060 | 2,390 | 1,590 | 319 |
| $SO_4$ | 2,270 | 1,300 | 513 | 1,360 | 455 |
| Sr | 424 | 378 | 33.9 | 279 | 0 |
| TOC | 1,730 | NR | 471 | 1,100 | 0 |
| U | 6,690 | 8,686 | 1,410 | 5,600 | 24,400 |
| Zn | 20.1 | 24 | 902 | 315 | NR |
| Zr | 33.6 | 131 | 26.4 | 63.7 | 0 |
| density | 1.64 | 1.90 | 1.31 | 1.62 | 1.77 |

Table C3-2. Mean Sludge Composition Estimate for 241-U-200 Tanks. (2 Sheets)

| Analyte | Tanks (segments) | | | Average concentration[d] ($\mu$g/g) | HDW model CWR1 concentration[e] ($\mu$g/g) |
|---|---|---|---|---|---|
| | 241-S-104[a] (all) ($\mu$g/g) | 241-S-107[b] (bottom 3) ($\mu$g/g) | 241-U-204[c] (average) ($\mu$g/g) | | |
| Radionuclides[f] ($\mu$Ci/g) | | | | | |
| $^{137}$Cs | 60.5 | 74 | 2.55 | 45.7 | 1.33 |
| $^{90}$Sr | 301 | 276 | 0.0059 | 192 | 1.16 |
| $^{239/240}$Pu | 0.282 | NR | NR | 0.282 | 1.04 |
| Total $\propto$ | 0.617 | 0.525 | 0.0967 | 0.413 | NR |

DL = Detection limit
HDW = Hanford Defined Waste
NR = Not reported
[a] DiCenso et al. 1994
[b] Statistically determined median R1 sludge concentrations for tank 241-S-107 contained in attachment to Simpson et al. 1996
[c] Raphael and Tran 1995
[d] Average of analyte concentrations for tanks 241-S-104, 241-S-107, and 241-U-204
[e] Agnew et al. 1997a
[f] Radionuclides decayed to January 1, 1994.

## C3.4 INVENTORY COMPARISONS

Table C3-3 contains the total engineering assessment-based inventories calculated by developing the waste inventories using an average composition from tanks 241-S-104, 241-S-107, and 241-U-204 to produce the tank inventory as shown below. Calculations for Table C3-3 are: (average concentration of analyte in $\mu$g/g) x (solid waste [4 kgal]) x 3,785 L/kgal x 1,000 mL/L x (density [1.62 g/mL]) x kg/(1 E+09) $\mu$g = total kg for this waste type in the tank

Table C3-3. Comparison of Hanford Defined Waste-Based and Engineering Assessment Inventory Estimates for Tank 241-U-202. (2 Sheets)

| Element | 241-U-202 HDW estimate[a] (kg) | 241-U-202 engineering assessment estimate (kg) |
|---|---|---|
| Al | 4,580 | 3,240 |
| Bi | 1.56E-04 | <15.3 |
| Ca | 73.3 | 14.2 |
| Cl | 3.80 | 42.2 |
| Cr | 1.62 | 32.1 |
| F | 6.85E-04 | 35.1 |
| Fe | 139 | 45.9 |
| Pb | 369 | 60.0 |
| Mn | 0 | 10.7 |
| Ni | 0.91 | 34.3 |
| $NO_3$ | 538 | 2,130 |
| $NO_2$ | 667 | 518 |
| $PO_4$ | 3.42E-03 | <48.8 |
| K | 0.91 | 8.0 |
| Si | 8.55 | 40.0 |
| Na | 2,730 | 1,630 |
| Sr | 0 | 6.84 |
| $SO_4$ | 12.2 | 33.3 |
| TOC | 0 | 27.0 |
| U | 653 | 137 |
| Zn | NR | 7.72 |
| Zr | 5.66E-06 | 1.56 |
| Density (g/mL) | 1.62 | 1.62 |
| wt% $H_2O$ | 33.9 | 29.3 |

Table C3-3. Comparison of Hanford Defined Waste-Based and Engineering Assessment Inventory Estimates for Tank 241-U-202. (2 Sheets)

| Element | 241-U-202 HDW estimate[a] (kg) | 241-U-202 engineering assessment estimate (kg) |
|---|---|---|
| Radionuclides[b] (Ci) | | |
| $^{137}Cs$ | 35.8 | 1,120 |
| $^{90}Sr$ | 31.1 | 4,710 |
| $^{239/240}Pu$ | 27.8 | 6.92 |
| Total $\alpha$ | NR | 10.1 |

HDW = Hanford Defined Waste
[a] Agnew et al. (1997a)
[b] Radionuclides decayed to January 1, 1994.

## C3.5 DOCUMENT ELEMENT BASIS

This section compares the engineering assessment and the inventory estimate calculated by the HDW model for selected analytes. Many of the differences observed between the estimates can be attributed to the differences in their respective mass bases. In other cases, the source term for the analyte in the waste type does not appear to be accurately described. Several analytes such as bismuth, nickel, manganese, phosphate, and TOC are not principal process chemicals in the CWR1 waste, but may be present in larger than expected amounts as a result of mixing with the first cycle bismuth phosphate process waste present in tank 241-U-110.

**Aluminum**. The two estimates are reasonably close. The engineering assessment is about 29 percent lower than the HDW estimate. They qualitatively agree that aluminum is a principal contributor to the waste in this tank. The difference in concentration between the HDW model and the average concentration based on other tanks is approximately 26 percent, accounting for most of the discrepancy. The data-based estimate may be biased low because of the acid-digestion result used from tank 241-S-107. The aluminum value from that tank could be much higher because of incomplete quantitation of the samples. However, given the assumptions of the HDW model and the measurement uncertainty, these values are in agreement.

**Nitrate.** The engineering assessment is about four times higher than the HDW estimate. They qualitatively agree that nitrate is a principal contributor to the waste in this tank. The source concentrations are approximately a factor of four different, accounting for nearly all of the discrepancy. Thus, there appears to be a source term error in the HDW model.

**Nitrite**. The two estimates are reasonably close. The engineering assessment is about 22 percent lower than the HDW estimate. They qualitatively agree that nitrite is a principal contributor to the waste in this tank. The source concentrations are approximately 17 percent different, accounting for much of the discrepancy. However, given the assumptions of the HDW model and the measurement uncertainty, these values are in agreement.

**Sodium**. The engineering assessment is 40 percent lower than the HDW estimate. They qualitatively agree that sodium is a principal contributor to the waste in this tank. The source concentrations are approximately a factor of two different, accounting for nearly all of the discrepancy. However, the contributing waste data were highly variable, and significant differences were evident between the data from the two S Tank Farm tanks and tank 241-U-204. Thus, there may be a source term error in the HDW model, or the sample data available may not be representative of the waste in the tank.

**Total Hydroxide.** Once the best-basis inventories were determined, the hydroxide inventory was calculated by performing a charge balance with the valences of other analytes. This charge balance approach is consistent with that used by Agnew et al. (1997a).

**Water**. The two estimates are very close. They qualitatively agree that water is a principal contributor to the waste in this tank. However, because of the volatility of water over time, the relatively small magnitude of the discrepancy observed is unexpected. This suggests that the heat load in the tank is small and the degree of air exchange with the outside is restricted.

## C4.0 DEFINE THE BEST-BASIS AND ESTABLISH COMPONENT INVENTORIES

Information about chemical, radiological, and/or physical properties is used to perform safety analyses, engineering evaluations, and risk assessment associated with waste management activities, as well as regulatory issues. These activities include overseeing tank farm operations and identifying, monitoring, and resolving safety issues associated with these operations and with the tank wastes. Disposal activities involve designing equipment, processes, and facilities for retrieving wastes and processing them into a form that is suitable for long-term storage/disposal.

Chemical and radiological inventory information are generally derived using three approaches: (1) component inventories are estimated using results of sample analyses, (2) component inventories are estimated using the HDW model based on process knowledge and historical information, or (3) a tank-specific process estimate is made based on process flowsheets, reactor fuel data, essential material usage, and other operating data. The information derived from these different approaches is often inconsistent

An evaluation of available chemical information for tank 241-U-202 was performed, including the following:

- An inventory estimate generated by the HDW model (Agnew et al. 1997a)
- A data-based inventory developed from concentration information from similar tanks.

Based on this evaluation, a best-basis inventory was developed for tank 241-U-202. No sampling information was available for tank 241-U-202; however, several tanks which were believed to contain similar wastes were used to derive an inventory. The data-based evaluation inventory was chosen as the best basis for those analytes for which sample-based analytical values were available for the following reasons:

- No independent data sources are available to predict CWR1 compositions from process flowsheet or historical records
- The engineering assessment inventory estimates appear reasonable, given the process knowledge available.
- For those few analytes where no values were available from the data-based inventory, or the estimate was considered suspect, the HDW model values were used.

Best-basis tank inventory values are derived for 46 key radionuclides (as defined in Section 3.1 of Kupfer et al. 1997), all decayed to a common report date of January 1, 1994. Often, waste sample analyses have only reported $^{90}Sr$, $^{137}Cs$, $^{239/240}Pu$, and total uranium (or total beta and total alpha), while other key radionuclides such as $^{60}Co$, $^{99}Tc$, $^{129}I$, $^{154}Eu$, $^{155}Eu$, and $^{241}Am$, etc., have been infrequently reported. For this reason it has been necessary to derive most of the 46 key radionuclides by computer models. These models estimate radionuclide activity in batches of reactor fuel, account for the split of radionuclides to various separations plant waste streams, and track their movement with tank waste transactions. (These computer models are described in Kupfer et al. 1997, Section 6.1 and in Watrous and Wootan 1997.) Model generated values for radionuclides in any of 177 tanks are reported in the HDW Rev. 4 model results (Agnew et al. 1997a). The best-basis value for any one analyte may be either a model result or a sample or engineering assessment-based result if available. For a discussion of typical error between model derived values and sample derived values, see Kupfer et al. 1997, Section 6.1.10.

The best-basis inventory for tank 241-U-202 is presented in Tables C4-1 and C4-2. The inventory values reported in Tables C4-1 and C4-2 are subject to change. Refer to the Tank Characterization Database (TCD) (LMHC 1998) for the most current inventory values.

Table C4-1. Best-Basis Inventory Estimates for Nonradioactive Components in Tank 241-U-202 (Effective May 31, 1997).

| Analyte | Total inventory (kg) | Basis (S, M, C or E)[1] | Comment |
|---|---|---|---|
| Al | 3,240 | E | |
| Bi | 15.3 | E | Bounding value |
| Ca | 14.2 | E | |
| Cl | 42.2 | E | |
| TIC as $CO_3$ | 110 | M | |
| Cr | 32.1 | E | |
| F | 35.1 | E | |
| Fe | 45.9 | E | |
| Hg | 2.91 | E | Simpson (1998) |
| K | 8.0 | E | |
| La | 0 | E | No history of 224 waste |
| Mn | 10.7 | E | |
| Na | 1,630 | E | |
| Ni | 34.3 | E | |
| $NO_2$ | 518 | E | |
| $NO_3$ | 2,130 | E | |
| $OH_{TOTAL}$ | 6,580 | C | Derived from charge balance |
| Pb | 60.0 | E | |
| $PO_4$ | 48.8 | E | Bounding value |
| Si | 40.0 | E | |
| $SO_4$ | 33.3 | E | |
| Sr | 6.84 | E | |
| TOC | 27.0 | E | |
| $U_{TOTAL}$ | 28.0 | E | From U-204 only. |
| Zr | 1.56 | E | |

[1]S = Sample-based

M = Hanford Defined Waste model-based, Agnew et al. (1997a)

E = Engineering assessment-based

C = Calculated by charge balance; includes oxides as hydroxides, not including $CO_3$, $NO_2$, $NO_3$, $PO_4$, $SO_4$, and $SiO_3$.

Table C4-2. Best-Basis Inventory Estimates for Radioactive Components in Tank 241-U-202 Decayed to January 1, 1994 (Effective May 31, 1997). (2 Sheets)

| Analyte | Total inventory (Ci) | Basis (S, M, or E)[1] | Comment |
|---|---|---|---|
| $^{3}H$ | 0.0153 | M | |
| $^{14}C$ | 0.00165 | M | |
| $^{59}Ni$ | 4.68E-04 | M | |
| $^{60}Co$ | 7.14E-04 | M | |
| $^{63}Ni$ | 0.0439 | M | |
| $^{79}Se$ | 3.59E-04 | M | |
| $^{90}Sr$ | 4,710 | E | |
| $^{90}Y$ | 4,710 | E | Referenced to $^{90}Sr$ |
| $^{93}Zr$ | 0.0017 | M | |
| $^{93m}Nb$ | 0.00138 | M | |
| $^{99}Tc$ | 0.0119 | M | |
| $^{106}Ru$ | 4.17E-09 | M | |
| $^{113m}Cd$ | 0.00531 | M | |
| $^{125}Sb$ | 0.00119 | M | |
| $^{126}Sn$ | 5.47E-04 | M | |
| $^{129}I$ | 2.27E-05 | M | |
| $^{134}Cs$ | 2.50E-05 | M | |
| $^{137}Cs$ | 1,120 | E | |
| $^{137m}Ba$ | 1,060 | E | Referenced to $^{137}Cs$ |
| $^{151}Sm$ | 1.28 | M | |
| $^{152}Eu$ | 0.00265 | M | |
| $^{154}Eu$ | 0.0174 | M | |
| $^{155}Eu$ | 0.126 | M | |
| $^{226}Ra$ | 4.28E-08 | M | |
| $^{227}Ac$ | 2.20E-07 | M | |
| $^{228}Ra$ | 4.42E-12 | M | |
| $^{229}Th$ | 6.25E-10 | M | |
| $^{231}Pa$ | 5.21E-07 | M | |
| $^{232}Th$ | 6.11E-13 | M | |
| $^{232}U$ | 4.19E-07 | E/M | From total U |

Table C4-2. Best-Basis Inventory Estimates for Radioactive Components in Tank 241-U-202 Decayed to January 1, 1994 (Effective May 31, 1997). (2 Sheets)

| Analyte | Total inventory (Ci) | Basis (S, M, or E)[1] | Comment |
|---|---|---|---|
| $^{233}U$ | 1.55E-08 | E/M | From total U |
| $^{234}U$ | 9.59E-03 | E/M | From total U |
| $^{235}U$ | 4.07E-04 | E/M | From total U |
| $^{236}U$ | 2.11E-04 | E/M | From total U |
| $^{237}Np$ | 8.30E-05 | M | |
| $^{238}Pu$ | 6.27E-05 | S/M | Total alpha distribution |
| $^{238}U$ | 9.34E-03 | E/M | From total U |
| $^{239}Pu$ | 4.02E-03 | S/M | Total alpha distribution |
| $^{240}Pu$ | 5.67E-04 | S/M | Total alpha distribution |
| $^{241}Am$ | 1.02E-06 | S/M | Total alpha distribution |
| $^{241}Pu$ | 3.46E-03 | S/M | Total alpha distribution |
| $^{242}Cm$ | 9.13E-09 | S/M | Total alpha distribution |
| $^{242}Pu$ | 1.47E-08 | S/M | Total alpha distribution |
| $^{243}Am$ | 9.32E-12 | S/M | Total alpha distribution |
| $^{243}Cm$ | 2.08E-10 | S/M | Total alpha distribution |
| $^{244}Cm$ | 3.25E-10 | S/M | Total alpha distribution |

[1]S = Sample-based
M = Hanford Defined Waste model-based, Agnew et al. (1997a)
E = Engineering assessment-based.

## C5.0 APPENDIX C REFERENCES

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