

ENGINEERING CHANGE NOTICE	Page 1 of <u>2</u>	1. ECN 643408
		Proj. ECN

2. ECN Category (mark one) Supplemental <input checked="" type="checkbox"/> <i>18</i> Direct Revision <input checked="" type="checkbox"/> Change ECN <input type="checkbox"/> Temporary <input type="checkbox"/> Standby <input type="checkbox"/> Supersedeure <input type="checkbox"/> Cancel/Void <input type="checkbox"/>	3. Originator's Name, Organization, MSIN, and Telephone No. B. C. Simpson, LMHC, R2-12 373-5915	4. USQ Required? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	5. Date 08/20/97
	6. Project Title/No./Work Order No. Tank 241-U-203	7. Bldg./Sys./Fac. No. NA	8. Approval Designator NA
	9. Document Numbers Changed by this ECN (includes sheet no. and rev.) WHC-SD-WM-ER-485, Rev. 0B	10. Related ECN No(s). NA	11. Related PD No. NA

12a. Modification Work <input type="checkbox"/> Yes (fill out Blk. 12b) <input checked="" type="checkbox"/> No (NA Blks. 12b, 12c, 12d)	12b. Work Package No. NA	12c. Modification Work Complete NA <hr/> Design Authority/Cog. Engineer Signature & Date	12d. Restored to Original Condition (Temp. or Standby ECN only) NA <hr/> Design Authority/Cog. Engineer Signature & Date
--	------------------------------------	--	--

13a. Description of Change Add Appendix B, Evaluation to Establish Best-Basis Inventory for Single-Shell Tank 241-U-203.	13b. Design Baseline Document? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
--	---

14a. Justification (mark one)			
Criteria Change <input type="checkbox"/>	Design Improvement <input type="checkbox"/>	Environmental <input type="checkbox"/>	Facility Deactivation <input type="checkbox"/>
As-Found <input checked="" type="checkbox"/>	Facilitate Const <input type="checkbox"/>	Const. Error/Omission <input type="checkbox"/>	Design Error/Omission <input type="checkbox"/>

14b. Justification Details

An effort is underway to provide waste inventory estimates that will serve as standard characterization source terms for the various waste management activities. As part of this effort, an evaluation of available information for single-shell tank 241-U-203 was performed, and a best-basis inventory was established. This work follows the methodology that was established by the standard inventory task.

15. Distribution (include name, MSIN, and no. of copies)			
Central Files	A3-88	K. M. Hall	R2-12
DOE Reading Room	H2-53	K. M. Hodgson	R2-11
TCSRC	R1-10	R. T. Winward	H5-49
File	H5-49	R. D. Schreiber	R2-12
B. C. Simpson	R2-12		
M. J. Kupfer	H5-49		
M. D. LeClair (3)	H0-50		

RELEASE STAMP

AUG 27 1997

DATE: _____

STA: 37

HANFORD
RELEASE

ID: 20

Tank Characterization Report for Single-Shell Tank 241-U-203

B. C. Simpson (LMHC) and R. T. Winward (Meier Associates)
Lockheed Martin Hanford Corporation, Richland, WA 99352
U.S. Department of Energy Contract DE-AC06-96RL13200

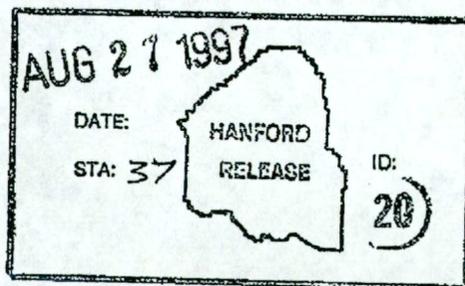
EDT/ECN: 643408 UC: 712
Org Code: 74610 Charge Code: N4G3A
B&R Code: EW3120074 Total Pages: 77

Key Words: TCR, best-basis inventory

Abstract: An effort is underway to provide waste inventory estimates that will serve as standard characterization source terms for the various waste management activities. As part of this effort, an evaluation of available information for single-shell tank 241-U-203 was performed, and a best-basis inventory was established. This work follows the methodology that was established by the standard inventory task.

TRADEMARK DISCLAIMER. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors.

Printed in the United States of America. To obtain copies of this document, contact: Document Control Services, P.O. Box 950, Mailstop H6-08, Richland WA 99352, Phone (509) 372-2420; Fax (509) 376-4989.



Janis Bishop 8/27/97
Release Approval Date

Release Stamp

Approved for Public Release

APPENDIX B

**EVALUATION TO ESTABLISH BEST-BASIS
INVENTORY FOR SINGLE-SHELL
TANK 241-U-203**

This page intentionally left blank.

APPENDIX B**EVALUATION TO ESTABLISH BEST-BASIS INVENTORY FOR
SINGLE-SHELL TANK 241-U-203**

An effort is underway to provide waste inventory estimates that will serve as standard characterization source terms for the various waste management activities (Hodgson and LeClair 1996). As part of this effort, an evaluation of available information for single-shell tank 241-U-203 was performed, and a best-basis inventory was established. This work, detailed in the following sections, follows the methodology that was established by the standard inventory task.

B1.0 CHEMICAL INFORMATION SOURCES

Available chemical information for tank 241-U-203 include the following:

- Data from push mode cores taken in 1995 (Section 4.0). Only safety screening analyses were performed, therefore, the only data pertinent to this assessment were the total alpha and percent water assays.
- Data from two push mode cores taken in 1995 from tank 241-U-204, a tank with a closely related process history (Raphael and Tran 1995)
- Data from other tanks containing Reduction and Oxidation (REDOX) process (R)/REDOX cladding waste (CWR1) sludge, tanks 241-S-104 and 241-S-107 (DiCenso et al. 1994, Simpson et al. 1996).
- The inventory estimate for this tank generated from the Hanford Defined Waste (HDW) model (Agnew et al. 1997a), developed at Los Alamos National Laboratory (LANL).

B2.0 COMPARISON OF COMPONENT INVENTORY VALUES

No sample-based inventory estimate is available for this tank. The HDW model estimates (Agnew et al. 1997a) for tank 241-U-203 are shown in Table B2-1 and B2-2. The chemical species are reported without charge designation per the best-basis inventory convention.

The HDW inventory estimates uses a solid waste volume of 7.6 kL (2 kgal), a supernatant volume of 3.8 kL (1 kgal), and an overall waste density of 1.71 g/mL. Note that the HDW model has been updated since the initial publication of this Tank Characterization Report (TCR), therefore, many of the values cited from the current version of the HDW model are not consistent with the version cited in the body of this TCR.

The calculation of a separate supernatant contribution will be excluded in the development and comparison of data-based inventory estimates, because the inventory contributions from the supernatant (except for water) are typically within the calculated uncertainty. However, the total inventory estimate and volume (supernatant and sludge) from the HDW will be used as a basis for comparison.

Table B2-1. Hanford Defined Waste-Based Inventory Estimates for Nonradioactive Components in Tank 241-U-203.

Analyte	HDW ^a inventory estimate (kg)	Analyte	HDW ^a inventory estimate (kg)
Al	2,540	NO ₃	1,190
Bi	0.326	OH	6,200
Ca	40.2	oxalate	0
Cl	23.3	Pb	186
Cr	35.6	P as PO ₄	7.16
F	1.43	Si	10.4
Fe	70.8	S as SO ₄	26.6
Hg	6.20	Sr	0
K	5.60	TIC as CO ₃	62.8
La	0	TOC	0
Mn	0	U _{TOTAL}	335
Na	2,420	Zr	0.0118
NH ₃	2.22	H ₂ O (wt%)	29.0
Ni	1.46	density (kg/L)	1.71
NO ₂	832		

HDW = Hanford Defined Waste

^a Agnew et al. (1997a).

Table B2-2. Hanford Defined Waste Predicted Inventory Estimates for Radioactive Components in Tank 241-U-203.

Analyte	HDW ^{a, b} inventory estimate (Ci)	Analyte	HDW ^{a, b} inventory estimate (Ci)
⁹⁰ Sr	225	²³⁹ Pu	12.3
¹³⁷ Cs	529	²⁴⁰ Pu	1.73

NR = Not reported

^a Agnew et al. (1997b)

^b The HDW model Rev. 4 reports inventories for 46 radionuclides. Only the four most significant are reported in this table. Radionuclides are decayed to January 1, 1994.

B3.0 COMPONENT INVENTORY EVALUATION

The following evaluation of tank contents is performed in order to identify potential errors and/or missing information that would influence the sample-based and HDW model component inventories. The types and volumes of solids accumulated in tank 241-U-203 reported by various authors is compiled in Table B3-1.

B3.1 CONTRIBUTING WASTE TYPES

The process history documents indicate the tank received mostly cladding waste from REDOX (CWR1) while the tank was active. Tank 241-U-203 went into service in 1956 receiving CWR1 from tank 241-U-110 through a diversion box (Agnew et al. 1997b). Before receiving CWR1, approximately 4,500 kL (1,190 kgal) of REDOX high-level (R) waste had been transferred through tank 241-U-110. The waste transferred to tank 241-U-203 may have been a combination of CWR1 and R waste types. For the remainder of its service life (1956 to 1977) tank 241-U-203 stored CWR1 (Agnew et al. 1997b).

Agnew et al. (1997a): CWR1

Hill et al. (1995): CW

CWR1 = REDOX process cladding waste (aluminum clad fuel--1952 to 1960)

CW = cladding waste

Current surveillance data (Hanlon 1997) provide estimated volumes for these waste types. Agnew et al. (1997a) uses these values for bases as well. There has been no change,

such as salt well pumping, to alter the volumes. These are the values in Table B3-1 used to derive inventories. The total volume is used in calculating inventories.

Table B3-1. Waste Volumes for Tank 241-U-203.

HDW ^a volumes	kL	kgal	Surveillance volumes ^b	kL	kgal
CWR1	7.6	2	sludge	7.6	2
supernatant	3.8	1	supernatant	3.8	1
Total tank	11.4	3	Total tank	11.4	3

CWR = Reduction and Oxidation (REDOX) Cladding Waste

HDW = Hanford Defined Waste

^a Agnew et al. (1997a)

^b Hanlon (1997).

B3.2 ASSUMPTIONS

The following evaluation provides an engineering assessment of tank 241-U-203 contents. For this evaluation, the following assumptions and observations are made:

- Tank waste mass is calculated using the measured average density from similar tanks (1.62 g/mL) and the solids tank volume listed in Hanlon (1997). The Agnew et al. (1997a) estimates have a different overall and sludge density basis (1.71 g/mL, and 1.77 g/mL, respectively).
- Only the CWR1 and R sludge waste streams contributed to solids formation.
- No comprehensive analytical data are available from tank 241-U-203.
- The sludge composition can be estimated by using sample-based concentrations from similar wastes (e.g. tanks 241-S-104, 241-S-107, and 241-U-204 [DiCenso et al. 1994, Simpson et al. 1996, and Raphael and Tran 1995]) for calculating the predicted engineering data set.
- No radiolysis of NO₃ to NO₂ is factored into this evaluation.

B3.3 BASIS FOR CALCULATIONS USED IN THIS ENGINEERING EVALUATION

The general approach in this engineering assessment is to identify waste types and their approximate volumes within the tank of interest. The sources of information may include analytical data from samples taken from the tank of interest, analytical data from other tanks thought to contain waste types similar to those thought to be in the tank of interest, and data from models utilizing historical process records. The confidence level assigned to the best-basis inventory values then depends on the level of agreement among the various information sources. This approach is best suited for cases where extensive analytical data exist from multiple sampling events from a number of tanks containing similar waste types.

The CWR1 sludge concentrations used in this engineering assessment were developed with analytical data taken from tanks 241-U-204, 241-S-104, and 241-S-107. Some REDOX process waste may be intermixed in tank 241-U-203. However, the same situation applies in the tanks used to predict the REDOX high-level waste generated between 1952 to 1957 (R1) waste concentration. Thus, the waste is considered a mixture. Data were selected based on Agnew et al. (1997a) predicted sludge location.

The concentrations from each tank and the segments used in the calculation are shown in Table B3-2. In many cases, data from several sources were assessed and used, some data sets were selected in favor of others (usually when evidence of bias or high variability was observed), and some of the average values include detection limit values, where additional data suggest the detection limits are high. The mean from each specified set of tank data was averaged to obtain the projected concentration for each analyte for the sludge. The HDW model values for CWR1 sludge are also listed in Table B3-2 for comparison with the data-derived values.

Table B3-2. Mean Sludge Composition Estimate for 241-U-200 Tanks (2 Sheets)

Analyte	Tanks (segments)			Average concentration ^d ($\mu\text{g/g}$)	HDW model CWR1 concentration ^e ($\mu\text{g/g}$)
	241-S-104 ^a (all) ($\mu\text{g/g}$)	241-S-107 ^b (segments) ($\mu\text{g/g}$)	241-U-204 ^c (average) ($\mu\text{g/g}$)		
Al	117,000	56,400	221,000	132,000	171,000
B	26.6	49	<DL	38	NR
Bi	<45.7	NR	1,200	<623	0
Ca	247	234	1,260	580	2,730
Cl	3,200	1,860	100	1,720	141
Cr	2,350	1,180	391	1,310	59.8
F	145	150	4,000	1,430	0
Fe	1,720	1,160	2,720	1,870	5,200

Table B3-2. Mean Sludge Composition Estimate for 241-U-200 Tanks (2 Sheets)

Analyte	Tanks (segments)			Average concentration ^d ($\mu\text{g/g}$)	HDW model CWR1 concentration ^e ($\mu\text{g/g}$)
	241-S-104 ^a (all) ($\mu\text{g/g}$)	241-S-107 ^b (segments) ($\mu\text{g/g}$)	241-U-204 ^c (average) ($\mu\text{g/g}$)		
K	300	457	220	326	33.9
Mn	1,150	83	82	438	0
Na	121,000	60,400	18,200	66,500	102,000
Ni	56	206	3,940	1,400	33.7
NO ₂	25,900	34,300	3,000	21,100	24,900
NO ₃	191,000	57,600	12,000	86,900	20,000
Pb	29.6	33	7,300	2,450	13,800
PO ₄	<2,190	1,630	2,150	<1,990	0
Si	1,330	1,060	2,390	1,590	319
SO ₄	2,270	1,300	513	1,360	455
Sr	424	378	33.9	279	0
TOC	1,730	NR	471	1,100	0
U	6,690	8,686	1,410	5,600	24,400
Zn	20.1	24	902	315	NR
Zr	33.6	131	26.4	63.7	0
density	1.64	1.90	1.31	1.62	1.77
Radionuclides ^f ($\mu\text{Ci/g}$)					
¹³⁷ Cs	60.5	276	3.96	113	1.33
⁹⁰ Sr	301	74	0.0092	125	1.16
^{239/240} Pu	0.282	NR	0.097	0.19	1.04

DL = Detection limit

HDW = Hanford Defined Waste

NR = Not reported

^a DiCenso et al. (1994)

^b Statistically determined median R1 sludge concentrations for tank 241-S-107 contained in attachment to Simpson et al. (1996)

^c Raphael and Tran (1995)

^d Average of analyte concentrations for tanks 241-S-104, 241-S-107, and 241-U-204

^e Agnew et al. (1997a)

^f Radionuclides decayed to January 1, 1994.

B3.4 INVENTORY COMPARISONS

Table B3-3 contains the total engineering assessment-based inventories calculated by developing the waste inventories using an average composition from tanks 241-S-104, 241-S-107, and 241-U-204 to produce the tank inventory as shown below. Calculations for Table B3-3 are: (average concentration of analyte in $\mu\text{g/g}$) x (total waste [2 kgal]) x 3,785 L/kgal x 1,000 mL/L x (density [1.62 g/mL]) x kg/(1 E+09) μg = total kg for this waste type in the tank

Table B3-3. Comparison of Hanford Defined Waste-Based and Data-Based Inventory Estimates for Tank 241-U-203. (2 Sheets)

Element	241-U-203 HDW estimate ^a (kg)	241-U-203 Data-based estimate (kg)
Al	2,540	1,620
Bi	0.326	<7.64
Ca	40.2	7.11
Chloride	23.3	21.1
Cr	35.6	13.9
F	1.43	17.5
Fe	70.8	22.9
Pb	186	30.0
Mn	0	5.37
Ni	1.46	17.2
NO ₃	1,190	1,070
NO ₂	832	258
PO ₄	7.16	24.4
K	5.60	3.99
Si	10.4	19.5
Na	2,420	816
Sr	0	3.42
SO ₄	26.6	16.7
TOC	0	13.5
U	335	68.7
Zn	NR	3.86
Zr	0.0118	0.78

Table B3-3. Comparison of Hanford Defined Waste-Based and Data-Based Inventory Estimates for Tank 241-U-203. (2 Sheets)

Element	241-U-203 HDW estimate ^a (kg)	241-U-203 Data-based estimate (kg)
Density (g/mL)	1.71	1.62
wt% H ₂ O	29.0	28.1
Radionuclides ^b (Ci)		
¹³⁷ Cs	529	1,390
⁹⁰ Sr	225	1,530
^{239/240} Pu	13.76	2.33

HDW = Hanford Defined Waste

^aAgnew et al. (1997a)

^bRadionuclides are decayed to January 1, 1994.

B3.5 DOCUMENT ELEMENT BASIS

This section compares the sample-based estimate, the engineering assessment, and the inventory estimate calculated by the HDW model for selected analytes. Many of the differences observed between the estimates can be attributed to the differences in their respective mass bases. In other cases, the source term for the analyte in the waste type does not appear to be accurately described. Several analytes such as bismuth, nickel, manganese, phosphate, and TOC are not principal process chemicals in the CWR1 waste, but may be present in larger than expected amounts as a result of mixing with the first cycle bismuth phosphate process waste present in tank 241-U-110.

Aluminum. The two estimates are reasonably close. The data-based assessment is about 36 percent lower than the HDW estimate. They qualitatively agree that aluminum is a principal contributor to the waste in this tank. The difference in concentration between the HDW model and the average concentration based on other tanks is approximately 26 percent, accounting for much of the discrepancy. The data-based estimate may be biased low because of the acid-digestion result used from tank 241-S-107. The aluminum value from that tank could be much higher because of incomplete quantitation of the samples.

Nitrate. The data-based assessment is about 10 percent lower than the HDW estimate. They qualitatively agree that nitrate is a principal contributor to the waste in this tank. The source concentrations are approximately a factor of four different. This condition suggests a case of coincidental agreement. Thus, there appears to be a source term error in the HDW model.

Nitrite. The two estimates are about a factor of three different. They qualitatively agree that nitrite is a principal contributor to the waste in this tank. The source concentrations are approximately 17 percent different, accounting for a small part of the discrepancy. However, there appears to be an error or incomplete description of the tank history in the HDW model.

Sodium. The data-based assessment is 3 times lower than the HDW estimate. They qualitatively agree that sodium is a principal contributor to the waste in this tank. The source concentrations are approximately a factor of two different, accounting for most of the discrepancy. However the contributing waste data were highly variable, and significant differences were evident between the data from the two 241-S farm tanks and tank 241-U-204. Thus, there may be a source term error in the HDW model, or the sample data available may not be representative of the waste in the tank.

Total Hydroxide. Once the best-basis inventories were determined, the hydroxide inventory was calculated by performing a charge balance with the valences of other analytes. In some cases, this approach requires that other analyte (e.g., sodium or nitrate) inventories be adjusted to achieve the charge balance. During such adjustments, the number of significant figures is not increased. This charge balance approach is consistent with that used by Agnew et al. (1997a).

Water. The two estimates are very close. They qualitatively agree that water is a principal contributor to the waste in this tank. However, because of the volatility of water over time, the relatively small magnitude of the discrepancy observed is unexpected. This suggests that the heat load in the tank is small and the degree of air exchange with the outside is restricted.

B4.0 DEFINE THE BEST-BASIS AND ESTABLISH COMPONENT INVENTORIES

Information about chemical, radiological, and/or physical properties is used to perform safety analyses, engineering evaluations, and risk assessment associated with waste management activities, as well as regulatory issues. These activities include overseeing tank farm operations and identifying, monitoring, and resolving safety issues associated with these operations and with the tank wastes. Disposal activities involve designing equipment, processes, and facilities for retrieving wastes and processing them into a form that is suitable for long-term storage/disposal.

Chemical and radiological inventory information are generally derived using three approaches: (1) component inventories are estimated using results of sample analyses, (2) component inventories are estimated using the HDW model based on process knowledge and historical information, or (3) a tank-specific process estimate is made based on process flowsheets, reactor fuel data, essential material usage, and other operating data. The information derived from these different approaches is often inconsistent.

An evaluation of available chemical information for tank 241-U-203 was performed, including the following:

- An inventory estimate generated by the HDW model (Agnew et al. 1997a)
- A data-based inventory developed from concentration information from similar tanks.

Based on this evaluation, a best-basis inventory was developed for tank 241-U-203. No sampling information was available for tank 241-U-203; however, several tanks which were thought to contain similar wastes were used to derive an inventory. The data-based evaluation inventory was chosen as the best basis for those analytes for which sample-based analytical values were available for the following reasons:

- No independent data sources are available to predict CWR1 compositions from process flowsheet or historical records.
- The data-based inventory estimates appear reasonable, given the process knowledge available.
- For those few analytes where no values were available from the data-based inventory, or the estimate was considered suspect, the HDW model values were used.

Best-basis tank inventory values are derived for 46 key radionuclides (as defined in Section 3.1 of Kupfer et al. 1997), all decayed to a common report date of January 1, 1994. Often, waste sample analyses have only reported ^{90}Sr , ^{137}Cs , $^{239/240}\text{Pu}$, and total uranium (or

total beta and total alpha), while other key radionuclides such as ^{60}Co , ^{99}Tc , ^{129}I , ^{154}Eu , ^{155}Eu , and ^{241}Am , etc., have been infrequently reported. For this reason it has been necessary to derive most of the 46 key radionuclides by computer models. These models estimate radionuclide activity in batches of reactor fuel, account for the split of radionuclides to various separations plant waste streams, and track their movement with tank waste transactions. (These computer models are described in Kupfer et al. 1997, Section 6.1 and in Watrous and Wootan 1997.) Model generated values for radionuclides in any of 177 tanks are reported in the HDW Rev. 4 model results (Agnew et al. 1997a). The best-basis value for any one analyte may be either a model result or a sample or engineering assessment-based result if available. (No attempt has been made to ratio or normalize model results for all 46 radionuclides when values for measured radionuclides disagree with the model.) For a discussion of typical error between model derived values and sample derived values, see Kupfer et al. 1997, Section 6.1.10.

The best-basis inventory for tank 241-U-203 is presented in Tables B4-1 and B4-2. The inventory values reported in Tables B4-1 and B4-2 are subject to change. Refer to the Tank Characterization Database (TCD) for the most current inventory values.

Table B4-1. Best-Basis Inventory Estimates for Nonradioactive Components in Tank 241-U-203 (Effective May 31, 1997). (2 Sheets)

Analyte	Total inventory (kg)	Basis (S, M, C, or E) ¹	Comment
Al	1,620	E	
Bi	<7.64	E	
Ca	7.11	E	
Cl	21.1	E	
TIC as CO ₂	62.8	M	
Cr	13.9	E	
F	17.5	E	
Fe	22.9	E	
Hg	6.20	M	
K	5.60	E	
La	0	M	
Mn	5.37	E	
Na	816	E	
Ni	17.2	E	
NO ₂	258	E	
NO ₃	1,070	E	
OH _{TOTAL}	3,270	C	Derived from charge balance
Pb	30.0	E	
PO ₄	24.4	E	
Si	19.5	E	
SO ₄	16.7	E	
Sr	3.42	E	
TOC	13.5	E	
U _{TOTAL}	68.7	E	
Zr	0.78	E	

¹S = Sample-based

M = Hanford Defined Waste model-based, Agnew et al. (1997a)

E = Engineering assessment-based

C = Calculated by charge balance; includes oxides as hydroxides, not including CO₃, NO₂, NO₃, PO₄, SO₄, and SiO₃.

Table B4-2. Best-Basis Inventory Estimates for Radioactive Components in Tank 241-U-203 Decayed to January 1, 1994 (Effective May 31, 1997). (2 Sheets)

Analyte	Total inventory (Ci)	Basis (S, M, or E) ¹	Comment
³ H	0.323	M	
¹⁴ C	0.0255	M	
⁵⁹ Ni	0.00345	M	
⁶⁰ Co	0.0101	M	
⁶³ Ni	0.322	M	
⁷⁹ Se	0.00543	M	
⁹⁰ Sr	1,530	E	
⁹⁰ Y	1,530	E	Referenced to ⁹⁰ Sr.
⁹³ Zr	0.0257	M	
^{93m} Nb	0.0210	M	
⁹⁹ Tc	0.179	M	
¹⁰⁶ Ru	3.01 E-08	M	
^{113m} Cd	0.0790	M	
¹²⁵ Sb	0.0150	M	
¹²⁶ Sn	0.00835	M	
¹²⁹ I	3.44 E-04	M	
¹³⁴ Cs	2.61 E-04	M	
¹³⁷ Cs	1,390	E	
^{137m} Ba	1,310	E	Referenced to ¹³⁷ Cs.
¹⁵¹ Sm	19.4	M	
¹⁵² Eu	0.00316	M	
¹⁵⁴ Eu	0.244	M	
¹⁵⁵ Eu	0.150	M	
²²⁶ Ra	4.01 E-07	M	
²²⁷ Ac	2.30 E-06	M	
²²⁸ Ra	4.67 E-12	M	
²²⁹ Th	7.78 E-10	M	
²³¹ Pa	8.19 E-06	M	

Table B4-2. Best-Basis Inventory Estimates for Radioactive Components in Tank 241-U-203 Decayed to January 1, 1994 (Effective May 31, 1997). (2 Sheets)

Analyte	Total inventory (Ci)	Basis (S, M, or E) ¹	Comment
²³² Th	6.84 E-12	M	
²³² U	5.00 E-06	M	
²³³ U	1.85 E-07	M	
²³⁴ U	0.115	M	
²³⁵ U	0.00487	M	
²³⁶ U	0.00251	M	
²³⁷ Np	0.00117	M	
²³⁸ Pu	0.191	M	
²³⁸ U	0.112	M	
²³⁹ Pu	13.8	M	
²⁴⁰ Pu	1.73	M	
²⁴¹ Am	0.0412	M	
²⁴¹ Pu	10.6	M	
²⁴² Cm	6.97 E-05	M	
²⁴² Pu	4.48 E-05	M	
²⁴³ Am	8.51 E-07	M	
²⁴³ Cm	1.59 E-06	M	
²⁴⁴ Cm	3.04 E-05	M	

¹S = Sample-based

M = Hanford Defined Waste model-based, Agnew et al. (1997a)

E = Engineering assessment-based.

B5.0 APPENDIX B REFERENCES

- Agnew, S. F., J. Boyer, R. A. Corbin, T. B. Duran, J. R. FitzPatrick, K. A. Jurgensen, T. P. Ortiz, and B. L. Young, 1997a, *Hanford Tank Chemical and Radionuclide Inventories: HDW Model Rev. 4*, LA-UR-96-3860, Los Alamos National Laboratory, Los Alamos, New Mexico.
- Agnew, S. F., R. A. Corbin, T. B. Duran, K. A. Jurgensen, T. P. Ortiz, and B. L. Young, 1997b, *Waste Status and Transaction Record Summary (WSTRS Rev. 4)*, LA-UR-97-311, Rev. 0, Los Alamos National Laboratory, Los Alamos, New Mexico.
- DiCenso, A. T., L. C. Amato, J. D. Franklin, G. L. Nuttall, K. W. Johnson, P. Sathyanarayana, and B. C. Simpson, 1994, *Tank Characterization Report for Single-Shell Tank 241-S-104*, WHC-SD-WM-ER-370, Rev. 0, Westinghouse Hanford Company, Richland, Washington.
- Hanlon, B. M., 1997, *Waste Tank Summary Report for Month Ending March 31, 1996*, HNF-EP-0182-108, Lockheed Martin Hanford Corporation, Richland, Washington.
- Hill, J. G., G. S. Anderson, and B. C. Simpson, 1995, *The Sort on Radioactive Waste Type Model: A Method to Sort Single-Shell Tanks into Characteristic Groups*, PNL-9814, Rev. 2, Pacific Northwest Laboratory, Richland, Washington.
- Hodgson, K. M., and M. D. LeClair, 1996, *Work Plan for Defining a Standard Inventory Estimate for Wastes Stored in Hanford Site Underground Tanks*, WHC-SD-WM-WP-311, Rev. 1, Lockheed Martin Hanford Corporation, Richland, Washington.
- Kupfer, M. J., A. L. Boldt, B. A. Higley, K. M. Hodgson, L. W. Shelton, B. C. Simpson, and R. A. Watrous (LMHC), S. L. Lambert, and D. E. Place (SESC), R. M. Orme (NHC), G. L. Borsheim (Borsheim Associates), N. G. Colton (PNNL), M. D. LeClair (SAIC), R. T. Winward (Meier Associates), and W. W. Schulz (W²S Corporation), 1997, *Standard Inventories of Chemicals and Radionuclides in Hanford Site Tank Wastes*, HNF-SD-WM-TI-740, Rev. 0, Lockheed Martin Hanford Corporation, Richland, Washington.
- Raphael, G. F., and T. T. Tran, 1995, *Tank Characterization Report for Single-Shell Tank 241-U-204*, WHC-SD-WM-ER-486, Rev. 0C, Westinghouse Hanford Company, Richland, Washington.
- Simpson, B. C., J. G. Field, D.W. Engel, and D. S. Daly, 1996, *Tank Characterization Report for Single-Shell Tank 241-S-107*, WHC-SD-WM-ER-589, Rev. 0, Westinghouse Hanford Company, Richland, Washington.

Watrous, R. A., and D. W. Wootan, 1997, *Activity of Fuel Batches Processed Through Hanford Separations Plants, 1944 Through 1989*, HNF-SD-WM-TI-794, Rev. 0, Lockheed Martin Hanford Corporation, Richland, Washington.